

# LNG-fuelled Container Ship Sailing on the Arctic Sea: Economic and Emission Assessment

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## Abstract

Global warming allows the Northern Sea Route (NSR) to be used as a potential alternative for Asia–Europe shipping. As a clean fuel, liquid natural gas (LNG) has been increasingly used as a marine fuel. This study aims to analyse the economic feasibility and CO<sub>2</sub> emission reduction of using LNG-fuelled container ships to sail through the NSR, under the assumption that Sabetta will be developed into an LNG refuelling centre. We establish a shipping profit model and a CO<sub>2</sub> emission model and then apply real data to them. Several scenarios are proposed to reflect the different circumstances in practice. We find that a shorter round-trip transit time and appropriate ship size are the most favourable factors for the proposed option. Although data suggests that it is often economically infeasible to deploy LNG-fuelled ships via the NSR, under certain circumstances where it is indeed cost-effective, considerable CO<sub>2</sub> emission reduction can be achieved.

**Keywords:** *Northern Sea Route, LNG-fuelled Ship, Economic Feasibility, CO<sub>2</sub> Emission.*

## 1 **1. Introduction**

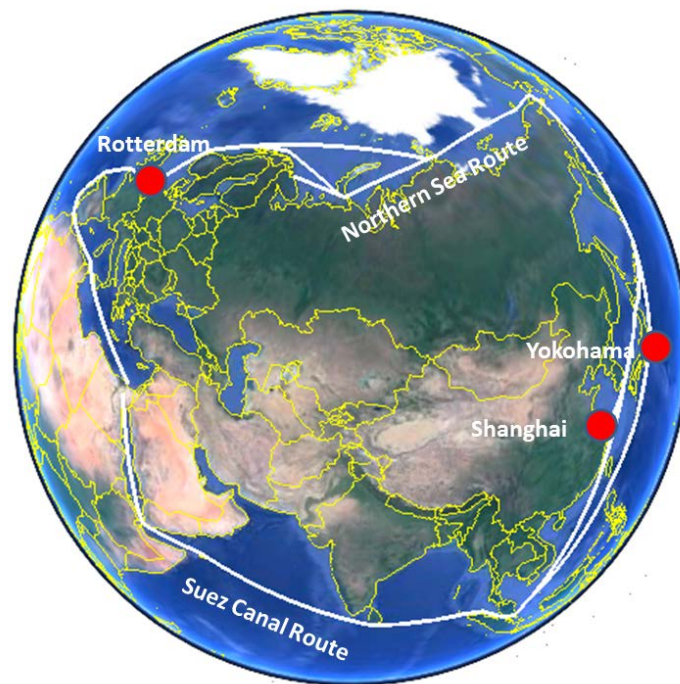
2 The extent of the retreat of Arctic sea ice has made the Arctic Ocean more navigable  
3 than ever. There are three main Arctic shipping routes: the Northeast Passage (the  
4 Russian sector between Cape Dezhnyov and the Kara Strait or Cape Zhelaniya is  
5 called the Northern Sea Route [NSR]), Northwest Passage (through Canadian and  
6 Alaskan Arctic waters), and Trans-Arctic Passage (through the central Arctic Ocean).  
7 These Arctic shipping routes can considerably shorten the sailing distances between  
8 North America, Europe, and East Asia.

9 Because recent ice conditions in the Northwest Passage and Trans-Arctic Passage  
10 have not been suitable for commercial transit navigation, only the NSR has been  
11 developed for transit shipping, a voyage where the origin and destination are both  
12 outside the Arctic region.

13 Non-Russian/Soviet commercial transit shipping on the NSR began in 2009, when  
14 two German ships sailed from Busan to Rotterdam with one stop at a Russian port,  
15 Novy Port, in the middle. Since then, more ships have used the route. In 2013, the  
16 volume of cargo transited via the NSR reached a peak of 1.36 million tonnes. In 2014,  
17 however, NSR transit traffic drastically decreased, partly because of the Western  
18 sanctions on Russia (Zhang *et al*, 2016b). In 2015, the transit cargo volume decreased  
19 to less than 40 thousand tonnes, accounting for only 3% of the amount in the peak  
20 year. After 2015, the transit cargo volume on the NSR began to increase again and

21 recovered to 491 and 697 thousand tonnes in 2018 and 2019, respectively. The recent  
22 main cargos were steel and windmill parts from China to Europe and paper pulp and  
23 non-ferrous ores from Europe to China.

24 As a potential rival to the traditional Suez Canal Route (SCR), the NSR is the main  
25 lane between Asian and European ports. These two routes are presented in Figure 1.  
26 Because of the large trade volume in manufactured goods between Asian and  
27 European countries, the Asia–Europe lane is one of the three busiest container lanes in  
28 the world, and the largest container ships are used on it. If the NSR becomes feasible  
29 for container shipping, the global container shipping map will change drastically.



30

31 **Figure 1 Northern Sea Route (NSR) and Suez Canal Route (SCR)**

32

Source: edited Google Earth screenshot

33 Although container shipping seems to be promising for the NSR, container ships have  
34 rarely observed on the route because of the seasonality and uncertainty of the ice  
35 condition along the NSR, as well as the lack of intermediate ports along the route.  
36 Nevertheless, *Venta Maersk*, a 3,600-TEU full container ship, passed the NSR in 2018.  
37 This is a milestone in Arctic shipping, because she is the first full container ship  
38 sailing the entire NSR.

39 One prominent worldwide trend in the maritime industry is that an increasing number  
40 of ships are being adapted to use liquid natural gas (LNG) as a fuel. LNG is clean  
41 energy relative to conventional oil-based fuels and thus can significantly reduce the  
42 emission of air pollution materials such as SO<sub>x</sub>, NO<sub>x</sub>, particulate matter (PM), and  
43 black carbon. LNG can reduce CO<sub>2</sub> emissions by at least 20% compared to  
44 conventional marine fuel (DNV GL, 2015). Although the “methane slip” problem  
45 (caused by uncombusted methane from engines) could be a major defect of LNG fuel  
46 because of the strong greenhouse capability of methane, high-pressure 2-stroke  
47 dual-fuel (LNG and conventional oil fuel) engines, a recently available technology,  
48 can significantly mitigate this problem (Lindstad and Rialland, 2020).

49 LNG has been widely recognised as an alternative marine fuel for the near future. It  
50 has become particularly relevant because of the 0.5% sulphur control regulation  
51 issued by the International Maritime Organization (IMO), which was enacted at the  
52 beginning of 2020. The number of LNG-fuelled ships is increasing rapidly. According  
53 to Yoo (2019), as of December 2019, there were 172 operating LNG-fuelled ships

54 worldwide, 20.3% more than 2018. Additionally, 31 LNG-fuelled ships were on  
55 order. Notably, the largest LNG-fuelled container ship in the world, 23,000 TEU  
56 *CMA CGM Jacques Saade*, was launched in 2019.

57 In the context of this background, LNG infrastructures are blooming worldwide,  
58 especially in the gas-rich Arctic region. The Yamal LNG project, a joint venture run  
59 by Russian, Chinese, and French enterprises, is located on the Yamal Peninsula. This  
60 Russian Arctic peninsula holds huge natural gas deposits. It is supported by the  
61 Yuzhno-Tambeyskoye gas field and designed to output 16.5 million tonnes of LNG  
62 annually when fully running, in 2018. Sabetta, the gate-port of this project, exported  
63 its first shipment of LNG in December 2017. The LNG will be mostly exported to  
64 Asian and European markets. A reasonable expectation is that LNG is cheaper at the  
65 place of production. Notably, the free on board (FOB) price of Yamal LNG is much  
66 lower than the Northeast Asia-delivered LNG bunker price (discussed in Section 4).  
67 Moreover, one of the challenges for LNG fuel is its high well-to-tank (from  
68 production plants to consumption places) greenhouse gas emission, which suggests  
69 that serious emission occurs in the transport of LNG (Lindstad and Riialand, 2020).  
70 Building an LNG refuelling centre at Sabetta to serve the LNG-fuelled ships sailing  
71 the NSR is a potential solution for this problem because it shortens the LNG supply  
72 chain.

73 The second LNG project, named Arctic LNG 2, is now under construction. It is  
74 located at Utrenneye gas field on the Gyda Peninsula, which is close to Yamal LNG.

75 This project is also an international joint venture, with Russian, French, Chinese, and  
76 Japanese shareholders, and is expected to launch in 2024. After it enters full  
77 production, 19.8 million tonnes of LNG will be produced annually, 20% higher than  
78 the annual output of Yamal LNG. Because of the new technology of gravity-based  
79 structures it applies, the construction of the project will cost approximately USD 21.3  
80 billion, well below that of Yamal LNG, and the production cost per tonne may  
81 decrease by more than 30% (Gulf-times, 2018). Therefore, the FOB LNG bunker  
82 price in Yamal region will be further reduced after Arctic LNG 2 is fully developed.

83 In this study, we explore to what extent the FOB Yamal LNG bunker price reductions  
84 can economically enable the sailing of LNG-fuelled container ships via the NSR  
85 instead of the SCR, and calculate the potential CO<sub>2</sub> emission reduction it can achieve.  
86 For comparison, we conceive three options, namely, LN, ON, and OS, defined as  
87 follows:

88 (1) LN indicates LNG-fuelled ships via the NSR with using Sabetta as an LNG  
89 refuelling centre;

90 (2) ON indicates oil-fuelled ships via the NSR; and

91 (3) OS indicates oil-fuelled ships via the SCR.

92 We assume that liner operators only use LN or ON during the ice-free season on the  
93 NSR but not year-round.

94 The remainder of this study is arranged as follows. In Section 2, the relevant studies  
95 on Arctic shipping and the environmental effects are reviewed. In Section 3, we build  
96 a shipping profit model for evaluating the economic feasibility of NSR LNG-fuelled  
97 shipping, and an emission model for estimating the CO<sub>2</sub> emissions from ships. In  
98 Section 4, an empirical study is conducted with real data to compare the profits and  
99 CO<sub>2</sub> emissions among the three options. Section 5 concludes.

## 100 **2. Literature review**

101 Many studies have focused on the economic feasibility of the NSR by using the  
102 traditional SCR as a benchmark. The majority of these works have been reviewed by  
103 Lasserre (2014) and Meng *et al* (2016). Many of these works reviewed non-container  
104 shipping, such as mineral fertiliser shipping (Schøyen and Bråthen, 2011, Cariou and  
105 Faury, 2015), iron ore shipping (Otsuka *et al*, 2013), LNG shipping (Otsuka *et al*,  
106 2013, Raza and Schøyens, 2014), frozen fish shipping (Otsuka *et al*, 2013), and oil  
107 tanker shipping (Faury and Cariou, 2016, Zhang *et al*, 2016a). One of the most recent  
108 studies was conducted by Theocharis *et al* (2019), who proposed a cost model for  
109 product tankers based on the optimal ship speed.

110 Liner shipping along the NSR has also attracted attention from researchers. Some  
111 studies have estimated the cost of a single voyage of the NSR, for example, Arpiainen  
112 and Kiili (2006) considered a container shuttle service between Alaska and Iceland;  
113 Verny and Grigentin (2009) compared the costs of routes between Shanghai and

114 Hamburg via the SCR, Trans-Siberian railway, NSR, sea and air route transiting in  
115 Dubai, and direct air route; Lasserre (2014) compared the costs of the NSR, the  
116 Northwest Passage, and the SCR with Rotterdam, Shanghai, and Yokohama as  
117 endpoint ports; and Zhang *et al* (2016a) compared the profits of an NSR voyage with  
118 a 5,100 TEU ship to those of an SCR voyage with a 13,900 TEU ship. In other studies,  
119 an NSR/SCR-combined service was considered, in which the NSR was used in the  
120 navigable window, whereas the SCR was used in other seasons. Among these studies,  
121 Liu and Kronbak (2010) compared the cost of a combined service for the SCR  
122 between Yokohama and Rotterdam under different scenarios of navigable time of the  
123 NSR, NSR fees, and bunker prices; Xu *et al* (2011) proposed a combined service in  
124 the NSR with multi-port calling and a one-month navigable window; Omre (2012)  
125 studied a combined service between Yokohama and Rotterdam and assumed 14 ‘ice  
126 alternatives’ with different combinations of ice conditions over 10 NSR sections;  
127 Furuichi and Otsuka (2014) assumed five different scenarios for a navigable window  
128 (105, 135, 165, 195, and 225 days); Zhao *et al* (2016) established a two-stage  
129 optimisation model for shipping network design with multi-port calling and  
130 considered three levels of navigable windows (4, 6, and 8 months); and Xu *et al* (2018)  
131 introduced a new approach for simulating the economic performance of a combined  
132 service with a dynamic navigable window of the NSR. These studies have evaluated  
133 the economic performance of the NSR from various perspectives, but all of them were



134 only concerned with conventional oil-fuelled ships. This study adds a new option to  
135 the literature: LNG-fuelled ships on this route.

136 Arctic shipping can decrease the distances thus reduce fuel consumption considerably;  
137 hence, many studies have focused on the environmental impacts of Arctic shipping,  
138 especially the assessment of ship emissions. For example, Paxian *et al* (2010)  
139 introduced a global bottom-up ship emission algorithm for estimating the fuel  
140 consumption, emissions, and vessel traffic densities of Arctic polar routes in 2050;  
141 Peters *et al* (2011) used a bottom-up shipping model and detailed global energy  
142 market model to construct emission inventories for Arctic shipping and petroleum  
143 activities in 2030 and 2050, given estimated sea ice extents; Dalsøren *et al* (2012)  
144 evaluated the changes in concentrations of atmospheric pollutants and radiative  
145 forcing of short-lived components due to ship emissions from 2004–2030, given the  
146 increasing traffic in the Arctic; Winther *et al* (2014) presented a detailed air pollutant  
147 emission inventory for ships in the Arctic in 2012, based on satellite automatic  
148 identification system data, ship engine power functions, and technologically stratified  
149 emission factors; Lindstad *et al* (2016) adopted the concept of Global Warming  
150 Potentials (GWP) to describe the warming intensity of many maritime air pollutants in  
151 terms of fuels and regions and observed that the net GWP in the Arctic is higher than  
152 those of other routes, even when cleaner fuels (e.g. LNG) are used; Yumashev *et al*  
153 (2017) studied the comprehensive economic impacts of NSR shipping that cover the  
154 environmental benefits from emission reduction, the environmental consequences

155 from the short-lived pollutants (e.g. black carbon) emitted by ships in the Arctic, and  
156 the emissions from the additional economic growth incurred by the NSR; Zhu *et al*  
157 (2018) calculated the emissions of greenhouse gases and pollutants overall in NSR  
158 container shipping and integrated the environmental costs from the emissions into a  
159 cost model; Wan *et al* (2018) provided a case study on emission reduction and profit  
160 increase by using the NSR; Cariou *et al* (2019) estimated the cost saving and CO<sub>2</sub>  
161 emission reduction of container shipping along the NSR by focusing on the impacts of  
162 various ice thicknesses over 49 route subzones; Ding *et al* (2020) investigated the  
163 effect of a carbon tax (fixed vs progressive schemes) on the economic viability of the  
164 NSR against the SCR. These reviewed studies have assessed the environmental  
165 impacts of the NSR shipping but have not associated the emission results with the  
166 economic feasibility of clean energy applied in NSR shipping. Liner operators are  
167 more concerned about the economic performance of the NSR shipping than emission  
168 reduction. This study estimates the CO<sub>2</sub> emission reduction of LNG-fuelled shipping  
169 on the NSR, based on its economic feasibility.

### 170 **3. Methodology**

171 In this section, we build models to estimate the shipping profit and CO<sub>2</sub> emission in a  
172 container vessel voyage. We define LN as “economically feasible” if it has the highest  
173 average voyage shipping profit (AVSP) among the three options.

#### 174 **3.1 Shipping profit model**

175 **3.1.1 Average voyage shipping profit**

176 The profit is defined as the difference between the revenue and the cost. The total  
177 shipping cost of a container ship comprises five components: fuel cost, capital cost,  
178 operating cost, container handling cost, and transit cost of passages (i.e. the Suez  
179 Canal toll or NSR icebreaking fee).

180 The fuel cost, which is determined by the bunker price, the voyage time, and the fuel  
181 consumption rate, is formulated as

$$182 \quad CFV_i = PF_i TS_i F_i,$$
$$183 \quad i = OS, ON, LN \tag{1}$$

184 where the subscript  $i$  denotes the options OS, ON, or LN hereinafter;  $CFV_i$  is the fuel  
185 cost in a voyage (US\$);  $PF_i$  is the bunker price (US\$/tonne);  $TS_i$  is the voyage time at  
186 sea (day); and  $F_i$  is the fuel consumption rate (tonne/day). The fuel consumption rate  
187 is usually considered to be proportional to the cubic of the ship speed (Psaraftis and  
188 Kontovas, 2013); thus,  $F_i$  is formulated as

$$189 \quad F_i = FMAX_i \frac{V_i^3}{VMAX_i^3} \tag{2}$$

190 where  $FMAX_i$  is the maximum fuel consumption rate of a ship sailing at its maximum  
191 speed (tonne/day),  $V_i$  is the ship speed (knot), and  $VMAX_i$  is the maximum (or design)  
192 speed of a ship (knot). The ship speed is determined by the voyage time at sea and the  
193 distance of the voyage:

194 
$$V_i = \frac{L_i}{24TS_i} \quad (3)$$

195 where  $L_i$  is the distance (nautical mile).

196 Substituting Equations (2) and (3) into Equation (1), we can obtain  $CFV_i$  as follows:

197 
$$CFV_i = \frac{PF_i FMAX_i L_i^3}{24^3 TS_i^2 VMAX_i^3} \quad (4)$$

198 The capital cost is the ship value depreciation and is determined by the new-building  
199 price of the ship and her lifetime. Otsuka *et al* (2013) suggested that the economic  
200 lifetime of a ship is 10 years, but the data from Shipping Intelligence Network shows  
201 that the average age at the demolition time of container ships is 20 years. In this study,  
202 we eclectically assume that the lifetime of a ship is 15 years. We adopt straight-line  
203 depreciation; thus, the annual depreciated value is 1/15 of the new-building price:

204 
$$CCY_i = \frac{CS_i}{15} \quad (5)$$

205 where  $CCY_i$  is the annual capital cost, and  $CS_i$  is the new-building price of a ship.

206 The operating cost includes repair and maintenance costs, insurance, administration  
207 costs, crew wages, and other miscellaneous costs. The estimation of the operating cost  
208 varies widely according to different sources, and Zhao *et al* (2016) suggested that it is  
209 as high as approximately 80% of the capital cost for a 4,800 TEU container ship.  
210 Zhang *et al* (2016a) suggested that this ratio is 56% for a 5,100 TEU ship. Tran and  
211 Haasis (2015) indicated that this ratio varies from 16% (for an 11,000 TEU ship) to

212 52% (for a 1,200 TEU ship). In this study, we adopt the average value of these studies  
213 and assume the operating cost to be 50% of the capital cost, as follows:

$$214 \quad COY_i = 0.5CCY_i \quad (6)$$

215 where  $COY_i$  is the annual operating cost. Because Arctic shipping requires more  
216 experienced and skilled seamen, more frequent inspection, and higher insurance, the  
217 operating costs of ice-class ships sailing the NSR are higher. We assume that the ratio  
218 of  $CCY_i$  to  $COY_i$  is identical between ice-class and ordinary ships.

219 Although the number of operating days is less than 365 because some days (often no  
220 more than 5 days) are usually spent on maintenance, the ship value depreciation and  
221 operating cost still incur during the maintenance days. Therefore, the sum of capital  
222 and operating costs for a voyage is

$$223 \quad CCV_i + COV_i = \frac{CCY_i + COY_i}{365} T = \frac{1.5CS_i}{15 \times 365} T \quad (7)$$

224 where  $CCV_i$  and  $COV_i$  are the voyage capital costs and operating costs, respectively;  
225 and  $T$  is the voyage transit time (day), which includes the times at sea ( $TS_i$ ) and at port.

226 All options have the same transit time to maintain the ship's schedule.

227 The container handling cost per voyage, denoted by  $CHV_i$ , is charged by ports. It is  
228 determined by the quantity of container transported  $Q_i$  (TEU) and the handling fee  
229 rate  $HR$  (US\$/TEU):

$$230 \quad CHV_i = 2Q_iHR \quad (8)$$

231 Each transported container is loaded once in the origin port and unloaded once in the  
 232 destination port; thus, it is handled twice in a voyage.  $Q_i$  is related to the ship capacity  
 233  $Z_i$  (TEU) and utilisation rate  $U_i$ :

$$234 \quad Q_i = U_i Z_i \quad (9)$$

235 The voyage transit cost of passages,  $CTV_i$ , is the NSR icebreaking fee if  $i$  is *ON* or  
 236 *LN*, or the Suez Canal toll if  $i$  is *OS* in each voyage. Notably, although Russia has  
 237 issued the maximum level of NSR tariffs, in practice, the actual NSR fees are  
 238 negotiated between shipowners and Atomflot (Russian nuclear icebreaker fleet), and  
 239 the Suez Canal toll is often quoted as a reference (Otsuka *et al*, 2013, Moe, 2014).

240 The voyage total shipping cost,  $CV_i$ , can then be determined by summing all of the  
 241 cost items, as follows:

$$242 \quad CV_i = CFV_i + CCV_i + COV_i + CHV_i + CTV_i$$

$$243 \quad = \frac{PF_i FMAX_i L_i^3}{24^3 TS_i^2 VMAX_i^3} + \frac{CS_i T}{3650} + 2U_i Z_i HR + CTV_i \quad (10)$$

244 The model is used to compare the AVSP (in US\$/TEU) of the three options. The  
 245 voyage shipping revenue,  $RV_i$ , is

$$246 \quad RV_i = Q_i FR = U_i Z_i FR \quad (11)$$

247 where  $FR$  is the freight rate (US\$/TEU).

248 The average voyage revenue and cost are obtained from ship capacity  $Z_i$ . The AVSP  
 249 of option  $i$  is denoted by  $APRV_i$  (US\$/TEU) and formulated as

$$\begin{aligned}
250 \quad APRV_i &= ARV_i - ACV_i = \frac{RV_i}{Z_i} - \frac{CV_i}{Z_i} \\
251 \quad &= U_i(FR - 2HR) - \left( \frac{PF_i FMAX_i L_i^3}{24^3 TS_i^2 VMAX_i^3} + \frac{CS_i T}{3650} + CTV_i \right) \frac{1}{Z_i} \\
252 \quad &= U_i(FR - 2HR) - \left( \frac{g_{1i} PF_i L_i^3}{24^3 TS_i^2} + \frac{g_{2i} T}{3650} + g_{3i} \right) \quad (12)
\end{aligned}$$

253 where  $ARV_i$  and  $ACV_i$  are the average voyage revenue and average voyage cost  
254 (US\$/TEU), respectively, and  $g_{1i}$ ,  $g_{2i}$ , and  $g_{3i}$  are the technological coefficients related  
255 to ship size:  $g_{1i} \equiv \frac{FMAX_i}{VMAX_i^3 Z_i}$ ,  $g_{2i} \equiv \frac{CS_i}{Z_i}$ ,  $g_{3i} \equiv \frac{CTV_i}{Z_i}$ .

### 256 **3.1.2 Bunker prices threshold**

257 The option LN is economically feasible only if the following two conditions are  
258 fulfilled:

$$259 \quad DIFF_1 \equiv APRV_{LN} - APRV_{ON} > 0 \quad (13)$$

$$260 \quad DIFF_2 \equiv APRV_{LN} - APRV_{OS} > 0 \quad (14)$$

261 where  $DIFF_1$  and  $DIFF_2$  are the differences of average voyage shipping profits  
262 (DAVSP) of LN over ON and OS, respectively. By substituting Equation (12) into  
263 (13) and (14), in turn, (13) and (14) can be transformed into

$$\begin{aligned}
264 \quad DIFF_1 &= (U_{LN} - U_{ON})(FR - 2HR) + \frac{1}{24^3} \left( \frac{g_{1ON} PF_{ON} L_{ON}^3}{TS_{ON}^2} - \frac{g_{1LN} PF_{LN} L_{LN}^3}{TS_{LN}^2} \right) + \\
265 \quad &\frac{(g_{2ON} - g_{2LN})T}{3650} + (g_{3ON} - g_{3LN}) > 0 \quad (15)
\end{aligned}$$

$$\begin{aligned}
266 \quad DIFF_2 &= (U_{LN} - U_{OS})(FR - 2HR) + \frac{1}{24^3} \left( \frac{g_{1OS} PF_{OS} L_{OS}^3}{TS_{OS}^2} - \frac{g_{1LN} PF_{LN} L_{LN}^3}{TS_{LN}^2} \right) + \frac{(g_{2OS} - g_{2LN})T}{3650} \\
267 \quad &+ (g_{3OS} - g_{3LN}) > 0 \quad (16)
\end{aligned}$$

268 We assume that the time at sea, the ship size and ice-class, and the quantity  
 269 transported are identical between options ON and LN, namely,  $U_{LN}=U_{ON}$ ,  $TS_{LN}=TS_{ON}$ ,  
 270  $Z_{LN}=Z_{ON}$ ,  $FMAX_{LN}=FMAX_{ON}$ ,  $VMAX_{LN}=VMAX_{ON}$ ,  $g_{1LN}=g_{1ON}$ , and  $g_{3LN}=g_{3ON}$ ,  
 271  $CTV_{LN}=CTV_{ON}$ . Because LNG is used in the option LN and oil is used in ON and OS,  
 272  $PF_{LN}$  can be renamed  $PF_L$ , and  $PF_{ON}=PF_{OS}$  can be renamed  $PF_O$ , where  $PF_O$  and  $PF_L$   
 273 represent the bunker prices of oil and LNG fuels, respectively. Thus Inequality (15)  
 274 can be simplified as

$$275 \quad PF_L < PF_{L1}^* \equiv a_1 PF_O - b_1 \quad (17)$$

$$276 \quad \text{where } a_1 \equiv \frac{I_{ON}^3}{L_{LN}^3} \text{ and } b_1 \equiv \frac{24^3 TS_{LN}^2 (g_{2LN} - g_{2ON}) T}{3650 g_{1LN} L_{LN}^3}.$$

277 Similarly, Inequality (16) can be changed into

$$278 \quad PF_L < PF_{L2}^* \equiv a_2 PF_O - b_2 \quad (18)$$

$$279 \quad \text{where } a_2 \equiv \frac{g_{1OS} TS_{LN}^2 L_{OS}^3}{g_{1LN} TS_{OS}^2 L_{LN}^3} \text{ and}$$

$$280 \quad b_2 \equiv \frac{24^3 TS_{LN}^2}{g_{1LN} L_{LN}^3} \left[ (U_{OS} - U_{LN})(FR - 2HR) + \frac{(g_{2LN} - g_{2OS})T}{3650} + (g_{3LN} - g_{3OS}) \right].$$

281  $PF_{L1}^*$  and  $PF_{L2}^*$  are the two thresholds of  $PF_L$  that enable LN to be more economical  
 282 than ON and OS, respectively. The LNG bunker price threshold  $PF_L^*$  is

$$283 \quad PF_L^* = \min(PF_{L1}^*, PF_{L2}^*) \quad (19)$$

284 If and only if  $PF_L < PF_L^*$ , LN is the economically feasible option.

285 By contrast, the threshold of oil bunker price can be formulated as a function with  
 286 respect to the ratio of LNG bunker price to oil bunker price, namely,  $d=PF_L/PF_O$ .



287 Given that the baseline of LNG bunker price is equal to the oil bunker price, the  
 288 discount of LNG bunker price is  $1-d$ . Inequalities (17) and (18) are transformed into

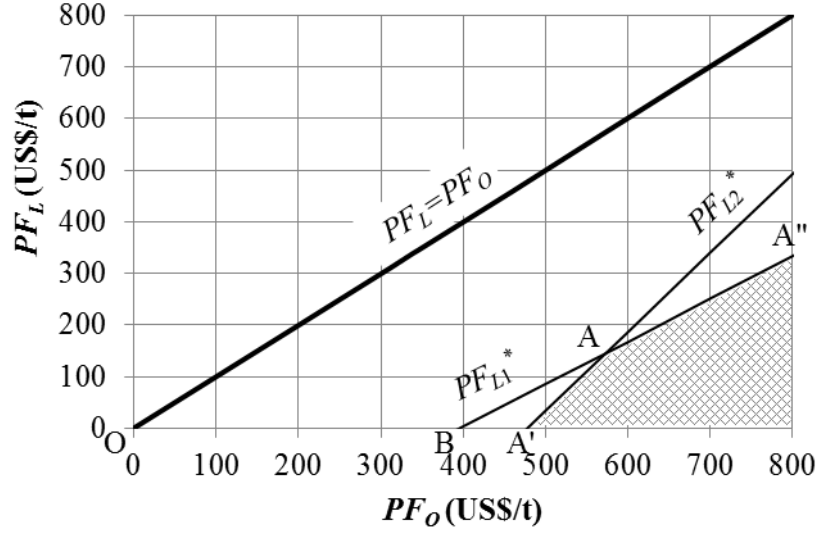
$$289 \quad PF_o > PF_{o1}^* \equiv \frac{b_1}{a_1-d} \quad (20)$$

$$290 \quad PF_o > PF_{o2}^* \equiv \frac{b_2}{a_2-d} \quad (21)$$

$$291 \quad PF_o^* = \max(PF_{o1}^*, PF_{o2}^*) \quad (22)$$

292 where  $PF_{o1}^*$  and  $PF_{o2}^*$  are the two thresholds of  $PF_o$  that enable LN to be more  
 293 economical than ON and OS, respectively, and  $PF_o^*$  is the oil bunker price threshold.  
 294 If and only if  $PF_o > PF_o^*$ , LN is economically feasible.

295 The thresholds of bunker prices are illustrated in Figure 2, where the horizontal axis  
 296 represents the bunker price of oil fuel and the vertical axis represents that of LNG fuel.  
 297 The lines representing  $PF_{L1}^*$  and  $PF_{L2}^*$  intersect at Point A. If LN is an economically  
 298 feasible option,  $PF_L$  should be lower than both of them, which is depicted as the grid  
 299 polygon in the figure, surrounded by the broken line A'AA'' ( $PF_L^*$ ) and the two axes.  
 300 The lengths of lines OB and OA' indicate the oil bunker price thresholds  $PF_{o1}^*$  and  
 301  $PF_{o2}^*$ , respectively, when the LNG bunker price is zero.



302

303 **Figure 2 Relations between LNG bunker price thresholds  $PF_{L1}^*$ ,  $PF_{L2}^*$ , and oil**  
 304 **bunker price  $PF_o$**

### 305 3.2 Emission model

306 The main types of gas emitted from a ship's combustion process are  $CO_2$ ,  $SO_x$ ,  $NO_x$ ,  
 307 and PM. The LNG-fuelled ship can reduce  $NO_x$  emissions by 85%–90% and can  
 308 nearly eliminate  $SO_x$  and PM emissions, compared to conventional fuel oil (IMO  
 309 report, 2016). By contrast, the reduction of  $CO_2$  is relatively minor and ranges  
 310 between 5% and 30% (Bouman *et al.*, 2017). Because LNG fuel has absolute  
 311 advantages over conventional fuel oil in  $NO_x$  and  $SO_x$  emissions, whereas the  
 312 reduction in  $CO_2$  is relatively modest, in this study, we only focus on the  $CO_2$   
 313 emission comparison among the three options.

314 The  $CO_2$  emission in option  $i$  is expressed as

$$315 \quad EM_i = EF_i \frac{FMAX_i L_i^3}{24^3 T S_i^2 V MAX_i^3} \quad (23)$$

316 where  $EM_i$  is the  $CO_2$  emissions per voyage (tonne), and  $EF_i$  is the  $CO_2$  emission  
 317 factor that indicates the tonnes of  $CO_2$  emitted from each tonne of fuel burnt in option

318 *i*. According to Peters *et al* (2011), the average CO<sub>2</sub> emission factor of residual fuel  
319 oil is 3.13; thus, we set  $EF_{ON}=EF_{OS}=3.13$ . DNV GL (2015) in its technology report  
320 "Focus - LNG as Ship Fuel" suggested that CO<sub>2</sub> emission per tonne of LNG fuel is set  
321 to be 20% lower than that of conventional oil fuel, which is close to the value  
322 suggested by Bouman *et al* (2017); thus, we set  $EF_{LN}=3.13*0.8=2.504$ . The fuel  
323 consumption rates of oil-fuelled and LNG-fuelled ships are assumed to be identical  
324 because DNV GL (2019) indicated that gas-fuelled engine systems have  
325 approximately the same efficiency as conventionally fuelled systems.

326 The average CO<sub>2</sub> emission per TEU in option *i* is therefore determined as follows:

$$327 \quad AEM_i = \frac{EM_i}{Z_i} = EF_i \frac{g_1 L_i^3}{24^3 TS_i^2} \quad (24)$$

328 The emission reduced by LN from OS is

$$329 \quad AEM_{OS} - AEM_{LN} = \frac{1}{24^3} \left( \frac{EF_{OS} g_1 OS L_{OS}^3}{TS_{OS}^2} - \frac{EF_{LN} g_1 LN L_{LN}^3}{TS_{LN}^2} \right) \quad (25)$$

330

#### 331 **4. Empirical Study**

332 In this section, we compare the shipping profits and CO<sub>2</sub> emissions among three  
333 options (LN, ON, and OS) by applying the real data of sample ships, distances  
334 between ports, and fuel prices to the profit and emission models.

335 To achieve this goal, we must first propose assumptions and scenarios by considering  
336 the variation of factors, to reflect the different circumstances in the real world. Then,  
337 we discuss the economic feasibility of LN, and its potential in reducing CO<sub>2</sub> emission.

#### 338 **4.1 Assumptions**

339 We provide the assumptions of this study as follows:

340 (1) Because of the economies of scale in ship size, container operators always employ  
341 the largest ships on the SCR; thus, we assume that the largest ships are always used  
342 on the SCR. For the two NSR options, we assume that the same ship sizes are  
343 employed, and the size is optimised in this empirical study to maximise the DAVSP  
344 of LN over OS,  $DIFF_2$ , under the cases that LN is economically feasible.

345 (2) In this study, the compared NSR voyages are assumed to be conducted in the  
346 ice-free season when the Arctic sea ice extent is minimal (approximately from late  
347 August to early October). According to recent Arctic sea ice charts from the National  
348 Snow and Ice Data Center, it is common that the entire NSR is ice-free during this  
349 season.

350 (3) Ice-class 1A (Finnish-Swedish Ice Class Rules) or ARC4 (Russian Maritime  
351 Register of Shipping, Rules 2007) ships are assumed to be deployed in two NSR  
352 options. This ice-class level is the most widely used in Arctic or sub-Arctic  
353 ice-infected waters. Compared to ordinary ships, ice-class ships consume more fuel in  
354 open water, and the ice-strengthened measures cost more to build; thus, we compare

355 the fuel consumption rates and new-building prices between ice-class 1A (or ARC4)  
356 ships and their ordinary peer ships. By regressing the data from the Shipping  
357 Intelligence Network, we find that the ratio of fuel consumption rate of oil-fuelled 1A  
358 ships to that of ordinary ships ( $FMAX_{ON}/FMAX_{OS}$ ) is 1.106, and the ratio of  
359 new-building prices of these two ship types ( $CS_{ON}/CS_{OS}$ ) is 1.123. Erikstad and Ehlers  
360 (2012) suggested that the capital cost of a 1A ship is 9.5% higher than that of an  
361 ordinary ship, which is close to our result. Therefore, we set these two ratios to 1.1 in  
362 this study.

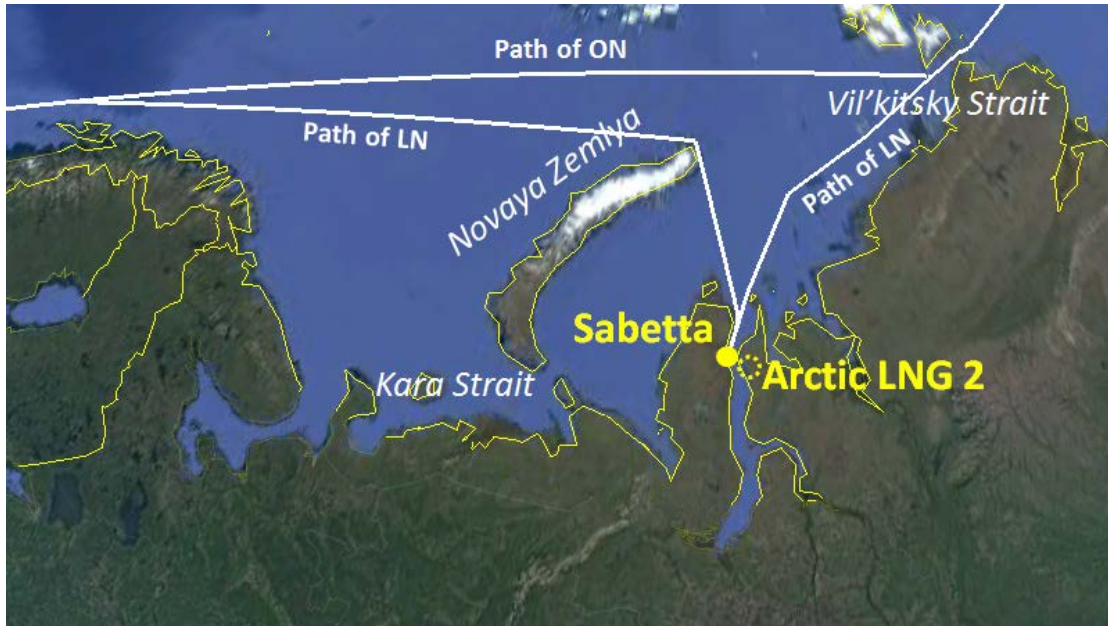
363 (4) According to *Rules of navigation in the water area of the Northern Sea Route*  
364 issued by Russia in 2013, ARC4 ships can independently sail the NSR from July to  
365 November if there is no ice or the ice condition is light. Therefore, we assume that the  
366 ice-class ships sail the NSR without icebreaker escorting during the ice-free season  
367 and the NSR icebreaking fee is null:  $CVT_{LN}=CVT_{ON}=0$ .

368 (5) The price of conventional oil fuel is based on the average cost of marine gas oil  
369 (MGO) and 380 cst fuel oil in Singapore, and this is close to the Northeast  
370 Asia-delivered LNG price; thus, we set  $PF_L=PF_O$  as the no discount baseline in our  
371 theoretical analysis framework. However, according to the Clipper Data daily LNG  
372 report in July and August 2018, the FOB LNG price from Yamal LNG at Sabetta,  
373 which is anticipated as the LNG refuelling location on the NSR, is approximately 80%  
374 of the Northeast Asia-delivered LNG price. Therefore, we set the base level of the

375 FOB Yamal LNG bunker price to be 80% of the oil fuel price in the empirical  
376 analysis in Section 4.3.

377 (6) Compared to a peer oil-fuelled ship, an LNG-fuelled ship has a more sophisticated  
378 design, which induces higher costs. The capital and operation costs for LNG-fuelled  
379 ships vary widely for different ship types. However, recent advancements in relevant  
380 technologies have made them cheaper. In May 2017, Sovcomflot (a Russian shipping  
381 company) ordered four LNG-fuelled 114,000 deadweight tankers at US\$60 million  
382 each; they were 27% more expensive than peer oil-fuelled ships. In a Bloomberg  
383 interview with DNV GL, LNG-fuelled ships were said to be 10%–25% more  
384 expensive than comparable vessels running on fuel oil (Bloomberg, 2015). An earlier  
385 report from Wärtsilä, a main marine engine manufacturer, suggested that the sum of  
386 the annual capital, lubrication oil, maintenance, and selective catalytic reduction  
387 system operation costs (conventional ships only) of an LNG-fuelled ship is  
388 approximately 15% higher than that of a conventional ship using MGO as fuel  
389 (Wärtsilä, 2011). Exact data on the capital and operating costs of LNG-fuelled ships  
390 remain very scarce. Considering all the aforementioned sources, in this study, we  
391 assume that the capital and operating costs of an LNG-fuelled ship are both 20%  
392 higher than those of a conventional ship, namely,  $g_{2LN}=1.2g_{2ON}$ .

393 (7) We assume that in LN, the ship will travel north of Novaya Zemlya because of the  
394 shorter distance to European ports. The location of Sabetta and the paths are presented  
395 in Figure 3.



396

**Figure 3 NSR paths near Sabetta**

397

Source: edited Google Earth screenshot

398

399 (8) Two port ranges are considered: the East Asian port range and the Northwest  
 400 European port range. We assume that the former range stretches from Yokohama in  
 401 the north to Hong Kong in the south, and the latter range stretches from Hamburg in  
 402 the north to Le Havre in the south. The container services of both routes are  
 403 considered a “multi-port calling” service, which indicates a series of ports are called  
 404 during the voyage. We use the longest distances between the pair of ports in each port  
 405 range as the distances of three options. The distances are measured on Google Earth:  
 406  $L_{OS}=11526$  nautical miles (between Yokohama and Hamburg),  $L_{ON}=8499$  nautical  
 407 miles (between Hong Kong and Le Havre), and  $L_{LN}=9038$  nautical miles (also  
 408 between Hong Kong and Le Havre but with calling at Sabetta). Moreover, referring to  
 409 the current Asia–Europe container services of several main liner operators (including

410 Maersk, MSC, CMA CGM, and COSCO), we find that on average, five ports are  
411 called on a one-way voyage within each range.

412 (9) Although the NSR shortens the distance considerably, the lack of intermediate  
413 ports may lead to the loss of revenue. If an Asia–Europe container service shifts from  
414 the SCR to the NSR, the cargos between Southeast Asia and Northwest Europe will  
415 be skipped. By analysing the bilateral trade data of SITC Category 5-9 commodities  
416 (roughly equivalent to manufactures) in 2018 from UN Comtrade Database, we find  
417 that Southeast Asia–Northwest Europe trade accounts for approximately 15% of Far  
418 East (East and Southeast Asia)–Northwest Europe trade. Therefore, we set both  
419 capacity utilisation rates  $U_{LN}$  and  $U_{ON}$  to be 15% lower than  $U_{OS}$ .

420 (10) Based on Shanghai Containerized Freight Index, the average monthly freight rate  
421 from Shanghai to Europe in 2016–2018 is 793.2 US\$/TEU; thus, we set the  
422 westbound freight rate of the Asia–Europe lane to be 800 US\$/TEU. Referring to the  
423 bilateral freight rate data from Sea & Air Shipper Insight (published by Drewry) and  
424 the container trade data from Shipping Review and Outlook (published by Clarksons),  
425 the ratio of freight rates between two directions is approximately the same as that of  
426 container trade volume. As in 2016–2019, the eastbound container trade volume of  
427 this lane is roughly half of the westbound, and the eastbound freight rate is set to 400  
428 US\$/TEU. The ratio of the westbound to eastbound capacity utility rate of an Asia–  
429 Europe container service is 1:0.5.



430 (11) The container handling fee is assumed to be 100 US\$/TEU, as suggested by  
431 Furuichi and Otsuka (2014).

## 432 **4.2 Scenarios**

433 In addition to the aforementioned assumptions, we propose several scenarios by  
434 considering the changes of two important factors: ship size and round-trip transit time  
435 of a service. The ship size determines many other parameters, for example, maximum  
436 ship speed, maximum fuel consumption rate, and new-building price. The round-trip  
437 transit time of a service is twice as long as the transit time per one-way voyage,  $T_i$ .

438 (1) Seven container ship size levels are considered on the NSR: 4000, 6000, 8000,  
439 10000, 12000, 14000, and 16000 TEU. The technical parameters of sample ships are  
440 listed in Table 1. On the SCR, only 16,000 TEU ships are assumed to be used, which  
441 is close to the average ship size employed on this lane currently. Most Arctic studies  
442 assume that sizes of container ships sailing the NSR are smaller than 5,000 TEU (e.g.  
443 3,800 TEU by Omre [2012], 4,000 TEU by Verny and Grigentin [2009] and Furuichi  
444 and Otsuka [2014], 4,300 TEU by Liu and Kronbak [2010], 4,500 TEU by Lasserre  
445 [2014], and 4,800 TEU by Zhao *et al* [2016]). This is because these studies have  
446 assumed that the ships pass a coastal route through shallow water in the Sannikov  
447 Strait (13 m deep). In this study, the NSR route is assumed to be north of the New  
448 Siberian Islands because of the minimal ice condition in the ice-free season; thus, the  
449 Sannikov Strait is bypassed, and larger ships can be used.

**Table 1 Scenarios of container ship size and their properties**

Ship size (TEU capacity)	4000	6000	8000	10000	12000	14000	16000
Sample ship	Xin Nan Sha	E.R. France	OOCL Ningbo	COSCO Kaohsiung	MSC Ivana	MSC Alexandra	CMA CGM Marco Polo
Max speed (kt)*	24.5	26	26	25	24	24.1	24.1
Max fuel consumption rate (t/d) *	133	200	248	250	250	262.2	288
New-building price adjusted to 2015 (million US\$) *	44	60	79	96	110	130	147
Gross tonnage (t) *	41482	66289	89097	115776	131771	153115	175343
Suez Canal toll (million US\$) **	0.240	0.335	0.406	0.487	0.533	0.594	0.658
$g_{10s}$ ( $10^{-6}$ )	2.261	1.897	1.764	1.600	1.507	1.338	1.286
$g_{20s}$	11000	10000	9875	9600	9167	9286	9188
$g_{30s}$	60.0	55.8	50.8	48.7	44.4	42.5	41.1
$g_{20s}/g_{10s}$ ( $10^{-6}$ )	4865.2	5272.8	5598.8	6000.0	6082.6	6940.0	7144.6

451 Source: \* Shipping Intelligence Network; \*\* Based on canal tariffs issued by Suez Canal Authority.

452 (2) Three round-trip transit times are set as 84, 77, and 70 days. The most common  
453 round-trip transit time of an Asia–Europe service is 84 days with  $84/7=12$  ships  
454 deployed. Services with a 77- or 70-day round trip also exist, and they require 11 or  
455 10 ships, respectively. In this study, we assume the voyage transit time  $T$  under the  
456 three scenarios is 42, 38.5, and 35 days, respectively. By investigating the major liner  
457 operators, we find that a typical Asian-Europe service has 10 port-calls in East Asia  
458 and Northwest Europe, and four port-calls in the middle (e.g. Singapore); thus, the  
459 port-call total is 14. Each call takes on average approximately 1 day at port; thus,  
460  $TS_{OS}=T-7$ . Because no commercial port exists along the NSR,  $TS_{ON}=TS_{LN}=T-5$ .

461 According to the assumptions, DAVSP in Inequalities (15) and (16) can then be  
 462 numerically expressed as

$$463 \quad DIFF_1 = \frac{(4.4409PF_0 - 5.3405PFL) * 10^7 g_{1ON}}{(T-5)^2} - 5.4795 * 10^{-5} g_{2ON} T \quad (26)$$

$$464 \quad DIFF_2 = -11.366 + \left( \frac{142.4372PF_0}{(T-7)^2} - \frac{5.3405 * 10^7 g_{1LN} PFL}{(T-5)^2} \right) + 2.7397 * 10^{-4} (9187.5 -$$

$$465 \quad g_{2LN}) T \quad (27)$$

### 466 **4.3 Result discussion**

467 Based on the assumptions and scenarios, our comparison of the three options is  
 468 presented in this section. First, we discuss the impacts of round-trip transit time and  
 469 NSR ship size on the results of DAVSP and bunker price thresholds, to understand  
 470 how the results change under different scenarios. Second, we analyse the economic  
 471 feasibility of LN. Finally, the CO<sub>2</sub> emission reduction is calculated.

#### 472 ***4.3.1 Impacts of round-trip transit time and NSR ship size***

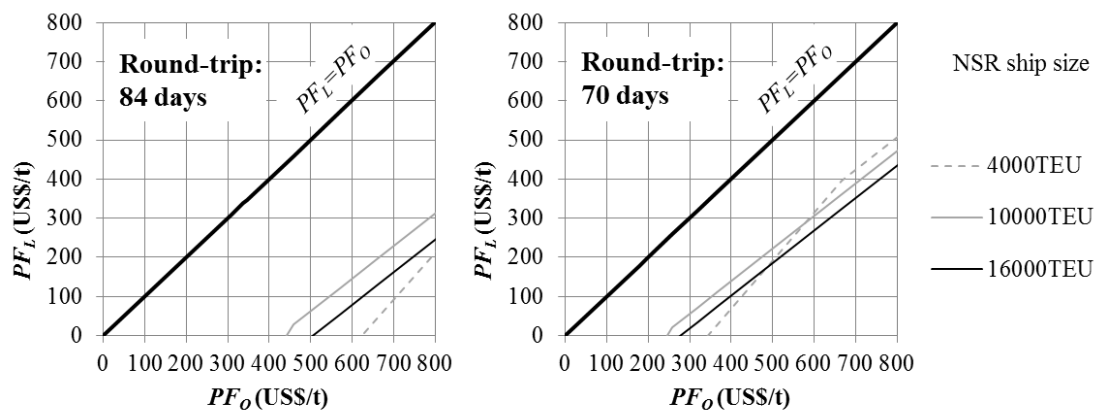
473 The round-trip transit time, twice as long as the voyage transit time  $T$ , affects the  
 474 LNG bunker price thresholds  $PF_{L1}^*$  and  $PF_{L2}^*$ . According to Inequalities (17) and (18),  
 475  $T$  changes in the same direction as  $b_1$  and  $b_2$ , and opposite direction against  $a_2$ . A  
 476 larger  $T$  will thus lead to a smaller  $PF_{L1}^*$  or  $PF_{L2}^*$ . This indicates that for a longer  
 477 round trip, a larger extent of LNG bunker price discount is necessary to make LN  
 478 economically feasible.

479 The transit time also affects the DAVSP. Based on Inequalities (15) and (16),  
 480  $PF_{OLON^3} - PF_{LLLN^3} > 0$  is a necessary condition for  $DIFF_1 > 0$ . Under this condition, a  
 481 larger  $T$  always leads to a larger  $TS_{ON}$  or  $TS_{LN}$ , leading to a lower  $DIFF_1$ . Similarly, a  
 482 larger  $T$  can also lead to a lower  $DIFF_2$ . This means that when slow steaming is  
 483 adopted, a longer round-trip transit time will make LNG-fuelled container shipping on  
 484 the NSR less likely to be economically feasible.

485 The NSR ship size affects the thresholds of bunker prices and the feasibility of LN  
 486 indirectly through technological coefficients  $g_{1i}$  and  $g_{2i}$ . Table 1 shows that  $g_{1i}$  and  $g_{2i}$   
 487 both decline with an increase of the ship size, except that  $g_{2i}$  is the lowest at  $Z_i = 12,000$   
 488 TEU. By contrast, the ratio  $g_{2i}/g_{1i}$  changes in the same direction as the ship size. From  
 489 Inequalities (17) and (18), we observe that the decreasing of NSR ship size will lower  
 490  $b_1$  and thus increase the threshold  $PF_{L1}^*$ ; the decreasing of NSR ship size will lower  
 491  $a_2$ , and thus decrease the slope of the curve of  $PF_{L2}^*$ ; however, the effect on  $b_2$  is  
 492 undetermined. Therefore, the composite effect of NSR ship size on the threshold of  
 493 LNG bunker price  $PF_L^*$  is also undetermined.

494 The impact of NSR ship size on DAVSP can be observed from Equations (26) and  
 495 (27). If  $DIFF_1 > 0$ , when NSR ship size decreases,  $g_{1ON}$  will increase but  $g_{2ON}/g_{1ON}$  will  
 496 decrease; thus,  $DIFF_1$  will increase. This suggests that a smaller ship size on the NSR  
 497 can enlarge the profit advantage of LNG-fuelled ships over oil-fuelled ships. However,  
 498 a smaller ship size will lead to larger  $g_{1LN}$  and  $g_{2LN}$  (except at  $Z_i = 12,000$  TEU) and  
 499 make  $DIFF_2$  decline, which shrinks the profit advantage of LN over OS.

500 Consequently, a trade-off exists among the three options: deploying smaller ships to  
 501 make LNG-fuelled shipping more economical than oil-fuelled shipping on the NSR,  
 502 or deploying larger ships to make the NSR more economical than the SCR. This  
 503 trade-off is illustrated in Figure 4, which shows the thresholds  $PF_L^*$  under two  
 504 round-trip transit times (84 and 70 days) and three NSR ship sizes (4000, 10000, and  
 505 16000 TEU). The lower-right areas beneath the thin lines indicate the economically  
 506 feasible spaces of bunker prices for LN under the corresponding ship sizes. In the left  
 507 panel, the line of 10,000 TEU has a larger feasible space than that of 4,000 or 16,000  
 508 TEU; thus, 10,000 TEU is more economical than 4,000 and 16,000 TEU in this case.  
 509 This implies that an optimal NSR ship size exists, and it varies with the round-trip  
 510 transit time and bunker prices.



511

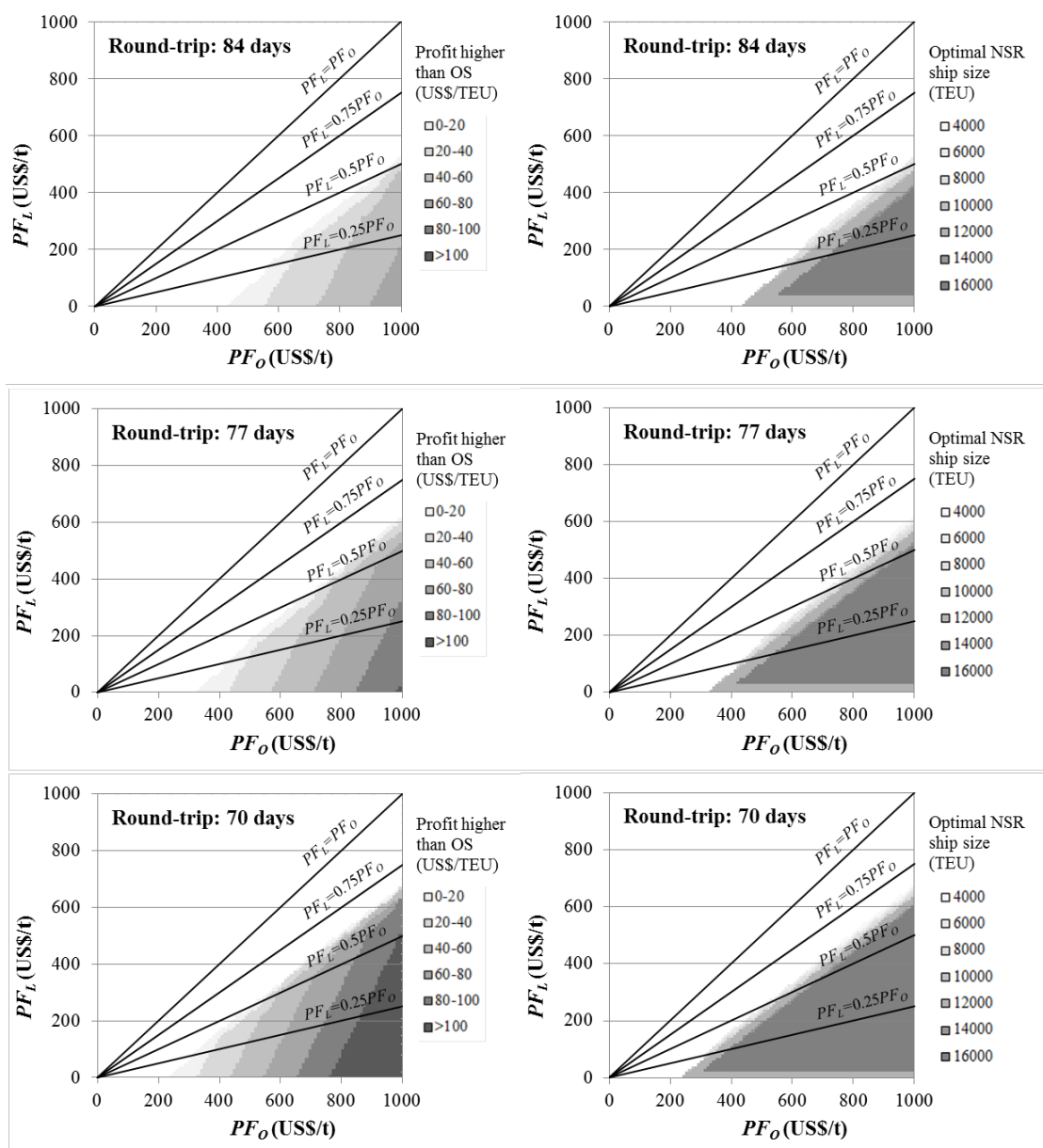
512 **Figure 4 LNG bunker price threshold  $PF_L^*$  under 3 NSR ship sizes and 2**  
 513 **round-trip transit times**

514 **4.3.2 Economic feasibility of LN**

515 In Figure 5, we plot the optimal NSR ship size and the corresponding DAVSP of LN  
 516 over OS ( $DIFF_2$ ) and under that ship size. This figure considers all three round-trip

517 transit times. The black lines reflect different values of  $d$  (ratio of LNG bunker price  
518 to oil bunker price). In the left three panels, the grey areas indicate the positive  
519 DAVSP, or called “feasible spaces” of LN; the white areas are “infeasible spaces” of  
520 LN. From the grey areas traversed by the black lines, we can understand the DAVSP  
521 under different oil bunker prices and LNG bunker price discounts. Similarly, in the  
522 right three panels, the grey areas indicate the optimal NSR ship sizes.

523 The left-side panels of Figure 5 imply that a shorter round-trip transit time will lead to  
524 a higher profit of LN. Given that the other conditions are unchanged, in the feasible  
525 space, a higher oil bunker price is always favourable for LN. The LNG bunker price  
526 threshold  $PF_L^*$  (represented by the borderline between feasible and infeasible areas) is  
527 closely related to the oil bunker price  $PF_O$ : a higher  $PF_O$  will lower the discount  
528 threshold  $PF_L^*$ . For example, for the 70-day round trip, when  $PF_O=400$  US\$/t, a  
529 discount no less than 59.4% ( $d=40.6\%$ ) is necessary to ensure the economic feasibility  
530 of LN, and when  $PF_O=800$  US\$/t, the discount threshold decreases to 36.5%  
531 ( $d=63.5\%$ ).



532

533 **Figure 5 Difference of AVSP of LN over OS and corresponding optimal NSR**  
 534 **ship size**

535 From each panel on the right side in Figure 5, the darkest grey triangle area indicates  
 536 that deploying the largest ships (16,000 TEU) on the NSR is the best choice under the  
 537 corresponding combination of two bunker prices  $PF_L$  and  $PF_O$ . In the lighter grey area  
 538 surrounding the darkest triangle, a smaller NSR ship size is optimal. This finding  
 539 reflects the trade-off of ship size choice in LN against OS and ON, simultaneously

540 depicted in Section 4.3.1. This lighter grey area becomes narrower when the  
541 round-trip transit time decreases, implying that larger LNG-fuelled ships with a short  
542 transit time are preferred on the NSR.

543 The points on the borderline between feasible space (grey area) and infeasible space  
544 (white area) in Figure 5, which indicate the threshold of bunker prices ( $PF_L^*$  or  $PF_O^*$ ),  
545 can be calculated from Inequalities (17)–(22). We define  $d^*=PF_L^*/PF_O^*$  to be the  
546 threshold of bunker price ratio  $d$ . LN can be economically feasible below  $d^*$ .  $d^*$  and  
547 its corresponding optimal NSR ship sizes are listed in Table 2. The oil bunker price  
548 higher than 800 US\$/t is excluded because this price is much higher than the  
549 reasonable range in reality. These points imply the feasible thresholds of bunker  
550 prices for the option LN. For example, in an 84-day round trip, to make LN  
551 economically feasible, when the oil bunker price is 600 US\$/t, the discount of LNG  
552 bunker price should not be lower than 71.9% ( $d=28.1\%$ ), which is unreasonably high;  
553 if the discount declines to 60% ( $d=40\%$ ), the oil bunker price should be higher than  
554 721 US\$/t, which is also much higher than the recent practical oil bunker price. In  
555 summary, for a container service with a round-trip of 84 days, it is generally  
556 uneconomical to deploy LNG-fuelled ships on the NSR. Nevertheless, for a shorter  
557 round trip, for example, of 70 or 77 days, the option LN is more likely to be feasible.

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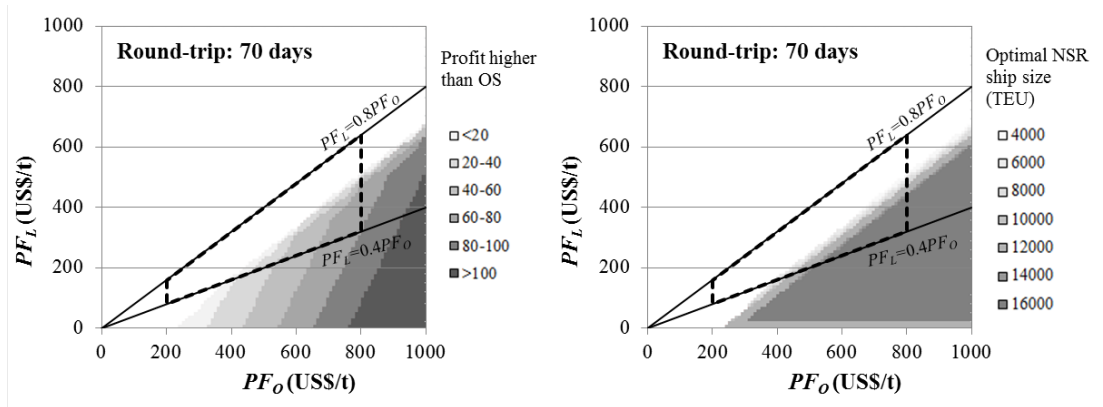
560  
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**Table 2 Threshold of bunker price ratio and corresponding optimal NSR ship size**

84-day round trip ( $T=42$ )			77-day round trip ( $T=38.5$ )			70-day round trip ( $T=35$ )		
$PF_o$ (US\$/t)	$d^*$ (%)	Optimal NSR ship size (TEU)	$PF_o$ (US\$/t)	$d^*$ (%)	Optimal NSR ship size (TEU)	$PF_o$ (US\$/t)	$d^*$ (%)	Optimal NSR ship size (TEU)
432	0.0	12000	324	0.0	12000	236	0.0	12000
484	10.0	10000	364	10.0	10000	265	10.0	10000
500	12.4	10000	400	16.7	10000	300	18.5	10000
550	20.0	8000	416	20.0	8000	307	20.0	10000
600	28.1	8000	467	30.0	8000	340	30.0	8000
621	30.0	8000	500	36.4	6000	395	40.0	6000
700	38.7	6000	542	40.0	6000	400	40.6	6000
721	40.0	6000	600	44.2	6000	500	49.1	6000
800	44.3	6000	700	49.8	6000	514	50.0	6000
			705	50.0	6000	600	54.8	6000
			800	53.9	6000	679	60.0	4000
						700	60.7	4000
						800	63.5	4000

562 As mentioned in Assumption (5), the FOB price of the Yamal LNG price is 20%  
563 lower than the oil fuel price, which means the baseline of the FOB Yamal LNG price  
564 is  $d=0.8$ . Due to the new project of Arctic LNG 2 under construction, the LNG price  
565 in this region is expected to decrease further. If the future FOB Yamal LNG price  
566 decreases to half of its recent level, then  $d$  will decrease to 0.4. The monthly average  
567 value of the MGO and 380 cst fuel oil prices in the last decade fluctuated between 200  
568 and 800 US\$/t. In Figure 6, we plot the DAVSP and optimal NSR ship size within the  
569 practical ranges of  $PF_o$  (200–800 US\$/t) and  $d$  (0.4–0.8) for a 70-day round-trip,  
570 indicated by the area surrounded by the dashed line. We find observe that the

571 economically feasible space of LN (grey area) within the practical ranges is very  
 572 limited.



573

574 **Figure 6 Difference in AVSP of LN over OS and corresponding optimal NSR**  
 575 **ship size under practical oil bunker price and LNG bunker price discount for a**  
 576 **70-day round trip**

577 In Table 3, we list the results of the DAVSP and optimal NSR ship size within the  
 578 practical space depicted in Figure 6. The percentage by which the AVSP of LN is  
 579 higher than that of OS is also calculated. We find that with the recent oil bunker price  
 580 fluctuating approximately 400 US\$/t, the only feasible scenario for LN is a 70-day  
 581 round-trip service with the LNG bunker price as 50% of the recent FOB Yamal LNG  
 582 price ( $d=0.4$ ), and the DAVSP of LN over OS is 3 US\$/TEU, or 2%, which is  
 583 marginal.

584

585

586

587

588 **Table 3 Difference in AVSP and optimal NSR ship size of LN under practical oil**  
589 **bunker price and LNG bunker price discount**

Round- trip (day)	$d$ (%)	Profit of LN higher than OS (US\$/TEU)					Optimal NSR ship size (TEU)					
		Oil bunker price $PF_O$ (US\$/t)					Oil bunker price $PF_O$ (US\$/t)					
		400	500	600	700	800	400	500	600	700	800	
84	40	-	-	-	-	13.2	-	-	-	-	8000	
						(12.0)						
77	40	-	-	12.0	36.3	50.9	-	-	8000	12000	16000	
				(9.6)	(32.6)	(52.4)						
	45	-	-	-	26.0	44.4	-	-	-	10000	12000	
					(23.3)	(45.7)						
	50	-	-	-	-	26.0	-	-	-	-	8000	
						(26.7)						
70	40	3.0	31.9	49.3	64.1	78.9	6000	12000	16000	16000	16000	
		(2.0)	(24.5)	(44.1)	(68.5)	(104.6)						
	45	-	16.7	44.6	61.2	75.6	-	8000	14000	16000	16000	
			(12.8)	(39.9)	(65.4)	(100.2)						
	50	-	-	40.2	58.2	72.2	-	-	12000	16000	16000	
				(36.0)	(62.2)	(95.7)						
	55	-	-	-	50.0	66.1	-	-	-	12000	14000	
					(53.4)	(87.7)						
	60	-	-	-	2.7	41.8	-	-	-	4000	8000	
					(2.9)	(55.5)						

590 Note: Numbers in brackets are the percentages of the profit of LN higher than OS.

### 591 4.3.3 CO<sub>2</sub> emission reduction of LN

592 Finally, we investigate the CO<sub>2</sub> emission reduction of the option LN compared to OS,  
593 based on Equation (25), and find that the CO<sub>2</sub> emission reduction depends on the  
594 distance, ship size, and transit time (ship speed). The bunker prices  $PF_O$  and  $PF_L$  also  
595 affect CO<sub>2</sub> emission but are through their relations to the optimal NSR ship size: At  
596 each combination of  $PF_O$  and  $PF_L$  in the feasible space in Figure 5, an optimal NSR  
597 ship size exists, which also determines the CO<sub>2</sub> emission reduction. We calculate the  
598 CO<sub>2</sub> emission reduction under each scenario and list the results in Table 4.

**Table 4 CO<sub>2</sub> emission reduction of LN compared to OS for NSR ship sizes**

NSR ship size (TEU)	84-day round trip (T=42)		77-day round trip (T=38.5)		70-day round trip (T=35)	
	CO <sub>2</sub> emission reduction (t/TEU)	As %	CO <sub>2</sub> emission reduction (t/TEU)	As %	CO <sub>2</sub> emission reduction (t/TEU)	As %
4000	0.121	33.2	0.153	34.0	0.199	35.0
6000	0.160	44.0	0.201	44.7	0.259	45.5
8000	0.174	47.9	0.218	48.5	0.280	49.3
10000	0.192	52.8	0.240	53.3	0.307	54.0
12000	0.202	55.5	0.252	56.0	0.322	56.7
14000	0.220	60.5	0.274	61.0	0.350	61.5
16000	0.226	62.0	0.281	62.5	0.358	63.0

600 We also calculate the practical CO<sub>2</sub> emission reduction based on the feasible cases by  
601 considering the practical range of oil bunker price and LNG bunker price discount.  
602 The results are listed in Table 5.

603 **Table 5 CO<sub>2</sub> emission reduction of LN compared to OS under practical oil**  
604 **bunker price and LNG bunker price discount**

Round -trip (day)	d (%)	CO <sub>2</sub> emission reduction (t/TEU)					As percentage of OS (%)				
		Oil bunker price $PF_o$ (US\$/t)					Oil bunker price $PF_o$ (US\$/t)				
		400	500	600	700	800	400	500	600	700	800
84	40	-	-	-	-	0.174	-	-	-	-	47.9
77	40	-	-	0.218	0.252	0.281	-	-	48.5	56.0	62.5
	45	-	-	-	0.240	0.252	-	-	-	53.3	56.0
	50	-	-	-	-	0.218	-	-	-	-	48.5
70	40	0.259	0.322	0.358	0.358	0.358	45.5	56.7	63.0	63.0	63.0
	45	-	0.280	0.350	0.358	0.358	-	49.3	61.5	63.0	63.0
	50	-	-	0.322	0.358	0.358	-	-	56.7	63.0	63.0
	55	-	-	-	0.322	0.350	-	-	-	56.7	61.5
60	-	-	-	0.199	0.280	-	-	-	35.0	49.3	

605 In summary, for a 70-day round-trip service, CO<sub>2</sub> emission per TEU can be reduced  
606 by more than 0.3 tonnes, when the NSR ship size is larger than 10,000 TEU. However,  
607 on a 77-day round-trip service, the emission reduction per TEU is between 0.2 and 0.3

608 tonnes. If the round-trip time is 84 days, such as those of most current Asia–Europe  
609 container services, the emission reduction will be less than 0.2 tonne per TEU, at the  
610 highest practical oil bunker price.

## 611 **5. Conclusion**

612 This study discusses the economic feasibility and potential CO<sub>2</sub> emission reduction  
613 for a container service using LNG-fuelled ships on the NSR (named “LN”),  
614 benchmarking oil-fuelled shipping on the SCR (named “OS”), or on the NSR (named  
615 “ON”). We assume that Sabetta, the gate-port of Yamal LNG, can be developed into  
616 an LNG refuelling centre. The option LN is economically feasible only if it has the  
617 highest AVSP among the three options.

618 We establish a profit model for estimating the shipping profit of a container service,  
619 and an emission model for calculating CO<sub>2</sub> emission. The real data of the ships, route  
620 information, and bunker prices are collected and applied to the models. To address the  
621 complexities in reality, multiple scenarios are proposed and analysed by considering  
622 variations in the factors, including seven levels of ship sizes deployed on the NSR,  
623 and three levels of the length of round-trip times. The results of this empirical study  
624 reveal the following findings:

625 (1) Smaller ships make LN more advantageous over ON by curbing the capital and  
626 operating costs but make it more disadvantageous against OS, in which economies of

627 scale in ship size are achieved by larger ships. Given round-trip transit time and  
628 bunker prices, an optimal ship size for the option LN exists.

629 (2) A shorter round-trip transit time can make the option LN more economically  
630 feasible because a shorter round-trip transit time is in line with a faster ship speed that  
631 substantially increases the fuel consumption. In addition, it leads to lower capital and  
632 operating costs because of shorter voyage times. For LN, its advantage in fuel cost  
633 offsets its loss in capital and operating cost.

634 (3) In the current circumstance, the option LN is hardly economically feasible, unless  
635 the round-trip transit time is 70 days. The additional cost of an LNG-fuelled ship and  
636 the detour to the proposed Sabetta LNG refuelling centre make this option less  
637 competitive.

638 (4) LN can reduce CO<sub>2</sub> emission significantly against OS. Practically, the option LN  
639 can reduce CO<sub>2</sub> emission by 0.174 to 0.358 tonne per TEU (or 45.5%–63%) against  
640 OS when it is economically feasible.

641 Although the economic feasibility of LN is not promising under the current situation,  
642 the environmental improvement is significant. CO<sub>2</sub> emissions can be reduced  
643 considerably as long as LN is economically feasible, NO<sub>x</sub> emissions can be reduced  
644 85%–90%, and SO<sub>x</sub> and PM emissions can be nearly eliminated. We also observe that  
645 the just-enacted sulphur control regulation may lead to a more prevailing use of  
646 very-low sulphur fuel oil (approximately 50%–80% more expensive than 380 cst fuel

647 oil), and the new project in Yamal region may lead to a cheaper price of LNG (or 30%  
648 lower than current level). With the joint effect of the potential increase in oil bunker  
649 price and decrease in LNG bunker price, LNG-fuelled container shipping on the NSR  
650 may—in the future—become much more economically feasible.

651 The contribution of this study is that we assess environmental impact based on an  
652 economic feasibility analysis of a clean energy application in Arctic shipping, because  
653 the connection has been ignored in the literature. We hope it can provide insights for  
654 further research on green shipping in this region.

655 Notably, this study has limitations. The main limitation is that the environmental  
656 consequences of various emissions on the Arctic or other regions are not analysed.  
657 For example, the Arctic is extremely vulnerable to black carbon. This analysis is  
658 beyond the scope of this study but will be included in our further research. In addition,  
659 we will also consider more greenhouse gases and pollutants and their impacts on the  
660 Arctic environment (especially the warming effect from black carbon), the influence  
661 of the sulphur limit regulation enacted in 2020, the development of technologies such  
662 as more new types of engines and energies, and supply chains of these energies in  
663 Arctic shipping.

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