

Atomistic Simulation on the Mechanical Properties of Diffusion Bonded Zr-Cu Metallic Glasses with Oxidized Interfaces

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ABSTRACT

A novel welding technique of diffusion bonding for Zr-Cu metallic glass with pre-oxidized surfaces is proposed in this study, which is systematically investigated by molecular dynamics (MD) simulation. Compared with the conventional welding technique, the diffusion bonding process can be well implemented below the crystallization temperature of metallic glass. The obtained structure possesses glass-glass interfaces (GGIs) similar with those in nano-glasses. As revealed by MD simulation, the diffusion bonded metallic glasses possess enhanced mechanical strength and ductility that generally do not exist in nano-glasses and their bulk metallic glass counterparts. The GGIs are found to hinder the propagation of shear bands, where there is strong bonding between Zr and O and the segregated Cu and ZrO₂ clusters could induce extra plasticity. The results demonstrate that the diffusion bonding of metallic glass with pre-oxidized surfaces could provide an alternative approach in solving the longstanding issue of size limitation on metallic glasses.

I. INTRODUCTION

Amorphous alloys, also known as metallic glasses (MGs), possess outstanding mechanical properties including high mechanical strength and excellent corrosion resistance, and are promising for structural applications [1]-[2]. Even though different MGs with a variety of compositions have been fabricated in the past decades, the MGs are still not large enough in physical dimensions (< 10 cm) due to the fast quenching rate required for suppressing crystallization. Meanwhile, conventional welding technique cannot be applied to MGs due to high temperature profiles at heat affected zone (HAZ) that might induce crystallization. The mechanical properties of MG might be greatly deteriorated if low-temperature (< 500 °C) solders are used in the welding process. Therefore, to overcome the size limitation on MGs, other welding techniques for MGs should be further investigated and developed. By far, only a few studies have been reported, demonstrating the feasibility of friction, electron-beam, spark, pulse-current and explosive jointing techniques in wedding MGs [3]-[7]. However, those alternative approaches are not suitable for massive manufacturing and the processing parameters must be precisely controlled. Moreover, the mechanical performances of MGs welded by those approaches are at best compatible to those of as-prepared MGs.

Recently, a novel type of nanomaterial, named as nano-glass, has been successfully prepared, which consists of numerous glass-glass interfaces (GGI) connecting different nano-sized MG clusters or particles [8]-[11]. It is mainly synthesized by inert gas condensation, magnetron sputtering, serve plastic deformations and electrodeposition. Among these techniques, inert gas condensation is the most commonly used one, which produces nano-glasses by compacting nano-sized MG clusters under high external pressure (>100 MPa) and

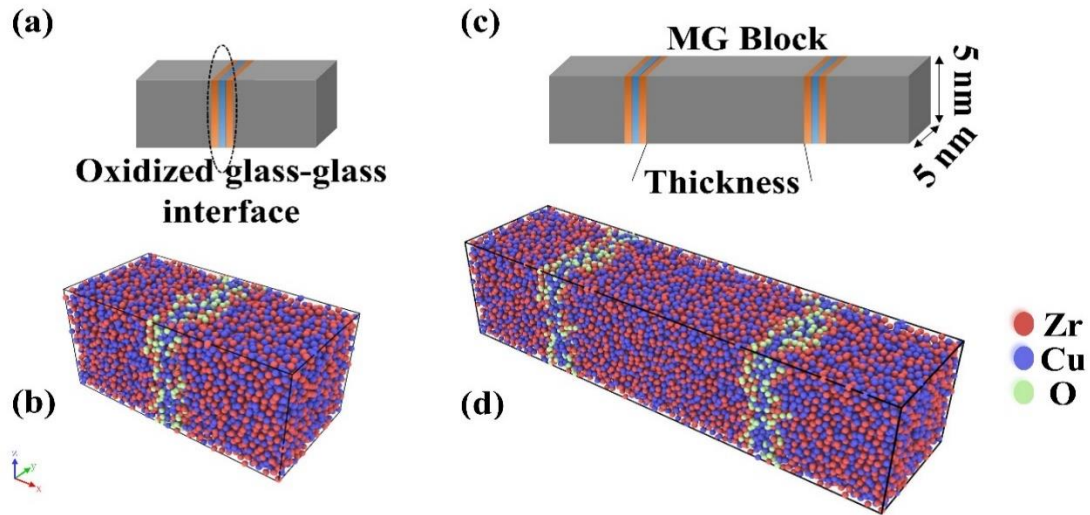
45 at ambient or elevated temperatures [12]-[13]. Such formation of nano-glasses can be
46 considered as diffusion bonding, and could be promising in solving the longstanding issue of
47 size limitation on MGs. Moreover, the ductility of as-prepared nano-glasses is found to be
48 enhanced, compared to those of their bulk MG counterparts [14]–[25]. On the other hand, the
49 viability of diffusion bonding for nano-glass fabrication under ambient conditions, e.g., without
50 the protection of inert gases, becomes critical and the formation of GGIs among different MG
51 clusters must be facile to eliminate the manufacturing barrier, for example, through the powder
52 metallurgy manufacturing route. Nonetheless, one of the challenging issues of handling nano-
53 sized MG clusters or powders in those manufacturing routes is the oxidation inevitably occurred
54 on the surfaces of MGs. Thus, it is necessary to understand the effects of oxidized layers of the
55 nano-sized MG clusters on the diffusion bonding of nano-glasses.

56 In this study, we investigate the diffusion bonding of MG blocks with oxidized surfaces
57 since surface oxidation of nano-sized MG blocks cannot be avoided at ambient processing
58 conditions. From molecular dynamics (MD) simulation, the pre-oxidized surfaces are found to
59 facilitate the formation of GGIs at different diffusion bonding temperatures under atmospheric
60 pressure, firmly connecting the nano-sized MG blocks and resulting in multilayer structures.
61 Furthermore, the mechanical properties of the diffusion bonded MGs are predicted and the size
62 effects of oxidized MG blocks on their mechanical properties are investigated.

63 64 **II. SIMULATION METHODOLOGIES**

65 The MD simulations were performed using Large-Scale Atomic/Molecular Massively
66 Parallel Simulator (LAMMPS) [26]. A representative crystalline $Zr_{50}Cu_{50}$ alloy with
67 dimensions of $5 \times 5 \times 5 \text{ nm}^3$, roughly 7000 atoms, was constructed using ATOMSK software
68 [27] and initially relaxed at 300 K for 100 ps under zero external pressure. Periodic boundary
69 conditions (PBCs) were applied and the embedded atom method (EAM) [28] was used to
70 describe the inter-atomic interactions of Zr-Zr, Zr-Cu and Cu-Cu atoms. Then the system was
71 heated gradually and equilibrated at 2000 K (above the melting temperature $T_m = 1400 \text{ K}$) for
72 2 ns to allow for the complete melting of $Zr_{50}Cu_{50}$, and the melt was quenched to 300 K at a
73 cooling rate of 10^{12} K s^{-1} and relaxed for 500 ps. The obtained $Zr_{50}Cu_{50}$ was further analyzed
74 by radial distribution function that confirmed its amorphous structure. Subsequently, a
75 replicated MG block was placed at the other side and an additional O_2 layer was inserted
76 between two MG blocks. As shown in Fig. 1(a), the surface of each MG block was exposed to
77 O_2 . Oxidation at the exposed MG surfaces under zero external pressure was simulated at 300-
78 600 K for 2 ns by using canonical-ensemble (NVT) MD. The Charge-Optimized Many-Body
79 (COMB3) potential [29] was used to describe the inter-atomic interactions of Zr-O, Cu-O and
80 O-O atoms. After the oxidation, the extra O_2 molecules were removed and the remained MG
81 blocks with oxidized surfaces were consolidated for 2 ns under a hydrostatic pressure of 1 bar
82 at 400, 500, 600 and 700 K (the glass transition temperature $T_g = 670 \text{ K}$), separately. After the
83 bonding process, the system was equilibrated at 300 K for 1 ns, resulting in the diffusion bonded
84 MG structure with one GGI, as shown in Fig. 1 (b). In order to investigate the size effects on
85 the mechanical properties of the diffusion bonded MGs, MG blocks with oxidized surfaces (Fig.
86 1c) which had roughly 10000, 20000, 30000, 40000 and 60000 atoms and were 2.5, 5, 10, 15,
87 20 nm in thickness, were consolidated at 600 K under a hydrostatic pressure of 1 bar, as
88 simulated by isobaric-isothermal (NPT) ensemble MD. Different from the previously obtained

89 systems with one GGI only, the systems containing MG blocks with different thicknesses
 90 contained two GGIs, as shown in Fig. 1 (d). In the aforementioned MD simulations of oxidation
 91 and diffusion bonding processes, PBC was applied in each direction and the finally obtained
 92 diffusion bonded MGs formed the multilayer structures, as shown in Fig. 1.

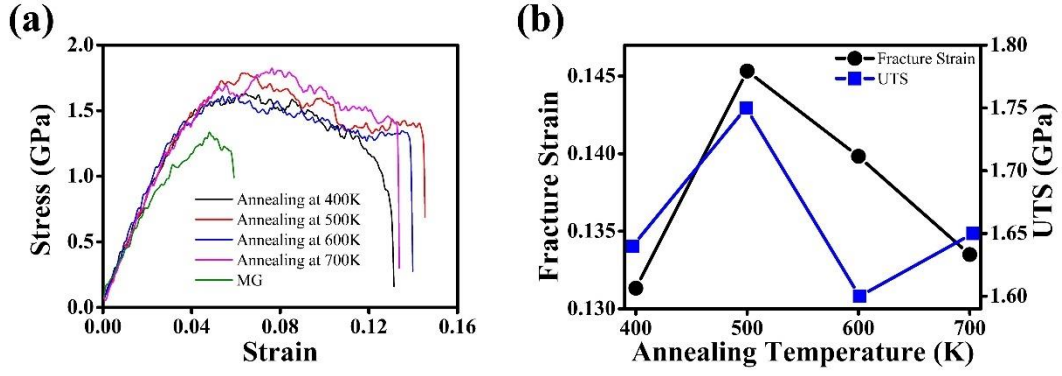


93
 94 **Fig. 1.** Schematics of diffusion bonded $Zr_{50}Cu_{50}$ MGs with (a) one GGI, and (c) two GGIs, whose atomic
 95 structures are shown in (b) and (d), respectively.

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 97 All diffusion bonded systems were equilibrated at 300 K for 2 ns before the uniaxial tensile
 98 loading was applied in x -direction at a strain rate of $3.33 \times 10^7 \text{ s}^{-1}$. There were lateral tractions
 99 at y - and z -directions during the tensile loading process, and the temperature was kept at 300 K
 100 by using a Nose-Hoover thermostat in NVT ensemble MD simulation. The atomistic
 101 mechanisms of diffusion bonding and mechanical deformation were analyzed by self-scripted
 102 MATLAB code and visualized by OVITO software packages [30].

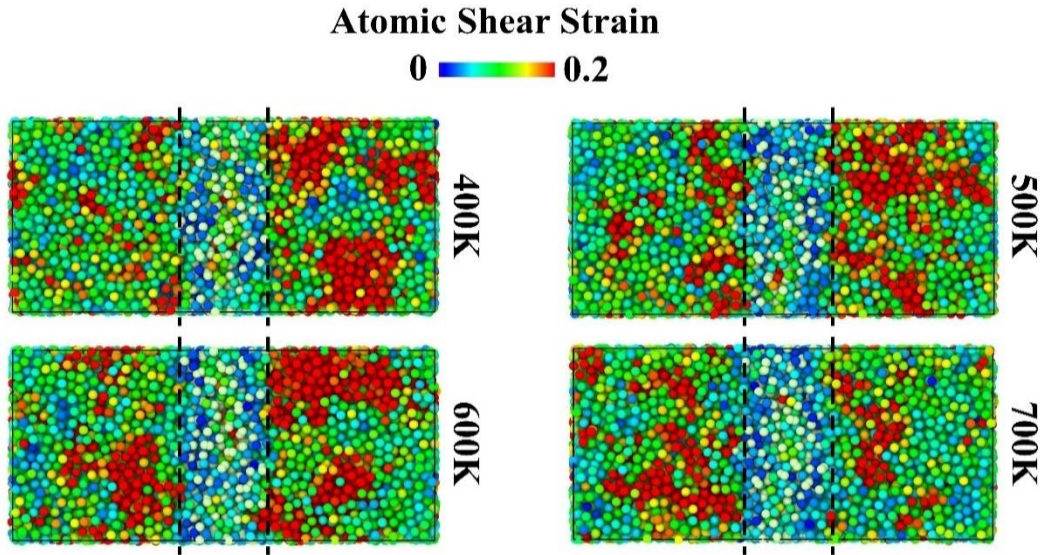
104 III. RESULTS AND DISCUSSION

105 The diffusion bonded MGs with one and two GGIs are shown in Fig. 1 (b) and (d),
 106 respectively, clearly indicating that the GGIs have different atomic structure with the MG
 107 blocks. The mechanical properties of diffusion bonded Zr-Cu MGs with one oxidized GGI,
 108 which contain 10 nm Zr-Cu MG blocks welded at different temperatures, are investigated by
 109 the tensile tests. The engineering stress vs. strain curves, presented in Fig. 2 (a), reveal that the
 110 Zr-Cu MGs are well bonded together, without showing a sudden stress drop with a strain lower
 111 than the elastic limit of Zr-Cu MGs ($\sim 2\%$). After reaching its ultimate tensile strength (UTS) at
 112 1.52 -1.75 GPa, the engineering stress starts decreasing until the fracture occurs. It is found that
 113 the welded Zr-Cu MGs with oxidized GGI could have enhanced UTS and ductility as measured
 114 by the plastic strain at the UTS, in comparison with those of pristine MGs (Fig. 2a). Among the
 115 systems investigated, Zr-Cu MG bonded at 500 K exhibits the best combination of mechanical
 116 strength and ductility, i.e., an extra plasticity of 6.2% and a UTS of 1.75 GPa.



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Fig. 2. The mechanical properties of diffusion bonded MGs with MG blocks 10 nm in thickness. (a) Stress vs strain curves for the MGs bonded at different temperatures. (b) The influences of welding temperature on fracture strain and UTS.



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Fig. 3. The atomic shear strain mapping for MGs bonded at 400, 500, 600 and 700 K with an engineering strain of 7.5 %. The dash lines mark the GGI regions.

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To have a better understanding on the welding temperature dependence mechanical properties, the mapping of atomic shear strain for each diffusion bonded MG at an engineering strain of 7.5% is shown in Fig. 3, and the shear bands can be identified as those localized regions with high shear strains. Here, the atomic shear strain is defined as [31-34]:

$$\eta_i = \frac{1}{2} (J_i J_i^T - I) \quad , \quad (1)$$

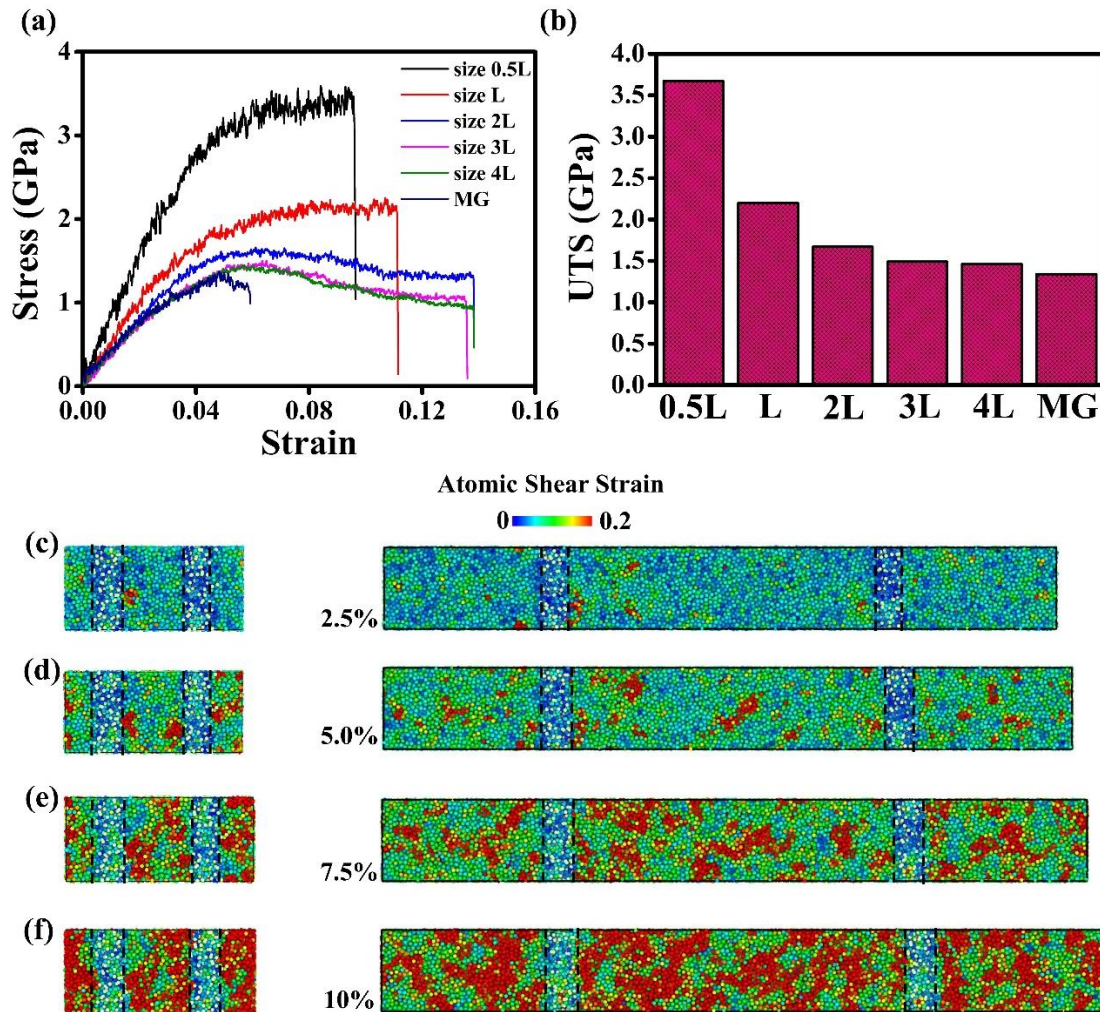
$$\eta_i^{\text{Mises}} = \sqrt{\eta_{xy}^2 + \eta_{xz}^2 + \eta_{yz}^2 + \frac{(\eta_{xx} - \eta_{yy})^2 + (\eta_{xx} - \eta_{zz})^2 + (\eta_{yy} - \eta_{zz})^2}{6}} \quad , \quad (2)$$

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where η_i is the local Lagrangian strain matrix for each atom i , J_i is the local transformation matrix and η_i^{Mises} is the atomic shear strain. It can be observed that in the MGs bonded at 500 K, the GGI actively involves in the plastic deformation and the roles of GGI are two folded. The shear bands can be generated from GGI and propagate into the MG blocks, or they are generated inside the MG block and are hindered by the GGI, resulting in the enhanced plasticity

137 and mechanical strength, respectively. The mapping of shear strain in the MG blocks at both
 138 sides of GGI, as shown in Fig. 3, indicates that in the MGs bonded at 500 K there are 5 localized
 139 shear regions that can be connected with GGI. For other diffusion bonded MGs at different
 140 temperatures (400, 600 and 700 K), on the contrary, the GGI is less involved during the plastic
 141 deformation and the number of those regions are only 2 to 3. It could be the reason that their
 142 mechanical properties are not compatible to those of MGs bonded at 500 K.

143 To investigate the size effects on the mechanical properties of diffusion bonded Zr-Cu
 144 MGs, MG blocks with different sizes in thickness are oxidized and welded at 600 K. The stress
 145 vs. strain curves for diffusion bonded MGs are analyzed, as shown in Fig. 4 (a). The Young's
 146 modulus and tensile strength of diffusion bonded MGs are enhanced as the thickness of MG
 147 block decreases, while the elongation to failure of diffusion bonded MGs is deteriorated. When
 148 the thickness of MG block is lower than 5 nm, its tensile strength is dramatically increased up
 149 to 3.7 GPa, as shown in Fig. 4 (b). The tensile strength of diffusion bonded MGs is close to that
 150 of pristine MGs when the thickness of MG block is increased to 20 nm. Moreover, the ductility
 151 is dramatically improved from 4.8% to nearly 10% when the thickness of MG blocks is reduced
 152 to 2.5 nm.

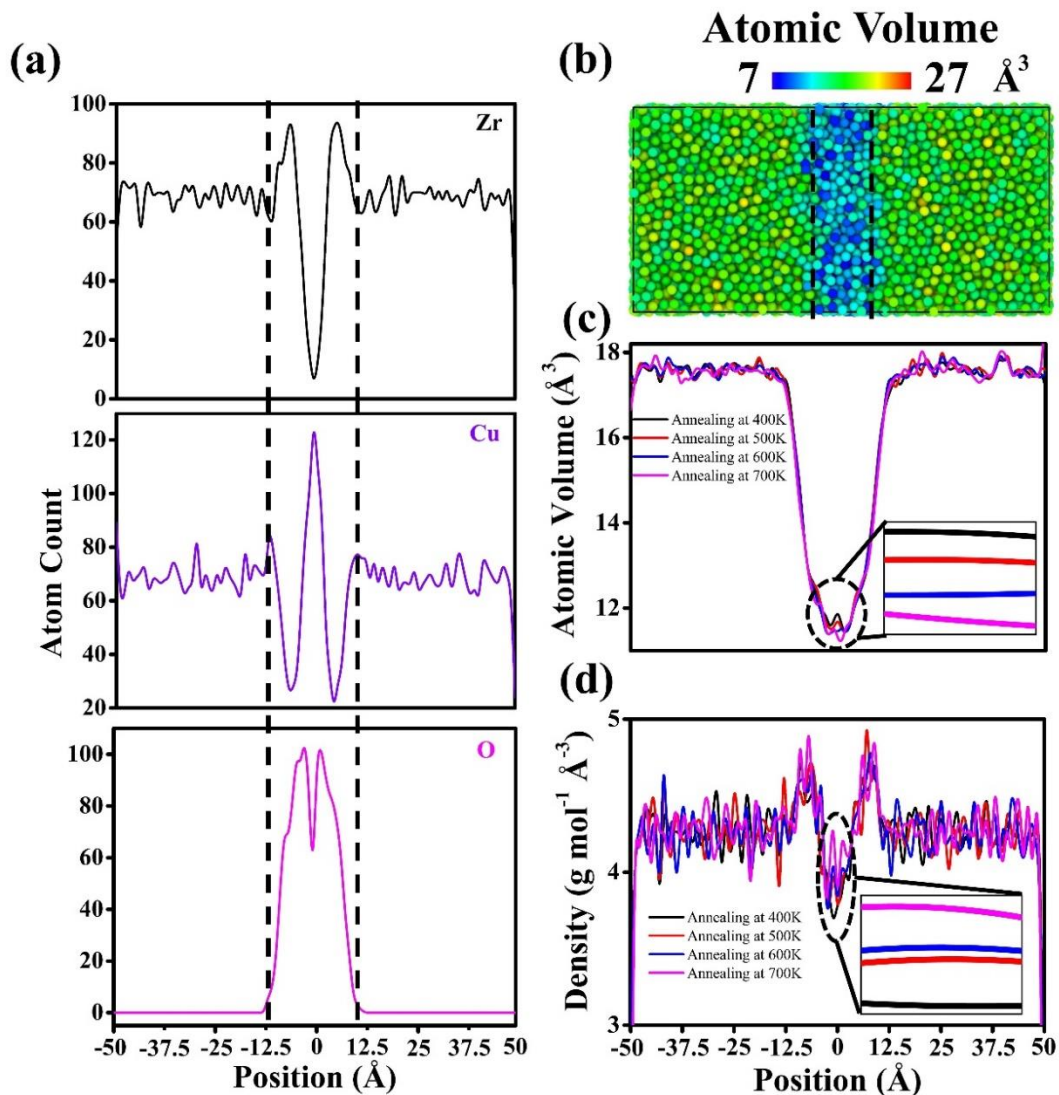


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 154 **Fig. 4.** (a) Stress vs strain curves of the diffusion bonded MGs with MG blocks in different sizes
 155 (thicknesses); L=5 nm. (b) The size effects on UTS. Atomic shear strain mapping of diffusion bonded
 156 MGs with MG blocks 5-nm (left column) and 20-nm in thickness (right column), which are deformed at

157 strains of 2.5% (c), 5% (d), 7.5% (e), 10% (f). The dash lines mark the GGI regions.

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159 The mapping of atomic shear strain for the diffusion bonded MGs with 5 and 20 nm MG
160 blocks in thickness is shown in Fig. 4. When the diffusion bonded MGs are under plastic
161 deformation (strain>2%), both systems are deformed heterogeneously with the initiation of
162 shear bands either inside the MG blocks or from the GGIs. At an engineering strain of 5%, the
163 shear bands are found to propagate along the direction with an incline angle of about 45° with
164 the loading direction. In the diffusion bonded MGs with 20 nm MG blocks, most shear bands
165 do not interact with GGIs, and grow across the system in the lateral direction, directly leading
166 to the catastrophic failure of the bonded MGs. However, in the diffusion bonded MGs with 5
167 nm MG blocks, the shear bands are hindered by GGIs, and as a result, the mechanical strength
168 is enhanced. Fig. 4 (c)-(f) thus demonstrates that the roles of GGI may be different in the
169 diffusion bonded MGs containing MG blocks with different sizes. Therefore, as shown in Fig.
170 4 (b), the mechanical strength of diffusion bonded MGs is found to significantly increase when
171 the ratio of thickness to lateral dimension of the MG blocks is less than 1.0.



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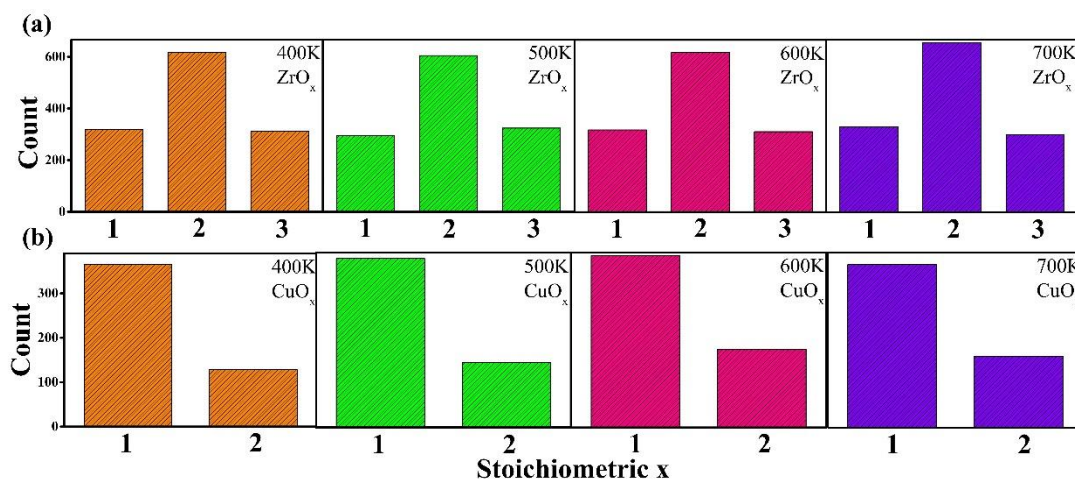
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Fig. 5. The chemical composition analysis on oxidized interfaces in the bonded Zr-Cu MGs with L=5 nm: (a) atomic count variation vs position, (b) visualization of atomic volume, (c) atomic volume at the

175 interface bonded at different welding temperatures, and (d) density at the interface bonded at different
 176 temperatures. The dash lines mark the GGI regions.

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178 Since the oxidized interface plays an important role in low-temperature welding and in
 179 enhancing mechanical properties of the diffusion bonded MGs, it is necessary to conduct a
 180 comprehensive investigation about the structure and composition of oxidized interface for a
 181 better understanding about the mechanisms of welding and the enhanced mechanical properties
 182 of bonded MGs. In Fig. 5 (a), the composition variation is plotted with respect to the position
 183 in the system. It can be seen from the plots that the atoms are evenly distributed in the MG
 184 blocks and the composition variation can be observed at the positions close to the oxidized
 185 interface. In general, the oxidized interface could be divided into two different regions that
 186 consist of different chemical compositions. The Cu atoms are highly concentrated in the center
 187 of oxidized interface, where Zr and O atoms are more preferentially located on the MG blocks
 188 at both sides of the interface. Compared with the MG blocks, the oxidized interface exhibits a
 189 reduced atomic volume, as shown in Fig. 5 (b). However, as the welding temperature is
 190 increased, the atomic volume at oxidized interface is further decreased while the density at the
 191 interface is enhanced, as shown in the Fig. 5 (c) and (d). Moreover, the density in the center of
 192 oxidized interface is determined to be the minimum, less than that of MG blocks. In contrast,
 193 the density at both sides of the oxidized interface exhibits the maximum, where Zr and O atoms
 194 are enriched. By analyzing the atomic structure, quite a few ZrO_2 clusters, as shown in Fig. 6
 195 (a), have been found at the oxidized interface. Moreover, as shown in Fig. 6(b), a small amount
 196 of CuO clusters can be observed at the oxidized interface where Cu atoms seem to be less
 197 favorable to interact with O atoms as compared with Zr atoms. The formation of ZrO_2 clusters
 198 is critical to the enhanced mechanical properties of the diffusion bonded MGs since the
 199 mechanical strength of ZrO_2 crystal is as high as 2000 MPa [35]. On the one hand, the ultimate
 200 tensile strength of diffusion bonded MGs could be much enhanced since the ZrO_2 clusters could
 201 be hard obstacles that impede the propagation of shear bands generated in the interiors of MG
 202 blocks. On the other hand, the formation of ZrO_2 clusters leads to the structural heterogeneity
 203 around the GGI, where shear bands could be generated close to the resultant ZrO_2 clusters.
 204 Because of the sparse distribution of ZrO_2 clusters, multiplication of shear bands at the ZrO_2
 205 clusters could lead to the enhanced ductility of the diffusion bonded MGs.

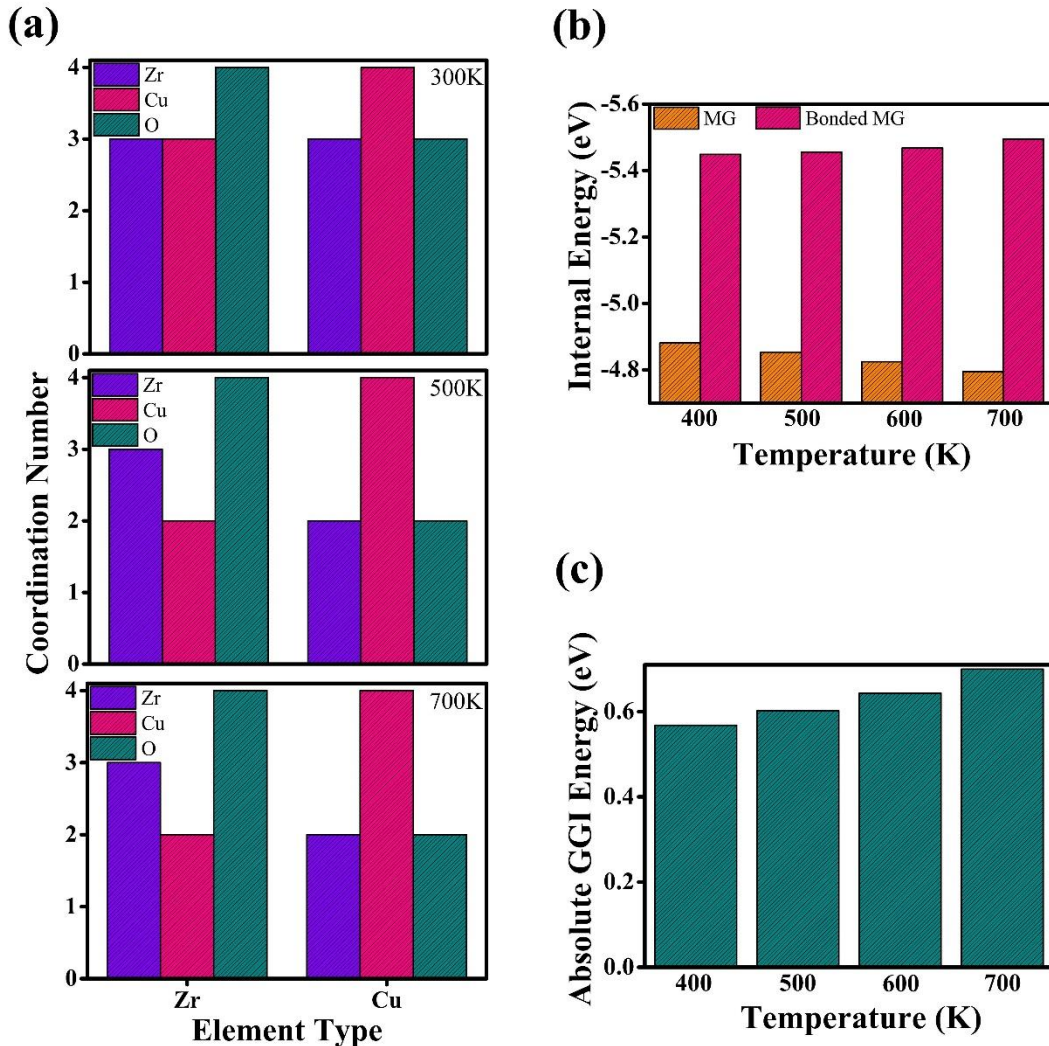


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Fig. 6. Analyses on the chemical composition of (a) Zr-O, and (b) Cu-O clusters formed at glass-glass

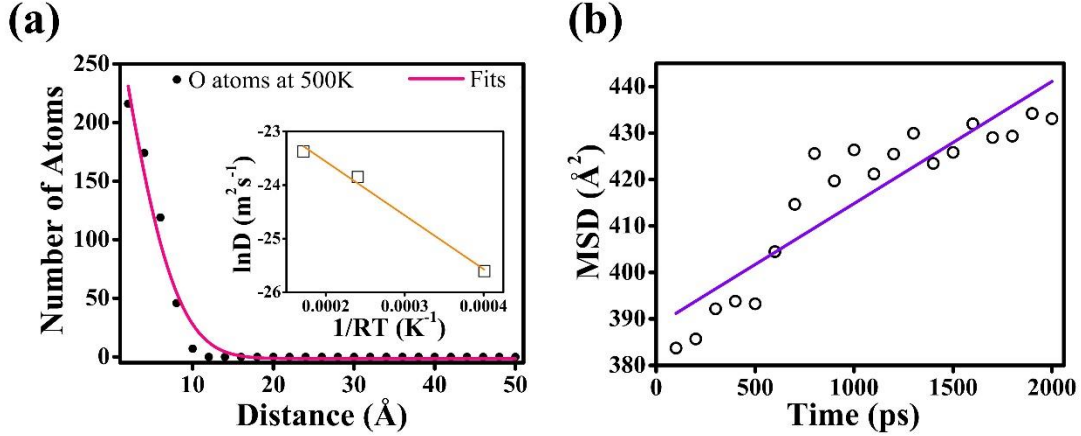
208 interfaces in the MGs bonded at different temperatures.
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210
 211 **Fig. 7.** (a) The coordination analysis on Zr-, and Cu-centered clusters in the MGs bonded at different
 212 temperatures. (b) Internal energy of MG and diffusion bonded MGs. (c) Absolute energy of the glass-
 213 glass interface.

214
 215 The atomic coordination of Zr and Cu atoms at the MG surface oxidized under different
 216 temperatures are analyzed, as shown in Fig. 7 (a). For all oxidization temperatures, the O atoms,
 217 with an approximated average amount of 4 for Zr-centered atom and 2-3 for Cu-centered atom,
 218 are more preferential to interact with the Zr atoms. Meanwhile, Cu-centered atom tends to
 219 closely interact with other Cu atoms, leading to the formation of Cu clusters during the
 220 oxidation process. Therefore, the majority of Cu clusters, concentrated in the center of oxidized
 221 interface, could be also responsible for the enhanced ductility of the diffusion bonded MGs. In
 222 other words, during the welding process, those Cu clusters play an important role, as low-
 223 temperature solder, firmly bonding the MG blocks together while providing high ductility of
 224 the diffusion bonded MGs under plastic deformation. The oxidized interface is found to be
 225 stable, as shown in Fig. 7 (b). As the welding temperature is increased, the internal energy of
 226 MGs increases and becomes less stable. In contrast, the internal energy of the diffusion bonded

227 MGs decreases at higher welding temperature. Such a phenomenon is obviously related with
 228 the oxidized interface or GGI and indicates a much stable structure of oxidized interface. In
 229 addition, the absolute average GGI energy is positively correlated with the welding temperature,
 230 which implies an excellent stability of oxidized interface at high welding temperatures, as
 231 shown in Fig. 7 (c).



232
 233 **Fig. 8.** Diffusion analysis on O atoms during the oxidation at the MG interface at 500 K by applying
 234 (a) Fick's second law of diffusion (at $t=2$ ns), and (b) Einstein relation. The inset in (a) is the fits of
 235 diffusion coefficient D by using Arrhenius equation.

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237 In order to explain the heterogeneous atomic structure and position-dependent chemical
 238 composition around the GGIs, the analysis on diffusions of Zr, Cu and O atoms during oxidation
 239 processes is conducted. At the surface of MG under oxidation, Fick's second law or non-
 240 steady state diffusion could be used to analyze the diffusion coefficients of Zr, Cu and O atoms
 241 and the relation is expressed in the following equation

$$242 \quad \frac{c_x - c_0}{c_s - c_0} = 1 - \operatorname{erf}\left(\frac{x}{2\sqrt{Dt}}\right) \quad , \quad (3)$$

243 where c_x is the concentration at position x , c_s is the surface concentration of diffusing atoms, c_0
 244 is the uniform concentration of diffusing atoms away from the surface, D is the diffusion
 245 coefficient and t is time. For the diffusion coefficient of each atom type inside the MG block,
 246 Einstein relation is applied, and the corresponding equation could be expressed as

$$247 \quad \text{MSD} = 6 D t + C \quad , \quad (4)$$

248 where MSD is the mean square displacement for each atom type and C is the constant. Finally,
 249 the activation energy of diffusion for each element is determined by Arrhenius relation, as
 250 follows:

$$251 \quad D = D_0 e^{\frac{E_a}{RT}} \quad , \quad (5)$$

252 where E_a is the activation energy, R is the universal gas constant, T is the temperature in Kelvin
 253 and D_0 is the maximal diffusion coefficient. Diffusion analysis at the interface under oxidation
 254 is performed in every 100 ps at different oxidation temperatures. Meanwhile, the diffusion
 255 coefficient inside the MG block is obtained when mean square displacement and its
 256 corresponding time follow a linear relationship. Taking the diffusions of O atoms as examples,
 257 Fig. 8(a) and (b) shows the determination on the diffusion coefficients D at the surface and in
 258 the interior of MG blocks during oxidation processes, using Eqs. (3) and (4), respectively. The

259 activation energy of diffusion of O atoms is determined by Eq. (5), as shown in the inset of Fig.
 260 8(a).

261

262 **Table I.** The diffusion coefficients and activation energies of Zr, Cu and O atoms at the surface and in
 263 the interior of MG blocks during oxidization

Element Type		Diffusion Coefficient ($\text{m}^2 \text{s}^{-1}$)			Activation Energy E_a (kJ mol^{-1})
		300 K	500 K	700 K	
Surface of MG block	Zr	5.71×10^{-13}	1.13×10^{-12}	2.20×10^{-12}	5.88
	Cu	7.29×10^{-12}	8.32×10^{-12}	7.56×10^{-11}	11.8
	O	5.32×10^{-12}	6.93×10^{-12}	2.44×10^{-11}	8.24
Interior of MG block	Zr	4.03×10^{-13}	2.02×10^{-12}	5.33×10^{-12}	11.1
	Cu	4.27×10^{-13}	2.73×10^{-12}	9.32×10^{-12}	13.3
	O	7.60×10^{-12}	4.38×10^{-11}	7.09×10^{-11}	10.0

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265 As listed in Table I, the diffusion coefficient of Zr atoms at the surface under oxidization
 266 is much lower than those of Cu atoms and O atoms. Consequently, the Cu atoms could diffuse
 267 to and aggregate at the outer layer of the oxidized surface of the MG block, while O atoms
 268 could diffuse into the interiors of MG block and interact with Zr atoms to form the ZrO_2 clusters,
 269 as shown in Fig. 7(a). Thus, the fact that after the diffusion bonding processes there is broken
 270 concentration homogeneity of Cu and Zr atoms in the GGIs, as shown in Fig. 5, can be well
 271 explained. In the diffusion bonded MGs, Cu atoms in the center of GGI could have the highest
 272 concentration, as shown in Fig. 5(a) and Fig. 7(a), and could serve as low-temperature solders
 273 during the welding process. In contrast, Zr atoms tend to form stable ZrO_2 clusters away from
 274 the center of GGI because of the fast diffusion of O atoms from the oxidized surface into the
 275 interior of MG blocks.

276

277 IV. CONCLUSION

278 In summary, a novel low-temperature welding technique for MG is investigated by MD
 279 simulation. The diffusion bonding of Zr-Cu MGs with pre-oxidized surfaces is found to result
 280 in the enhanced mechanical properties of MGs when the bonding temperature and aspect ratio
 281 of the MG blocks are properly chosen. The GGIs in the diffusion bonded MGs are characterized
 282 by the presence of segregated Cu and ZrO_2 clusters, mainly resulting from the fast diffusions
 283 of Cu atom to the center of interface and the diffusion of oxygen atoms into the interior of MG
 284 blocks. The effects of GGIs on the plastic deformation of diffusion bonded MGs are
 285 investigated. This study paves a new avenue to overcome the longstanding issue of size
 286 limitation on MGs.

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