

19 **Abstract**

20 The construction industry around the globe is facing a massive predicament of work-related musculoskeletal
21 disorders (MSDs), largely attributed to the excessive physical exertion at worksites. While ergonomic interventions
22 are suggested to be an effective approach to mitigate such routine exertion, these ergonomic interventions should be
23 task specific given the unique characteristics of each trade (such as rebar work; a construction trade with a high
24 prevalence rate of MSDs). Despite numerous potential interventions available for rebar workers, none of them have
25 been widely adopted, especially in the Asian market. After considering various reasons impeding their broad usage,
26 the authors coined a simple ergonomic solution by attaching a low height domestic stool to the pants of rebar
27 workers. This would allow them to sit and work instead of squatting, which is the most preferred posture in Asian
28 cultures for working at ground level. The novel intervention was tested against squatting for various physical
29 outcomes (i.e. muscle activity, neuromuscular fatigue, trunk kinematics and lower extremity blood circulation) and
30 self-perceived discomfort, using a simulated rebar tying task in a laboratory. These findings demonstrate that the
31 intervention has beneficial effects on both physical and subjective outcomes, and has a great potential in reducing
32 work-related MSDs among Asian rebar workers. Additionally, the current study highlights that ergonomic
33 interventions in the construction industry should be derived based on both the characteristics of specific construction
34 trades and culture of workers.

35 **Keywords**

36 Construction ergonomics; Rebar tying; Occupational safety and health; Biomechanical evaluation

37 **Introduction**

38 Work-related Musculoskeletal disorders (MSDs) are a substantial burden on the construction industry. A recent
39 systematic review (Umer et al. 2017a) found that more than 50% of the construction workers suffer from symptoms
40 of low back MSDs annually around the globe. The review also noted that approximately one-third of the
41 construction workforce face symptoms of knee, shoulder and wrist MSDs. These MSDs impose substantial direct
42 and indirect costs (Lehtola et al. 2008), work absenteeism (Rinder et al. 2008), schedule delays and lost time claims
43 to the industry (Inyang et al. 2012). Multiple studies have reported the high direct and indirect costs of traumatic and
44 non-traumatic MSDs in the construction industry (Pandey et al. 2012), including loss of productivity (van der Molen
45 et al. 2009), increased insurance premium (Inyang et al. 2012) and permanent disability (Welch et al. 2009). During
46 the year 2014, MSDs resulted in one-third of all work absenteeism related to illness and injuries in the US
47 construction industry (BLS 2015). In Canada, Alberta Construction Safety Association reported that 41.9% of all
48 accepted lost time claims and 46.8% of total injury claims were related to MSDs in 2008 (ACSA 2009).

49
50 Work-related MSDs among construction workers are highly related to physically demanding work tasks (Cheng et
51 al. 2013), which exposes these workers to numerous ergonomic risk factors. These risk factors include heavy lifting
52 and carrying, jerky movements, vibrations, and repetitive works in prolonged awkward work postures (Buchholz et
53 al. 1996; Forde and Buchholz 2004; Umer et al. 2017b; Welch et al. 2009). These factors overload the workers`
54 musculoskeletal system and increase the workers` vulnerability to work-related MSDs (Inyang et al. 2012). By
55 reducing or eliminating these risk factors, the propensity of work-related MSDs can be controlled. It is generally
56 agreed that effective technological and ergonomic interventions are crucial for the mitigation of prevalent MSDs in
57 the construction industry (Lehtola et al. 2008; Rinder et al. 2008). However, since each construction trade has a
58 unique set of tasks that may expose the workers to specific ergonomic risk for certain MSDs (Choi et al. 2014),
59 ergonomic interventions should be task specific (Wang et al. 2015; West et al. 2016).

60
61 Among workers in different construction trades, rebar workers are highly vulnerable to MSDs because of their task
62 contents (Ontario data:1994-1998; Schneider and Susi 1994; Silverstein and Kalat 1999). In particular, manual rebar
63 workers frequently need to bend forward in stooping or squatting posture in order to tie reinforcement bars with
64 metal tie-wires on the floor (Dababneh et al. 2000). Observational ergonomic studies have revealed that rebar

65 workers remain in non-neutral trunk postures for up to 58% of the workday when they opt for stooping (Buchholz et
66 al. 2003; Forde and Buchholz 2004; Saari et al. 1978). A recent biomechanical study also found that rebar tying in a
67 stooping posture led to flexion-relaxation phenomenon of lower back, which deactivates back muscles and may
68 result in increased loading stress on passive torso tissues (e.g. ligaments or facet joint capsules) (Umer et al. 2017b).
69 As such, prolonged and repetitive highly flexed trunk posture is known to be a risk factor for back MSDs (Garg
70 1992; McGill and Kippers 1994; Neumann et al. 1999). In Asian culture, squatting is preferred to stooping for rebar
71 tying (Chung et al. 2003; Jung and Jung 2008). In such posture, lower extremities are subjected to surge in postural
72 load (Buchholz et al. 1996; Genaidy et al. 1994). Since squatting increases the contact pressure at knees at the end-
73 range of knee flexion, this biomechanical factor can increase the risk of knee MSDs (Kivimäki et al. 1992; Thun et
74 al. 1987). Additionally, squatting posture may affect the blood circulation of lower extremities (Basmajian and
75 Deluca 1985), which may cause discomfort or compromise functional performance of workers. Given that many
76 postural-related physical risk factors are modifiable, task-specific ergonomic interventions should be implemented
77 (Forde et al. 2005; Vi 2003) to alleviate the high physical workload of manual rebar tying.

78
79 To reduce physical workload of the trunk and knees during rebar tying, different commercially available wearable
80 ergonomic devices may be used although the adoption rate is low (Weinstein et al. 2007). These ergonomic
81 interventions include, but are not limited to, Bending Non-Demand Return (BNDR) (Ulrey and Fathallah 2013),
82 Happyback (ErgoAg Company, Aptos, CA) and Personal Lift Assist Device (PLAD) (Lotz et al. 2009). These
83 exoskeletons provide anti-gravity moment to reduce trunk muscular workloads. Although these devices were
84 primarily designed for the agriculture and manufacturing industry rather than the construction industry, the inventors
85 claim that these devices can be used in other physically demanding jobs (e.g. rebar tying) (Ulrey and Fathallah
86 2013). However, rebar workers rarely use these devices (especially those working in the fastest growing Asian
87 construction market, Horta et al. 2013). To understand the reasons for not adopting these interventions by Asian
88 rebar workers, one of the authors (WU) interviewed four veteran construction project managers in Hong Kong, who
89 have been working in the Asian industry for at least 20 years. These managers were chosen because their experience
90 in project management and their knowledge on construction work-site characteristics, workers' behavior, work
91 demands of construction tasks enabled them to provide comprehensive and pragmatic overview on our interested
92 issues. The interviews revealed several reasons for the reluctance in adopting ergonomic interventions in the

93 industry: inability to use these devices in squatting, high cost, difficulty in handling and storing these tools, and
94 difficulty in repairing and maintenance. Importantly, rebar workers dislike wearing any ergonomic tools that irritate
95 their body parts during the hot and humid season, which is common in Asia.

96

97 To reduce the physical discomfort of Asian workers during rebar tying in squatting, it is essential to develop a low
98 cost and comfortable wearable ergonomic tool. To this end, the authors derived an idea of attaching a stool (10 to 15
99 cm height) to the pants of rebar workers using self-adhesive Velcro straps (Fig. 1). This inexpensive tool allows the
100 workers to work in a low sitting posture instead of squat. Having discussed with the interviewed project managers,
101 they unanimously supported the use of this pragmatic tool. Accordingly, the objective of the present study was to
102 compare the physical and subjective responses of asymptomatic individuals during simulated rebar tying in low
103 sitting and squatting. The findings might have a great potential to improve the health and practice of rebar workers.

104 [Fig. 1]

105 **Methods**

106 *Participants*

107 To evaluate the effectiveness of the “squatting-stool” for rebar tying, fourteen healthy male participants aged
108 between 18 and 40 years were recruited. The exclusion criteria were a previous history of cardiac and pulmonary
109 disorders, current disability of lower back and lower extremity (identified using modified Oswestry Disability Index
110 scores > 20%, Wong et al. 2015), and inability to rate discomfort using self-perceived discomfort ratings
111 (Gescheider 1985; Han et al. 1999). The experimental procedures were approved by the Human Research Ethics
112 Committee of The Hong Kong Polytechnic University.

113

114 *Experimental Procedure*

115 The current experiment adopted a randomized crossover study design in a single visit. Following the detailed
116 explanation of the experiment, written consent was sought from eligible participants. While surface
117 electromyography (sEMG) was used to measure trunk and leg muscle activity, motion sensors and oximeter were
118 used to monitor trunk movement and leg blood circulation, respectively. Prior to the simulated rebar tying task,
119 participants performed a series of reference isometric contraction (RIC) tests of trunk and leg muscles in order to
120 estimate the post-task muscle fatigue (Fig. 2). Participants were then randomly assigned to perform the simulated

121 rebar tying task for 12.5 minutes in one of the two postures: (1) squatting; and (2) low sitting (stool-squatting).
122 Participants needed to report their self-perceived discomfort every 2.5 minutes throughout the rebar tying task.
123 Participants underwent the RIC tests immediately after the task to evaluate muscle fatigue. Thereafter, participants
124 were given a 20-minute sitting break before repeating the entire testing procedures with the untested posture.

125 **[Fig. 2]**

126 ***Reference Isometric Contractions (RICs)***

127 Each participant performed three 5-second RICs involving the lower back, thigh and calf muscles. A 5-second rest
128 was given between contractions (Lotz et al. 2009). The primary purpose of the RIC test was to compare post-task
129 changes in median frequency (MF) of sEMG signals of different muscles, where decrease in MF indicated muscle
130 fatigue (as explained in the section *Muscle Activity* below). Secondly, the amplitude of sEMG signals of different
131 muscles during the pre-task RIC test was used to normalize the respective sEMG signals collected during the
132 simulated rebar tying task (see below).

133

134 The RIC test of lower back muscles involved a modified Sorensen test (Coorevits et al. 2008; Dederling et al. 2000;
135 Mannion and Dolan 1994). Specifically, the participant laid prone on a bench such that his upper body was
136 unsupported (i.e. outer border of the anterior iliac crest was at the edge of the bench) (Fig. 3a). The participant was
137 instructed to keep his hands touching his ears with elbows out to the side at the same level as the trunk, during the
138 test. An examiner fixated the participant's legs during the test.

139 **[Fig. 3]**

140 To perform RIC test of the thigh muscles, the participant was instructed to perform three forward lunges with
141 alternative legs (Pincivero et al. 2000). The participant should keep his back straight, arms beside the body, and the
142 non-lunging (rear) knee slightly off the ground during the lunges (Fig. 3b). The lunge distance of each participant
143 should be equal to the distance between the anterior superior iliac spine and the respective medial malleolus.

144

145 The RIC test of calf muscles involved the performance of an alternative heel rise of each leg (Kasahara et al. 2007;
146 Österberg et al. 1998). The participant raised his heel off the ground (Fig. 3c) while he could touch his index fingers
147 slightly against a wall for balance.

148

149 ***Simulated Rebar Tying***

150 The simulated rebar tying tasks could be performed with or without a stool. To meet individual comfort, participants
151 could choose a plastic stool, either 10cm or 15cm high. Although the originally planned duration of rebar tying task
152 was 20 minutes, the pilot testing on two participants revealed that participants requested to stop the task before the
153 stipulated time due to extreme discomfort. As such, the duration of rebar tying was shortened to 12.5 minutes in
154 each posture. 12.5 minutes was chosen because it was a multiple 2.5 minutes (the time interval for evaluating self-
155 perceived discomfort ratings).

156

157 The simulated rebar tying was conducted on a mesh of 5 by 5 plastic pipes of 1.2m length, separated from each other
158 by a center-to-center distance of 20cm as described elsewhere (Umer et al. 2017b). Participants were instructed to
159 repetitively tie rebar using pigtail tool and tie-wires in the first three rows of the simulation setup unless the
160 stipulated time had elapsed. To evaluate the effects of prolonged squatting/low sitting posture on the participant's
161 physical responses, the participant was not allowed to significantly alter the body posture and position (e.g. standing
162 up). However, slight movements were allowed to accomplish the task.

163

164 ***Measurements***

165 ***a. Muscle Activity***

166 The trunk and leg muscle activity was measured by a 16-channel wireless surface electromyography (sEMG) system
167 (TeleMyo, Noraxon USA, Arizona). Five pairs of muscles were evaluated including bilateral lower back muscles
168 (lumbar erector spinae at the L3 level, and lumbar multifidus at the L5 level), bilateral anterior thigh muscles (rectus
169 femoris) and bilateral calf muscles (gastrocnemius lateralis and gastrocnemius medialis). Surface electrodes were
170 adhered to target muscle locations as recommended by *Surface ElectroMyoGraphy for the Non-Invasive Assessment*
171 *of Muscles* (SENIAM, 2005, Fig. 4). Standardized skin preparation (including shaving, abrading with sandpaper and
172 cleaning with alcohol swabs) was performed on the target sites to ensure the skin impedance below 10k Ω .

173 Disposable bipolar electrodes with a diameter of 15mm and an inter-electrode distance of 20mm were used. The
174 sampling rate and common mode rejection ratio were 1,500 Hz and 100 dB, respectively. The sEMG activities of all
175 muscles during RIC tests and rebar tying tasks were measured.

176

[Fig. 4]

177 Muscle fatigue secondary to rebar tying was estimated from the decrease in MF of sEMG signals during the RIC
178 tests before and after the task (Basmajian and Deluca 1985; Mannion and Dolan 1994; Potvin and Norman 1993).
179 This method has been widely used in biomechanical studies to quantify neuromuscular fatigue of lumbar (Coorevits
180 et al. 2008; Mannion and Dolan 1994), thigh (Longpré et al. 2015; Pincivero et al. 2000) and calf muscles (Kasahara
181 et al. 2007; Wim Ament et al. 1993) during functional tasks.

182

183 ***b. Trunk Kinematics***

184 Spinal movements during the rebar tying task were captured by the MyoMotion system (Noraxon USA, Arizona).
185 Three motion sensors were placed at the T4, T12 and S1 spinous processes (Fig. 4). The spinal segment between T4
186 and T12 was defined as the thoracic spine whereas the segment formed between T12 and S1 sensors was determined
187 as the lumbar spine. Motion data was sampled at 100 Hz. An examiner first guided each participant to maintain an
188 erect standing posture, where the thoracic and lumbar angle was calibrated as zero degree. The trunk segmental
189 flexion angle measured during rebar tying were referenced to this calibration.

190

191 ***c. Lower Extremity Blood Circulation***

192 Blood circulation in the lower extremities was indirectly quantified by measuring the oxygen saturation level (SpO₂)
193 in arterial blood using an oximeter. A perfusion resistant sports grade oximeter (MightySat Pulse Oximeter 9900,
194 Masimo Corporation, Irvine, CA) was placed on the right big toe and data was collected at a rate of 0.5 Hz. The big
195 toe was cleaned by alcohol swabs prior to placing the oximeter for continuous monitoring of SpO₂ levels during
196 rebar tying.

197

198 Initially, this measurement was not planned in the experiment. However, during the pilot trial on two participants,
199 they complained of numbness in their legs after a few minutes of squatting. As squatting posture is known for
200 decreasing blood circulation in lower extremities (Basmajian and Deluca 1985), the leg numbness experienced by
201 the participants might be associated with compromised blood circulation (Ogata and Whiteside 1982; Skobelkin et
202 al. 1990), As such, blood circulation measurement was added in the current study.

203

204 ***d. Self-perceived Discomfort***

205 The subjective perceived discomfort of each participant was measured by the method of Magnitude Estimation.
206 Magnitude Estimation has been widely used to estimate perceived discomfort in psychophysical research (Chung et
207 al. 2003). In the current study, participants utilized whole numbers to rate discomfort levels in various parts of the
208 body (lower back, upper legs, lower legs, and whole body) every 2.5 minutes. The participants chose any arbitrary
209 number (such as zero) to express their discomfort at the beginning of each task. As the task continued and the
210 discomfort increased, the participant could continue to report higher numbers (such as 40, 50, 100 and so on) at each
211 time point, to indicate the heightened self-perceived discomfort (Han et al. 1999). To compare the discomfort rating
212 among participants, min-max normalization was used where minimum and maximum discomfort values were used
213 as references for normalization (Chung et al. 2003). The normalized self-perceived discomfort was calculated as
214 follow

$$PD_{ij} = \frac{x_{ij} - Min_j}{Max_j - Min_j} \times 100\%$$

215
216 where PD_{ij} is the normalized self-perceived discomfort rating for i^{th} reading of the j^{th} participant, x_{ij} is the non-
217 normalized i^{th} discomfort rating for the j^{th} participant, Min_j and Max_j are minimum and maximum discomfort rating
218 perceived by the j^{th} participant throughout the experiment.

219
220 To evaluate the participant's capability in making correct ratio judgments for Magnitude Estimation, two protocols
221 of "line production" and "numerical estimation" were used. For "line production", the participant was instructed to
222 draw seven lines with appropriate lengths to represent seven given random numbers. For "numerical estimation", the
223 participant was asked to estimate the length of seven presented lines (Chung et al. 2003). Separate linear regression
224 analyses were performed for the two protocols by logarithmic plotting of the information provided by the examiner
225 (i.e. random numbers or the length of lines) versus the corresponding participant's responses (Han et al. 1999). If the
226 slopes (i.e. regression coefficients) of the two lines of a given participant were not significantly different from the
227 value of 1.0 (Gescheider 1985), the participant was deemed to be able to make correct ratio judgements. Elsewise,
228 the corresponding data was not included in data analysis.

229 230 **Data Processing**

231 Noraxon MyoResearch MR3.8 (Noraxon USA Inc., USA) software was used for all sEMG signal processing. Raw
232 sEMG data during rebar tying were filtered to remove electrocardiography signals using adaptive filter methods,

233 bandpass filtered at 20-500 Hz, notched filtered at 50 Hz to remove electrical noise, and then smoothen using 50 ms
234 root mean square (RMS) moving window (Xie et al. 2015). The maximum sEMG signal of a given muscle during
235 the pre-task RIC test was identified by applying a moving window of 1000ms with a step size of 50ms to the sEMG
236 signals. To enable between-participant comparison, the sEMG data of each muscle recorded during rebar tying was
237 normalized to and expressed as the percentage of the respective maximum sEMG signal at the pre-task RIC test
238 (%RIC).

239
240 Amplitude Probability Distribution Function (APDF) was used to compare the muscle activity in the two rebar tying
241 postures. Specifically, 50% APDF was used to indicate average muscle activity during the rebar tying task (Xie et al.
242 2015). Although sEMG data were captured from both sides of muscles, paired t-tests with false detection rate (FDR,
243 see below) correction revealed no significant difference in the amplitude of sEMG signals from both sides of any
244 given muscle. Therefore, left and right side values were averaged for further statistical analysis.

245
246 To calculate MF from a raw sEMG power spectrum, each 5-second RIC test was divided into five 1-second
247 segments (without overlapping). A Hanning window was applied to the sEMG signals of each 1-second segment
248 followed by the calculation of MF using Fast Fourier Transformation. The five MF values during each RIC test were
249 averaged to obtain a single MF value (Lotz et al. 2009). As three repetitions of RIC tests were performed for each
250 muscle, MF values of these three RIC tests were averaged for subsequent statistical analysis (Lotz et al. 2009). The
251 post-task MF value of each muscle was then normalized to pre-task MF values (considered as 1.0) to identify
252 fatigue.

253
254 Spinal movement data from the motion sensors were smoothened using Kalman filter prior to statistical analysis.
255 The average thoracic, lumbar, and total trunk flexion angles at 50% APDF of the two rebar tying postures were
256 compared. Blood oxygen saturation (SpO₂) values obtained through oximeter were unfiltered. The temporal changes
257 in SpO₂ values between the two rebar tying postures were estimated from the differences in SpO₂ values at 10%,
258 50% and 90% APDF.

259
260 **Statistical Analysis**

261 Table 1 summarizes various statistical tests conducted on different variables of interest in the current study. Multiple
262 paired t-tests with false detection rate (FDR) correction were used to compare the between-posture difference in the
263 average sEMG activity (50% APDF) of various muscles. FDR was chosen instead of the overly conservative
264 Bonferroni adjustment because it was more suitable for multiple comparisons (Benjamini and Hochberg 1995; Lotz
265 et al. 2009). One-way repeated measures analyses of variance (ANOVA) were used to explore the differences in the
266 normalized pre- and post-rebar tying MF values. Rebar tying postures were chosen as the independent variable,
267 whereas pre- and post-task MF values were the dependent variables. Post-hoc tests involved paired t-tests with FDR
268 correction. Similarly, the differences in the spinal flexion angles and SpO₂ values between the two rebar tying
269 postures were analyzed by multiple paired t-tests with FDR correction. Two-way repeated measures ANOVA was
270 used to investigate the effect of time and stool condition (independent variables) on the normalized self-perceived
271 discomfort ratings (dependent variable). Significant main effects were explored by using paired t-tests. SPSS
272 (version 19.0, IBM Corporation, Armonk, NY) software was used for the statistical analysis with significance value
273 set at $p < 0.05$.

274 [Table 1]

275

276 **Results**

277 The fourteen participants (including two participants in the pilot testing) had a mean age of 27.6 years (SD \pm 4.2
278 years, 10 participants aged between 20 and 29 years and 4 participants aged between 30 and 39 years) and BMI 22.7
279 kg/m² (SD \pm 1.5 kg/m²). The mean and standard deviation of the participants' Oswestry Disability Index score was
280 2.3 \pm 4.0%. All participants chose the stool with a height of 15 cm. When tested, all participants were found able to
281 make correct ratio judgements.

282

283 ***Muscle Activity***

284 Fig. 5 demonstrates the normalized 50th percentile sEMG amplitudes of the various muscles (along with standard
285 deviations) during rebar tying in the two postures. The average sEMG activities of different muscles during rebar
286 tying varied between 1.2% and 3.8%RIC. The lumbar muscles tended to show the least activity whereas
287 gastrocnemius lateralis muscles showed the highest magnitude of activity.

288

[Fig. 5]

289 Lower back muscles (i.e. lumbar erector spinae and multifidus) and the calf muscle - gastrocnemius medialis
290 exhibited no significant difference in activity during rebar tying in the two postures. The thigh muscle, rectus
291 femoris, tended to have a higher absolute muscle activity in the squatting posture as compared to stool-squatting (a
292 mean difference of 1.6%RIC, $p=0.12$). On the contrary, gastrocnemius lateralis muscles showed significantly higher
293 muscle activity during stool-squatting rebar tying than squatting rebar tying task [mean difference = 1.6%RIC (95%
294 CI = 0.1 to 3.1%RIC)].

295

296 The pre- and post-task changes in normalized MF in the two rebar tying postures are depicted in Fig. 6. Depending
297 on the muscles, there were variations in post-rebar tying MF values (ranging from a decrease of 4.3% in right
298 lumbar erector spinae after stool-squatting to an increase of 3.9% in right gastrocnemius lateralis after squatting
299 rebar tying). However, one-way repeated measures ANOVA revealed no significant temporal changes in pre-task,
300 post-squatting, and post-stool-squatting MF.

301

[Fig. 6]

302 *Trunk Kinematics*

303 The average total trunk flexion angles at 50% APDF were 57.3° and 66.0° for rebar tying with and without stool,
304 respectively (Fig. 7). For both rebar tying postures, the average total trunk flexion angles were mainly contributed
305 by lumbar flexion (average values of 43.0° to 48.8°), whereas thoracic flexion only contributed to less than 18° in
306 both postures. Squatting demonstrated significantly larger thoracic, lumbar, and total trunk flexion angles as
307 compared to stool-squatting rebar tying. Specifically, the mean difference was 3.0° for thoracic flexion (95% CI =
308 0.2° to 5.7°), 5.8° for lumbar flexion (95% CI = 1.3° to 10.3°) and 8.7° for total trunk flexion (95% CI = 5.6° to
309 11.9°).

310

[Fig. 7]

311 *Lower Extremity Blood Circulation*

312 Fig. 8 depicts the lower extremity SpO₂ values at 10%, 50% and 90% APDF of the two rebar tying postures. The
313 SpO₂ values varied from 73.9% to 96.8%. Regardless of the APDF percentile chosen for the comparison, rebar tying
314 using the stool demonstrated significantly larger SpO₂ values than rebar tying in squatting. Specifically, the mean
315 difference in SpO₂ values for 10%, 50% and 90% APDF of the two rebar tying postures was 13.2% (95% CI = 5.2 to
316 21.2%), 10.6% (95% CI = 4.1 to 17.2%) and 7.1% (95% CI = 1.2 to 12.9%), respectively.

317 [Fig. 8]

318 ***Self-perceived Discomfort***

319 Two-way repeated measures ANOVA revealed significant interaction between stool condition and time ($p < 0.01$,
320 Table 2) for various body parts (i.e. lower back, upper legs, lower legs, and whole body) examined in this study.
321 Post-hoc tests revealed that the use of a stool yielded significantly lower (better) self-perceived discomfort ratings of
322 all aforementioned body parts as compared to squatting. These differences began from the first 2.5 minutes to the
323 end of the task (Fig. 9). The maximum difference in the normalized self-perceived rating for rebar tying with and
324 without stool was noted at lower legs toward the end of experiments [mean difference = 65.1% (95% CI = 50.8 to
325 79.3%)]. On the other hand, there was minimum difference in lower back discomfort at the end of the tasks [mean
326 difference = 23.9% (95% CI = 10.0 to 37.9%)]. For upper legs and whole body, normalized self-perceived
327 discomfort ratings at end of the experiments varied in two rebar tying postures with a mean value of 44.5% (95% CI
328 = 33.3 to 55.6%) and 53.9% (95% CI = 40.1 to 67.6%) respectively (Fig. 9).

329 [Fig. 9]

330 [Table 2]

331 **Discussion**

332 The current results indicate that multiple biomechanical and physiological measurements are necessary to
333 understand physical demands of occupational work tasks comprehensively. Specifically, the two rebar tying postures
334 elicited comparable muscle activity and muscle fatigue in back and lower limb muscles. However, trunk kinematics,
335 blood circulation and self-perceived discomfort significantly differed between the two postures. Importantly, the
336 current findings suggest that a small change in work practice may bring significant ergonomic benefits.

337

338 ***Muscle Activity***

339 The normalized average sEMG amplitude of various muscles during simulated rebar tying indicated that the tasks
340 did not involve extensive muscle activity irrespective of the adopted posture (i.e. muscle activity was less than
341 4%RICs in all muscles) (Fig. 5). However, this does not imply that such small muscle activity cannot induce
342 neuromuscular fatigue. Literature suggests that tasks involving sustained contractions as low as 2% of maximum
343 voluntary contraction in the lumbar erector spinae muscles can significantly decrease tissue oxygen levels, and cause
344 muscle fatigue that may lead to work-related MSDs in the long run (McGill et al. 2000). Further, the comparison of

345 muscle activity in the two rebar tying postures reveals a tradeoff between the thigh and calf muscles. Specifically,
346 rectus femoris muscles showed larger average activity in the squatting posture whereas gastrocnemius lateralis
347 muscles were more active during stool-squatting rebar tying. These results concur with those from Sriwarno et al.
348 (2007) who also reported this shift in thigh and calf muscle activity between squatting and stool-squatting postures
349 for a paper cutting task. Unfortunately, Sriwarno et al. (2007) did not investigate the neuromuscular fatigue and
350 blood circulation of lower limbs, which might improve the understanding of differences in biomechanical and
351 physiological demands of lower extremities in the two postures. Further, the negative MF findings suggest that both
352 rebar tying tasks did not induce neuromuscular fatigue of lumbar and calf muscles (Fig. 6). It indicates that the
353 increases in self-perceived discomfort following the rebar tying task (especially in the squatting posture) may be
354 unrelated to local muscle fatigue of lower extremities.

355

356 ***Trunk Kinematics***

357 The use of a stool during stool-squatting rebar tying helped reduce the average total trunk flexion angle by
358 approximately 9° as compared to squatting (Fig. 7). This ergonomic tool helps restore the trunk flexion angle back to
359 the limit (60°) recommended by the international organization for standards (ISO) for static working postures [ISO
360 11226:2000 (*ISO 2006*)]. Sriwarno et al. (2007) also reported a decrease in trunk flexion after using a stool for a
361 paper cutting task as compared to squatting posture. However, their findings could not be directly compared with the
362 present study given the discrepancy in the definitions of “trunk” in the two studies. Despite significant reduction in
363 the total trunk flexion angle in the current study, no significant differences in the muscle activity or normalized MF
364 values of lower back muscles between the two rebar tying postures were observed. This finding may be attributed to
365 the flexion-relaxation phenomenon which involves myoelectric silence of lumbar paraspinal muscles when
366 asymptomatic individuals maintain an almost fully flexed lumbar spine (McGill and Kippers 1994; Shirado et al.
367 1995). Literature suggests that such silence in lower back muscle activity starts at around 50° of trunk flexion
368 (Solomonow et al. 2003). With the mean trunk flexion angle of > 55° and lower back muscle activity of < 1.5%RIC
369 in the current study, the flexion-relaxation phenomenon might occur during both rebar tying tasks. The notion is
370 further supported by previous studies that found a significant decrease in paraspinal muscle activity during passive
371 sitting postures (i.e. slump sitting) as compared to active sitting (Sullivan et al. 2002, 2006).

372

373 ***Lower Extremity Blood Circulation***

374 To the knowledge of the authors, no prior study has compared the lower extremity SpO₂ levels between the two
375 rebar tying postures. The significantly higher SpO₂ values of legs during stool-squatting rebar tying as compared to
376 squatting (Fig. 8) indicate a potential temporary ischaemia of lower extremities in the squatting posture. As a result,
377 this may reduce the oxygen supply (local hypoxia) to skeletal muscles which is necessary for their normal
378 functioning. It is well known that reduced oxygen supply to muscle tissues can adversely affect human muscle
379 performance (e.g. increased rate of muscle fatigue, and decreased time to exhaustion and muscle numbness (Chung
380 et al. 2003; Cymerman et al. 1989; Hepple 2002)). The local hypoxia of lower limb muscle during squatting rebar
381 tying might explain the significant temporal increases in self-perceived discomfort during the squatting rebar tying
382 despite the absence of decreases in MF values. It also explains the lower self-perceived discomfort during stool-
383 squatting rebar tying given the better blood circulation of lower extremities.

384

385 ***Self-perceived Discomfort***

386 As aforementioned, the difference in self-perceived discomfort in the two postures could be associated with
387 differential decreases in blood circulation in lower extremities. Additionally, different body weight transfer
388 mechanisms might explain the difference in self-perceived discomfort ratings. Sriwarno et al. (2007) revealed that
389 using a stool in squatting could significantly reduce the feet-ground reaction force up to 25% by providing an
390 alternate path for body weight transfer through a stool. Overall, these findings substantiated that the effect of stool
391 significantly decreased the self-perceived discomfort rating and this beneficial effect became more obvious as time
392 elapsed (Fig. 9).

393

394 ***Implications***

395 Work-related MSDs are one of the leading causes of occupational disability among construction workforce (Arndt et
396 al. 2005). Ergonomic interventions are one of the effective avenues for preventing MSDs in the construction
397 industry (Denis et al. 2008). Construction professionals, specifically project managers and policymakers can play a
398 vital role in this regard. By deepening their understanding of physical demands and postural practices employed by
399 workers in various construction trades, it may help identify the root causes of the trade specific MSDs and derive

400 new solutions to alleviate high physical workload in each trade. For instance, the current results help construction
401 professionals recognize a simple stool can reduce discomfort of manual rebar tying in Asian culture.

402

403 The use of such a squatting-stool might serve even a wider construction worker community. As most Asian
404 construction workers squat down to undertake work tasks near or at ground level (e.g. floor dismantling, tile fixing,
405 welding and electrical works) (Fig. 10). Given the simplicity and low cost of the squatting-stool, it may have a great
406 potential to be widely adopted among Asian construction workers.

407 **[Fig. 10]**

408 Although the results of the current study might help alleviate the physical workload of manual rebar tying, the use of
409 squatting-stool should be a part of a wider management policy rather being the only strategy for managing MSDs.
410 Other work-related MSD management approaches such as regular muscle strengthening and stretching exercises
411 (Parker and Worryingham 2004), postural variation, adjustment of the work schedule to make physically demanding
412 tasks intermittent should also be included in a broader mitigation scheme (Umer et al. 2017b). Additionally,
413 manufacturing alternatives such as offsite prefabrication might be considered to eliminate the need of onsite
414 fabrication/assembly of certain items, which demands strenuous physical work and/or awkward postures.

415

416 **Limitations and Future Works**

417 Despite our promising findings, future research is warranted. First, the biomechanical effectiveness of the squatting-
418 stool and its acceptance/feasibility should be verified in actual rebar workers at construction sites. Second, the
419 biomechanical and physiological effects of prolonged use of squatting-stool (three to four hours work shift) should
420 be investigated prior to its onsite adoption. Third, the design of the squatting-stool should be refined. For example,
421 the interviewed construction project managers suggested the legs of the stool to be modified to prevent the legs from
422 being stuck in the rebar mesh. Other design variables of the stool (e.g. material, height, weight and foldability)
423 should also be considered.

424

425 Although the use of the stool has resulted in significant physical and self-perceived benefits, the outcomes indicate
426 that squatting-stool rebar tying still requires large trunk flexion (mean flexion angle = 57°). This underpins the
427 necessity of improving this domain. Power tying tools may have the potential to solve this shortcoming by allowing

428 rebar workers to perform rebar tying in standing (Albers and Hudock 2007; Vi 2003). However, power tying tools
429 also have their drawbacks including higher initial cost, frequent maintenance cost, inability to handle all sizes of
430 rebars (in terms of diameter), substantial weight, need for special tying wire, operational vibrations, and loss of
431 productivity in case of machine breakdown (Albers and Hudock 2007; Dababneh et al. 2000; Vi 2003). It is hoped
432 that future power tools will solve some or all of these limitations. Alternatively, semi-automatic ergonomic tools
433 could be developed to replace electric motors with hydraulic/mechanical components so as to lower the cost and
434 weight of these tools. Nevertheless, till then squatting-stool could serve as an interim low-cost intervention which
435 can significantly mitigate the physical workload in manual rebar tying.

436

437 **Conclusions**

438 This was the first study to investigate the effectiveness of using a squatting-stool for manual rebar tying against
439 squatting in Asian workers. While the results revealed similar trunk and leg muscle activity and no significant
440 difference in neuromuscular fatigue level of trunk and leg muscles between both rebar tying postures, stool-
441 squatting rebar tying demonstrated significantly better: (1) lower extremity blood circulation; (2) trunk flexion angle
442 (within the ISO recommended limits for static working postures); and (3) self-perceived discomfort ratings. These
443 encouraging findings highlight the potential prospects of such a simple and low cost intervention for Asian workers
444 in various construction trades (including rebar tying). Future field research is warranted to evaluate the
445 acceptance/feasibility of using this stool in the construction industry. Importantly, the current study highlights that it
446 is essential to consider both the characteristics of individual construction trades and cultures of workers in order to
447 derive proper task-specific ergonomic interventios for the construction industry. Given the high physical demands of
448 construction workers, more ergonomic studies should be conducted in the construction industry to help construction
449 managers and policy makers design effective mitigation strategies to reduce work-related MSDs.

450

451 **Data Availability Statement**

452 Data generated or analyzed during the study are available from the corresponding author by request.

453

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457

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596

597 **Fig. 1.** Attachment of a stool to the trousers using self-adhesive Velcro straps

598 **Fig. 2.** Experimental flowchart

599 Note: sEMG = surface electromyography; MF = median frequency

600 **Fig. 3.** Performance of reference isometric contractions (RICs) for the muscles under study

601 **Fig. 4.** sEMG and motion sensors` placement on various body parts

602 Note: T4, T12 and S1 refers to body landmarks of various spinal levels; LES = lumbar erector spinae; MultF =
603 multifidus; for lumbar erector spinae (a), the electrodes were placed at L3 level of lumbar spine (5cm laterally from
604 midline); for multifidus, electrodes were placed along the line joining caudal tip posterior iliac spine to L1-L2 joint
605 (2cm laterally from midline at L5 level); for rectus femoris (b), at 50% of the line distance formed by joining
606 anterior iliac spine and superior part of patella; for gastrocnemius lateralis (c), at one third of the line length formed
607 by joining the head of fibula and the heel and at the most prominent bulge of the muscle for gastrocnemius medialis
608 muscles (SENIAM 2005).

609 **Fig. 5.** Muscles` activity comparison between two rebar tying postures for average activation levels (50% APDF)

610 Note: * indicates $p < 0.05$; RIC = reference isometric contraction; bars indicate standard deviation

611 **Fig. 6.** Pre and post-task normalized median frequency analysis for the two rebar tying postures

612 Note: MF = median frequency; Lt= left side muscle; Rt= right side muscle; bars indicate standard deviation

613 **Fig. 7.** Comparison of spinal flexion variables

614 Note: * indicates $p < 0.05$; bars indicate standard deviation

615 **Fig. 8.** Comparison of blood oxygen saturation levels (SpO₂)

616 Note: * indicates $p < 0.05$; APDF = amplitude probability distribution function

617 **Fig. 9.** Normalized self-perceived discomfort ratings comparison between the two postures

618 Note: where * indicates $p < 0.05$; bars indicate standard deviation

619 **Fig. 10.** Other construction tasks requiring squatting postures

620 **Table 1.** Summary of the statistical tests conducted in the current study

Variables under consideration	Statistical tests conducted	Objectives of the tests
Muscle activity	Paired t-tests (with FDR correction)	To identify changes in muscle activations between the two rebar-tying postures
MF (sEMG)	One-way repeated measures ANOVA, paired t-tests for post-hoc analysis	To quantify post-task muscle fatigue
Spinal flexion angles	Paired t-tests (with FDR correction)	To compare trunk flexion angles during rebar tying
SpO ₂ levels	Paired t-tests (with FDR correction)	To quantify temporal changes in SpO ₂ levels of lower limbs during rebar tying
Self-perceived discomfort	Two-way repeated measures ANOVA, paired t-tests for post-hoc analysis	To compare the self-perceived discomfort levels of the two postures at various time points during rebar tying

621 Note: MF = median frequency; sEMG = surface electromyography; SpO₂ refers to blood oxygen saturation levels;
 622 FDR = false detection rate; ANOVA = analysis of variance
 623

624 **Table 2.** ANOVA Results for Discomfort Rating

Body part	Factors		
	p (stool condition)	p (time)	p (stool x time)
Lower back	.001	<.001	.008
Upper legs	<.001	<.001	<.001
Lower legs	<.001	<.001	<.001
Whole body	<.001	<.001	<.001

625