

1 **Effects of Traffic Load Amplitude Sequence on the Cracking Performance of**  
2 **Asphalt Pavement with a Semi-rigid Base**

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# 1 Effects of Traffic Load Amplitude Sequence on the Cracking Performance of 2 Asphalt Pavement with a Semi-rigid Base

3 The propagation of cracks in in-service asphalt pavements is closely related to the complicated  
4 traffic loading patterns over time. However, typical traffic-related variables capture only the  
5 overall traffic level without being able to account for the load-time history. Therefore, this  
6 study aims to investigate the effects of traffic load sequence on the cracking performance of  
7 asphalt pavement from both field and laboratory perspectives. A load amplitude sequence  
8 (LAS) index was developed to characterize the traffic loading sequence in the field. Two  
9 machine learning (ML) algorithms, namely artificial neural network (ANN) and random forest  
10 regression (RFR), were applied to correlate the LAS index with field pavement cracking  
11 performance. The two-block semi-circular bending (SCB) test was developed to characterize  
12 the non-linear fatigue damage accumulation of asphalt mixtures. It was found that heavier  
13 traffic loads in early stages are detrimental to the long-term pavement cracking performance.  
14 The LAS index plays a crucial role in the prediction and development of pavement cracks. The  
15 laboratory test results reveal that a loading sequence starting with a higher stress may shorten  
16 the fatigue life and vice versa. The outcomes of this study may contribute to a better  
17 understanding of the traffic loading characterization of in-service asphalt pavements.

18 *Keywords:* Load amplitude sequence, Pavement cracking, Traffic loading characterization,  
19 Machine learning, Variable amplitude fatigue test.

## 21 1 Introduction

22 The semi-rigid base asphalt pavement, consisting of one or more asphalt layers on a cement-treated  
23 base, is the main type of pavement structure in China since 1997 (Dong *et al.*, 2021). Compared with  
24 conventional flexible pavement, the cement-treated materials in semi-rigid base asphalt pavement

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1 could effectively reduce the vertical compressive strain on the subgrade and enhance the bearing  
2 capacity of the road structure (Zang *et al.*, 2018). However, asphalt pavement with a semi-rigid base  
3 is prone to generate transverse cracks due to temperature variation, cycling traffic loading and  
4 reflection from the base layer. As a result, periodic maintenance and rehabilitation (M&R) treatments  
5 are required to maintain the functionality of the pavement, which incur vast maintenance costs and  
6 significant environmental burdens (Santos *et al.*, 2017; Hu *et al.*, 2019). Therefore, it is necessary to  
7 examine the influence of different factors, such as material properties and climate and traffic conditions  
8 (Abaza, 2016), on the deterioration of pavement cracking performance.

9         In terms of traffic, equivalent single axle load (ESAL) is commonly used for characterizing the  
10 traffic load conditions of a road segment. It has been often employed as an important traffic input for  
11 pavement design (AASHTO, 1993) and as a key influencing factor for pavement performance  
12 prediction (Yao *et al.*, 2019; Guo *et al.*, 2021). Damage caused by wheel loads of varying magnitudes  
13 and repetitions is converted to damage from an equivalent number of standard loads by ESAL. It  
14 depicts a mixed stream of traffic accumulated over the analysis period with various axle loads and axle  
15 configurations. However, the accuracy of the ESAL expression has long been debated by pavement  
16 experts (Prozzi and Madanat, 2004; Guler and Madanat, 2011). To avoid the errors caused by ESAL  
17 conversion, some studies directly used the information from the entire axle load spectrum, such as the  
18 proportion, magnitude and repetitions of loads in each axle load group, to characterize the traffic load  
19 condition (Timm *et al.*, 2005; Haider and Harichandran, 2009). Although many researchers have  
20 claimed the importance of ESAL and axle load spectrum in predicting pavement performance  
21 (Solatifar and Lavasani, 2020; Yao *et al.*, 2020; Tran and Hall, 2007), both measures can only capture  
22 the overall traffic level of a road section. ESAL is calculated by summing up the equivalent axle loads  
23 over the analysis period, whereas variables extracted from the axle load spectrum depict the overall  
24 distribution of axle loads in various weight ranges. Neither of them has taken into account the traffic  
25 loading history over a certain period of time, but some studies have reported the impact of loading  
26 sequences on the performance deterioration of asphalt mixtures (Jiang *et al.*, 2016).

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1           Moreover, field observations show that asphalt pavements with similar ESAL or axle load  
2 spectrum in the same climate zone can have significantly distinct degradation rates, resulting in  
3 different maintenance needs. The early damage of asphalt pavement is also considered to be closely  
4 related to the traffic overload phenomenon at the beginning of the service life (Pais *et al.*, 2013). Both  
5 phenomena are very likely to be caused by the different traffic loading histories. Therefore, in addition  
6 to the overall traffic level, other factors associated with the traffic loading history, such as the time  
7 series of load amplitudes, are also potential contributing factors to the deterioration of asphalt  
8 pavements.

9           Most laboratory tests for testing the performance of asphalt mixture were developed based on  
10 cyclic loading with single amplitude, frequency and waveform (Benedetto *et al.*, 2011; Wang *et al.*,  
11 2022), which can hardly reflect the complex loading sequence effects. Considering the complex and  
12 almost stochastic loading conditions of in-service pavements, it would be useful to understand the  
13 deterioration of pavement cracking performance under variable-amplitude loading, which has been  
14 well applied to characterize the fatigue cracking propagation in other materials and structures (Zhu *et*  
15 *al.*, 2019; Yuan *et al.*, 2015). At present, several incremental dynamic loading tests are available to  
16 simulate the multiple load amplitude conditions in the field, such as the Incremental Repeated Load  
17 Permanent Deformation (iRLPD) test (Azari and Mohseni, 2013), Multi-sequenced Repeated Load  
18 (MSRL) test (Dong *et al.*, 2018), and Triaxial Stress Sweep (TSS) test (Kim and Kim, 2017). They  
19 introduced load amplitude sequences into laboratory tests for characterizing the rutting resistance of  
20 asphalt mixtures (Azari and Mohseni, 2021; Zhao *et al.*, 2020; Wang *et al.*, 2018). The creep  
21 accumulation process in asphalt mixtures at high temperatures depends on the time history of the  
22 applied stress/strain. However, for intermediate temperatures, there is still little field or laboratory  
23 validation for the impact of loading sequences on the development and propagation of cracks in asphalt  
24 pavements. The load amplitude sequence was also rarely considered in the performance model of  
25 asphalt pavements.

26           To fill the aforementioned knowledge gap, this study aims to investigate the effects of traffic

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1 load amplitude sequence on the cracking performance of semi-rigid base asphalt pavement from both  
2 field and laboratory perspectives. A new Load Amplitude Sequence (LAS) index is proposed, which  
3 is expected to compensate for the traditional traffic variables, allowing for more accurate pavement  
4 performance prediction and improved maintenance planning.

## 5 **2 Data and Material Preparation**

### 6 **2.1 Field data collection**

7 The Pavement Management System (PMS) in Jiangsu, China has a databased with a large amount of  
8 field data for over 14,000 lane kilometers of highway. These data cover information related to  
9 pavement structures and materials, traffic loads, climate conditions, pavement performance, and  
10 maintenance history for each expressway. The time span of these data ranges from 2003 to 2021,  
11 providing sufficient data support for the smooth running of the research. Prior to analysis, each  
12 expressway was divided into sub-sections based on the location (pavement or bridge), lanes, directions,  
13 and the structural and traffic sections to which they belong. Subsections longer than 1.5 km were  
14 further subdivided at 1 km intervals. After excluding some segments with incomplete information or  
15 very short length, a total of 10,330 pavement segments were obtained, totaling 8,771 lane kilometers.

### 16 **2.2 Selection of influential factors and pavement cracking index**

17 Transverse cracking is the most prevalent forms of cracking on asphalt pavement with a semi-rigid  
18 base, accounting for more than 85% of all distress (Zhou *et al.*, 2014). Thus, in this study, the  
19 Transverse Cracks Evaluation Index (TCEI) proposed in (Zhou *et al.*, 2010) was used to assess the  
20 cracking performance of semi-rigid base asphalt pavements. The TCEI was derived by converting the  
21 ratio of Transverse Crack Spacing (TCS) to transverse crack width ratio (TWR) to a scale of 0 to 100,  
22 with 100 being the intact condition (i.e., no transverse cracks). The influential factors for constructing  
23 the cracking performance model were identified by reviewing the relevant literature (Yao *et al.*, 2021;  
24 Karlaftis and Badr, 2015) and checking the availability of information in the PMS. Particularly, the

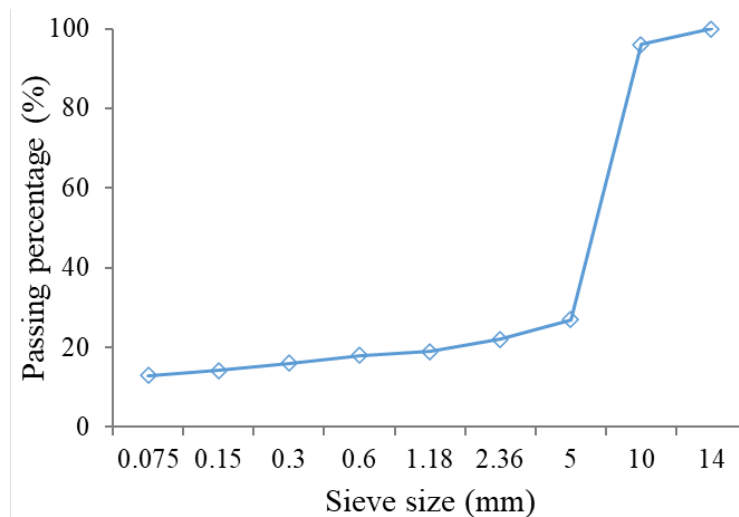
1 LAS index was proposed to approximately describe the evolution of field load amplitudes during a  
 2 given analysis period. The detailed definition of LAS will be introduced later. PLDF (Proxy of Lane  
 3 Distribution Factor) is a nominal variable, combining the number of lanes (4, 6, or 8) in the current  
 4 section with the index of the current lane (1, 2, 3, or 4). It was used to represent the lane distribution  
 5 factor, indicating how traffic is distributed in different lanes. **Table 1 summarizes the influencing**  
 6 **factors considered in this study.**

7 Table 1 The selected influential factors and pavement cracking index.

Class	Variables	Description	Unit or magnitude
Pavement structures and materials	SBS modified asphalt layer thickness	The thickness of Styrene-Butadiene-Styrene (SBS) modified asphalt layers	cm
	Asphalt layer thickness	The total thickness of all asphalt layers	cm
	Asphalt layer material	The gradations of the multiple asphalt layers	/
	Base layer thickness	The thickness of base course	cm
	Base layer material	The material of base course	/
Traffic loads	ESAL	The equivalent single-axle loads	$\times 10^4$
	Overload rate	The percentage of overweight axle loads to total axle loads	dimensionless
	LAS	The load amplitude sequence index proposed in this study	dimensionless
Climate factors	R <sub>over 35 °C</sub>	Proportion of days with daily maximum temperature over 35 °C	%
	R <sub>below 0 °C</sub>	Proportion of days with daily minimum temperature below 0 °C	%
	Ratio of rainy days	Proportion of rainy days	%
	Mean temperature	The daily average air temperature	°C
	Mean precipitation	The daily average precipitation	mm
Performance	TCEI	Transverse Cracks Evaluation Index	dimensionless
Others	PLDF	The combination of the number of lanes in the current section and the index of the current lane	/
	Road or bridge	Whether it is a bridge pavement or a road pavement	/
	Service time	The interval from the time when the road section was opened to traffic to the time	year

### 2.3 Materials and mixture design

To further verify the loading sequence effect on asphalt mixtures, a commonly used stone mastic asphalt (SMA) mixture with a nominal aggregate size of 10mm and aggregate type of granite was selected for the research. SBS modified asphalt binder with Superpave performance grade of 76-16 (PG76-16) and optimum content of 6.0% by weight of asphalt mixture was used. The target air void content was  $4\pm 0.5\%$ . The detailed aggregate gradation is shown in Figure 1. The loose mix was first subjected to a long-term oven aging procedure at 135 °C for 8 h (Chen *et al.*, 2021). Then, the aged loose mix was compacted into cylindrical specimens with diameters and heights of 150 mm using the Superpave Gyrotory Compactor (SGC). Following that, around 20 mm were removed from both ends of each cylindrical specimen due to a considerably larger air void content as compared to the central region. Finally, the remaining middle part of each cylindrical specimen was cut into four half rings with a diameter of 150 mm and a height of 50 mm, as shown in Figure 2(a). All half ring specimens were measured for air void content, and those with air void content outside the range of  $4\pm 0.5\%$  were discarded. As Figure 2(b) shows, the qualified half ring specimens were selected for the semi-circular bending (SCB) test under different load conditions.



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17 Figure 1. Aggregate gradation.

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(a)



(b)

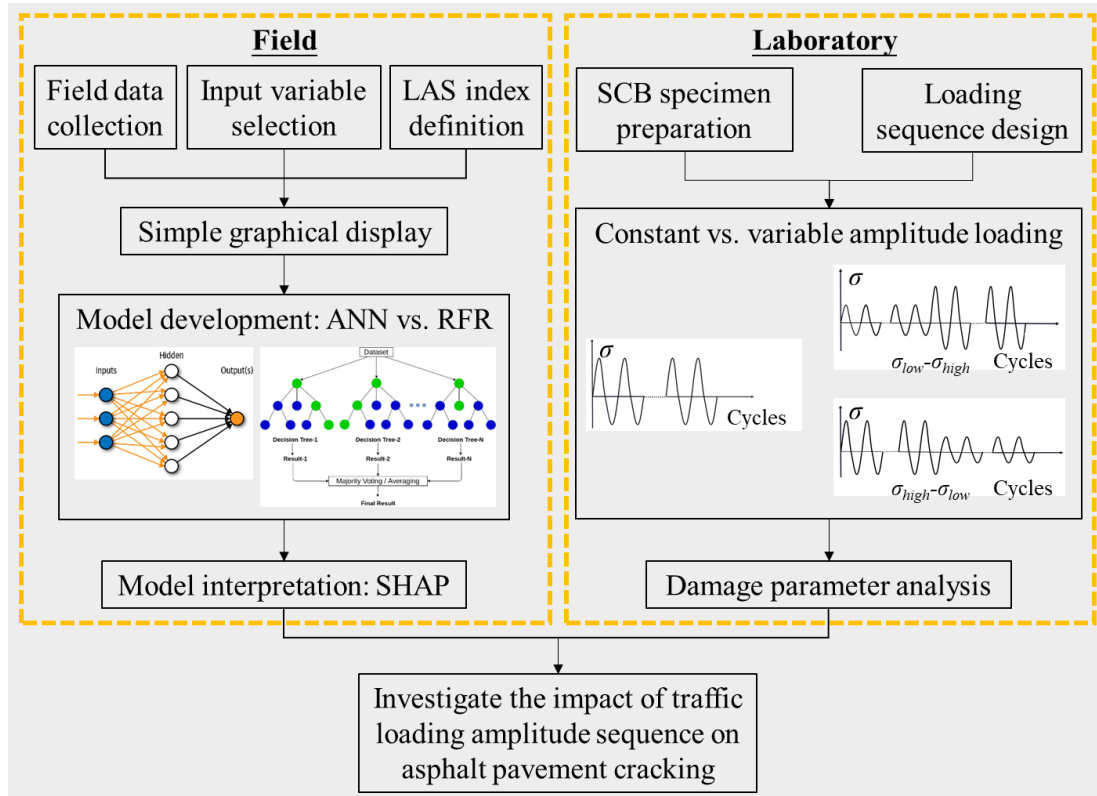
1 Figure 2. Specimen preparation: (a) half ring specimens; (b) set-up of the SCB test.

### 2 3 Methodology

3 An overview of the methodology used in the present study is shown in Figure 3. The effect of traffic  
4 load amplitude sequence on asphalt pavement cracking were investigated from both field and  
5 laboratory perspectives. Field validation started from collecting field data, selecting influential factors,  
6 and defining load amplitude sequence (LAS) index. Armed with this information, the deterioration of  
7 pavement cracking condition at different LAS levels was first graphically displayed to show the  
8 presence of the loading sequence impact on pavement cracking. Then, two machine learning (ML)  
9 models were developed to model the correlation between the LAS index and TCEI. Finally, for the  
10 superior model, an in-depth interpretation and analysis of the model output would be performed to  
11 further examine the effect of loading sequence on pavement cracking and its interaction with other  
12 factors. Laboratory validation was achieved by conducting two-block SCB tests to characterize the  
13 nonlinear damage accumulation in asphalt mixture under different loading conditions. To do so, SCB  
14 specimens were first prepared and loading sequences with constant and variable amplitudes were  
15 designed accordingly. Based on this, the fatigue curves and fatigue damage parameters of asphalt



1 mixtures under different loading conditions were obtained and compared. The laboratory test results  
 2 are expected to provide a better understanding of the underlying physical meaning of the LAS index.  
 3



4  
 5 Figure 3. Overview of the methodology adopted in the present study.

6 **3.1 Field validation**

7 **3.1.1 Load amplitude sequence index**

8 To capture the characteristics of traffic load amplitude sequence in the field, the LAS index was  
 9 proposed in this study. It was developed based on the variation of overload rate of the vehicle axle  
 10 during a specific period. Overloading of large and medium-sized trucks was very common on the  
 11 highways in Jiangsu, especially in the early years, causing a lot of early damage to the pavement  
 12 structure. According to the regulations issued by the Ministry of Transport of the People's Republic  
 13 of China (Ministry of Transport of the People's Republic of China, 2016), the axle limits for single-,

1 tandem- and tridem-axle double-wheel set are 10, 18 and 22 tonnes, respectively. Based on this, Eq. 1  
 2 gives the formula for determining the LAS index for a certain pavement section:

$$3 \quad LAS = R_{overload}(T_{half})/R_{overload}(T) \quad (1a)$$

$$4 \quad R_{overload}(t) = \sum_{a \in A} \sum_{t'=0}^t n_{a,t'}^{overload} / \sum_{a \in A} \sum_{t'=0}^t n_{a,t'}^{tot} \quad (1b)$$

$$5 \quad A = \{\text{single, tandem, tridem}\} \quad (1c)$$

$$6 \quad f: ESAL \rightarrow t \quad (1d)$$

$$7 \quad T = f(ESAL_{end}) \quad (1e)$$

$$8 \quad T_{half} = f(ESAL_{end}/2) \quad (1f)$$

9 where  $R_{overload}(t)$  = the overload rate during the time period of 0 to  $t$ ;  $a$  = a specific axle type,  $a \in$   
 10  $A$ ;  $A$  = the set of axle types;  $n_{a,t'}^{overload}$  = the number of overloaded axles of axle type  $a$  at time  $t'$ ;  
 11  $n_{a,t'}^{tot}$  = the total number of axles of axle type  $a$  at time  $t'$ ;  $f$  = a mapping from  $ESAL$  to time  $t$ ;  
 12  $ESAL_{end}$  = the ESAL at the end point of the calculation range;  $T$  = the time at the end of the  
 13 calculation range;  $T_{half}$  = the time when ESAL is equal to half of the ESAL at the end point of the  
 14 calculation range.

15 Essentially, the LAS index is the ratio of the overload rate for the first half of ESALs to the  
 16 total overload rate for all ESALs. A simple rule is that LAS index less than one corresponds to the case  
 17 where the traffic load is first light and then heavy, and vice versa. In addition, LAS index can be  
 18 calculated for various calculation ranges, which allows to investigate the loading sequence effect on  
 19 pavement cracking performance at different service stages.

### 20 3.1.2 Modelling of field data

21 To explore the effect of load amplitude sequence on pavement cracking from massive and multi-source  
 22 field data, two popular ML algorithms, artificial neural network (ANN) and random forest regression  
 23 (RFR), were applied for modelling the relationships between the LAS index and other selected  
 24 influential factors with TCEI.

25 ANN models have been extensively used for pavement performance prediction because of their

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1 effectiveness in handling complex nonlinear relationships (Yao *et al.*, 2019; Guo *et al.*, 2021). These  
2 models are typically composed of many artificial neurons that are mutually connected. The  
3 connections are referred to as parameters or weights, reflecting the learnt knowledge from a dataset.  
4 Back-propagation was employed to train the ANN model which fine-tunes the parameters of the neural  
5 network depending on error rates acquired in each iteration. The optimum hyper-parameters in this  
6 study were determined through a simple grid search method which builds a model for every specified  
7 hyper-parameter combination and compares the performance of each model. The entire dataset was  
8 randomly divided into two groups: 80% for training and 20% for testing (Gholamy *et al.*, 2018). The  
9 mean squared error (MSE) was chosen as the loss function. The ANN model was built and tested on  
10 PyTorch, a well-known deep learning framework in Python (Van Rossum and Drake, 2009).

11 Random Forest (RF) is an ensemble technique that uses multiple decision trees to solve both  
12 regression and classification problems. It utilizes bagging and feature randomness in the creation of  
13 each individual tree in an attempt to generate an uncorrelated forest of trees whose prediction is more  
14 accurate than that of any individual tree. Therefore, RF is usually less likely to be over-fitting. In this  
15 study, the application of RFR algorithm was performed using the scikit-learn package in Python  
16 (Pedregosa *et al.*, 2011). The optimum set of hyper-parameters was found through random search  
17 which creates a grid of hyper-parameter values and picks random combinations to train and assess the  
18 model. This process was completed using the *RandomizedSearchCV* function in scikit-learn.

### 19 3.1.3 Model interpretation

20 The ML models were interpreted through the SHapley Additive exPlanations (SHAP) approach, which  
21 is a game-theoretic technique for explaining the output of any ML model (Lundberg and Lee, 2017).  
22 It is a unified framework for explanation models using additive feature attribution methods. SHAP  
23 specifies the explanation model as:

$$24 \quad g(z') = \phi_0 + \sum_{i=1}^M \phi_i z_i' \quad (2)$$

25 where  $g$  is the explanation model,  $\phi_0$  is the model output with all inputs absent which can be

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1 approximated by the average model predictions,  $z' \in \{0,1\}^M$  is the simplified features,  $M$  is the  
2 number of simplified input features, and  $\phi_i$  is the feature attribution for a feature  $i$ , i.e., the SHAP  
3 values. The SHAP value is computed by averaging the changes in conditional expectations over all  
4 possible feature orderings (Lundberg and Lee, 2017). It represents the responsibility of a feature for a  
5 change in the model output. In this study, the Python SHAP library was used to apply the SHAP  
6 method so as to explain the effect of loading amplitude sequence on the cracking performance of in-  
7 service asphalt pavements.

### 8 **3.2 Two-block SCB test**

9 The setup of the two-block SCB test includes a loading ramp at the top center of the specimen, and  
10 two support rollers on the bottom sides with a spacing of 120 mm, which was 0.8 times the diameter  
11 of the asphalt mixture specimen. Two pre-tests, SCB strength test and SCB constant amplitude fatigue  
12 test (Jiang *et al.*, 2018), were first conducted to determine the strength and fatigue life of the asphalt  
13 mixture under a single load amplitude, respectively. The SCB strength test was carried out under a  
14 constant pre-defined displacement rate of 50mm/min at room temperature of 25°C. Three replicated  
15 specimens were tested to obtain the load-displacement curves and the corresponding mean value and  
16 coefficient of variable (COV) of the tensile strength were calculated according to Eq. 3 and shown in  
17 Table 2. As for the SCB constant amplitude fatigue test, the loading frequency was determined to be  
18 10Hz with haversine waveform. One low stress ratio ( $\sigma_{low}$ ) of 0.135 and one high stress ratio ( $\sigma_{high}$ ) of  
19 0.190 were selected for testing. Three replicates were prepared for both testing conditions and the  
20 corresponding fatigue lives of the asphalt mixture are also exhibited in Table 2.

$$21 \quad \sigma_{max} = \frac{4.976F_{max}}{BD} \quad (3)$$

22 where  $\sigma_{max}$  = the tensile strength of specimen (MPa);  $F_{max}$  = the peak load of specimen (N); B = the  
23 height of specimen (mm); and D = the diameter of specimen (mm).

24 Table 2 Testing results of the SCB strength test and SCB constant amplitude fatigue test.

Tensile Strength (MPa)		Stress ratio	Stress amplitude (MPa)	Fatigue life (Cycles)	
Mean	COV			Mean	COV
5.321	9.0%	0.135	0.718	56,722	6.1%
		0.190	1.011	18,502	12.9%

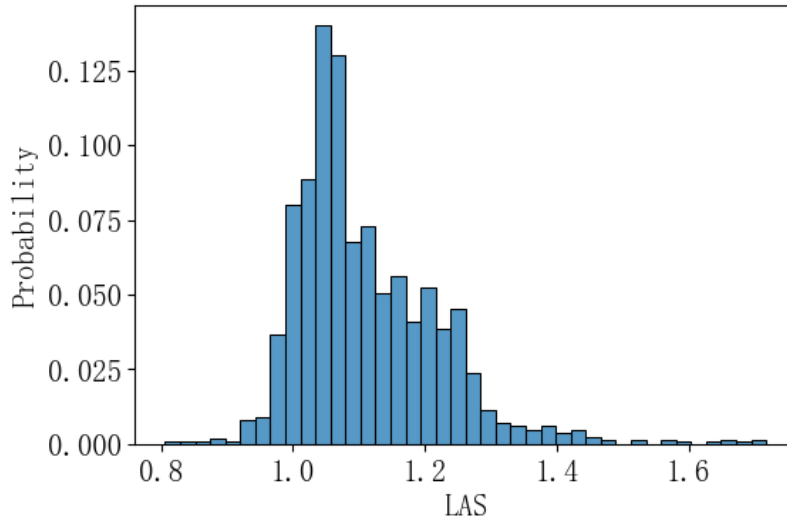
1 Two different loading sequences were considered for the two-block SCB tests, one from low  
2 to high stress ratios ( $\sigma_{low}-\sigma_{high}$ ) and the other in the opposite direction ( $\sigma_{high}-\sigma_{low}$ ). The loading sequence  
3 and waveform settings are the same as those of the SCB constant amplitude fatigue test. The cyclic  
4 loading number of the first block was 30% of the fatigue life of the asphalt mixture obtained from the  
5 SCB constant amplitude fatigue test. In the second block, the specimen was continuously loaded until  
6 fatigue failure. Three replicates were tests for each loading sequence.

## 7 **4 Results and Discussion**

### 8 **4.1 Field validation**

#### 9 *4.1.1 Graphical display of the loading sequence effect*

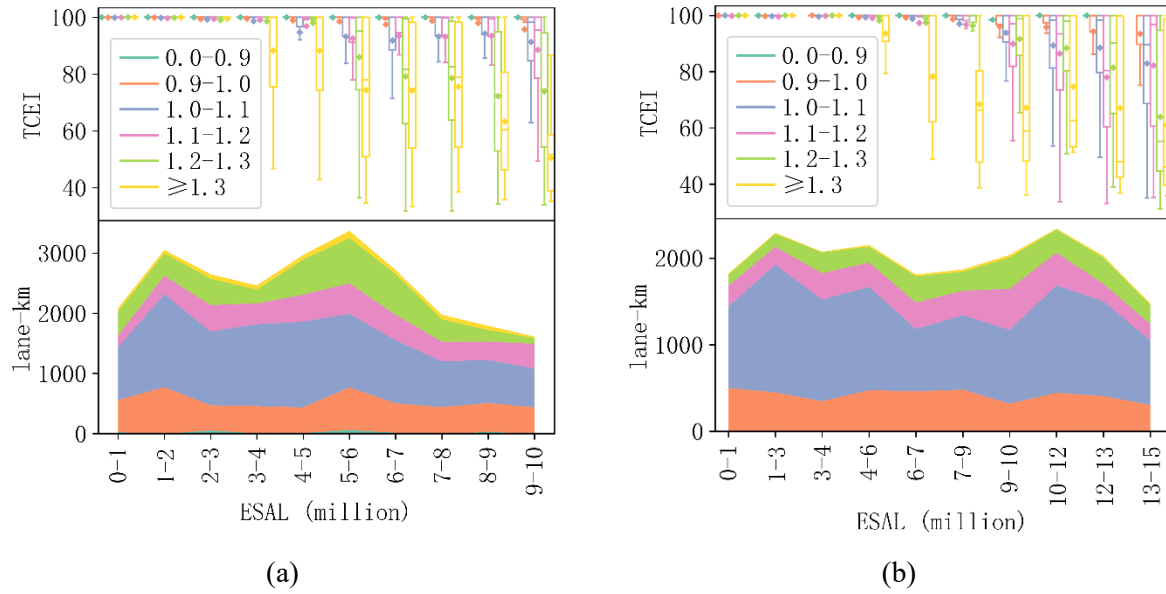
10 Although the LAS index can be calculated for different service stages, this study aims to explore the  
11 long-term effect of loading sequence on pavement cracking performance. Meanwhile, it is believed  
12 that the loading sequence effect would become obvious only after a relatively long period of service.  
13 Therefore, only calculation ranges of more than 10 years were considered in the subsequent modelling  
14 process. In other words, pavement segments that have been maintained before the tenth year or that  
15 have been in service for less than ten years were excluded. For segments with more than ten years of  
16 service, the time at the end of the calculation range need to be outside the tenth year. Figure 4 shows  
17 the distribution of the LAS index. It is obvious that a considerable percentage of the pavement  
18 segments have a higher overload rate in the early years, resulting in a LAS index greater than one. This  
19 is consistent with the situation in Jiangsu, where the overload rate was initially high but was later  
20 effectively controlled, resulting in a reduction in the overload rate.



1

2 Figure 4. Distribution of the LAS index.

3 A graphical display of the loading sequence effect on pavement cracking propagation was  
 4 provided in Figure 5. Figure 5(a) shows the calculated LAS index considering the range of ESAL from  
 5 0 to 5-10 million (i.e., the ESAL at the end point of the calculation range is between 5-10 million)  
 6 while Figure 5(b) is for the range of ESAL from 0 to 10-15 million. The top half of Figure 5(a) and  
 7 (b) displays the deterioration of pavement cracking condition with ESAL for different LAS groups.  
 8 The box plots were used to illustrate the TCEI distribution for each ESAL and LAS combination,  
 9 which allows for multi-dimensional comparisons such as mean (the diamond symbol), median (the  
 10 horizontal line in the box) and variation (the height of the box). The total length of the pavement  
 11 segments corresponding to each combination of ESAL and LAS is presented in the bottom of Figure  
 12 5(a) and (b), implying the sample size utilized to support the results. It can be observed that a larger  
 13 LAS value tends to increase the TCEI deterioration rate. This suggests that different load amplitude  
 14 sequences do have an effect on asphalt pavement cracking, which motivated the further analysis of the  
 15 contribution of the LAS index to pavement cracking through advanced ML modeling and interpretation  
 16 techniques afterwards.



1 Figure 5. Deterioration of pavement cracking condition for different LAS values and calculation  
 2 ranges: (a) in the range of ESAL from 0 to 5-10 million and (b) in the range of ESAL from 0 to 10-  
 3 15 million.

#### 4 4.1.2 Importance of LAS in pavement cracking prediction

5 To examine the importance of LAS in pavement cracking prediction, the accuracy of the prediction  
 6 models built based on the two ML algorithms were assessed first. Three metrics, including the  
 7 coefficients of determination (R-square), mean absolute error (MAE), and root mean square error  
 8 (RMSE), were employed, as shown in Table 3. The R-square values of the two models with LAS  
 9 reached above 0.85 on the training set and exceeded 0.76 on the test set. The scatter plots in Figure 6  
 10 indicate that the majority of the points are densely distributed around the line of equality, which  
 11 represents the most ideal condition, i.e., the predicted results are exactly equal to the measured results.  
 12 Therefore, it can be concluded that both models have relatively high accuracy and are able to model  
 13 the relationship between pavement cracking condition and load amplitude sequence and other factors  
 14 very well.

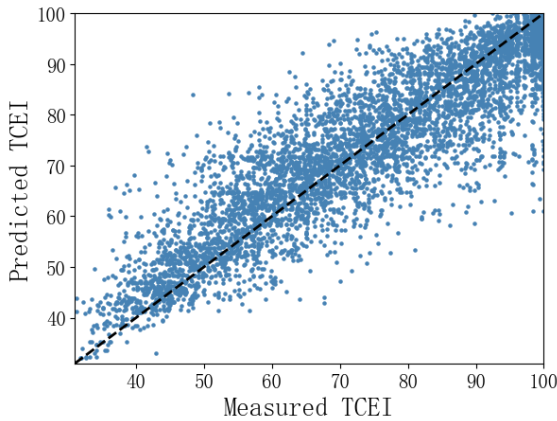
15 Moreover, two more models excluding the LAS index but including all other factors were

1 developed. The evaluation results are also shown in Table 3. It can be found that the performances of  
 2 both ANN and RFR models are slightly improved after adding the LAS index. Therefore, LAS has a  
 3 certain contribution to the prediction of pavement cracking. In addition, the RFR model slightly  
 4 outperforms the ANN model. Hence, in the subsequent analysis, the results of the RFR model were  
 5 interpreted to examine the effect of loading sequence on pavement cracking.

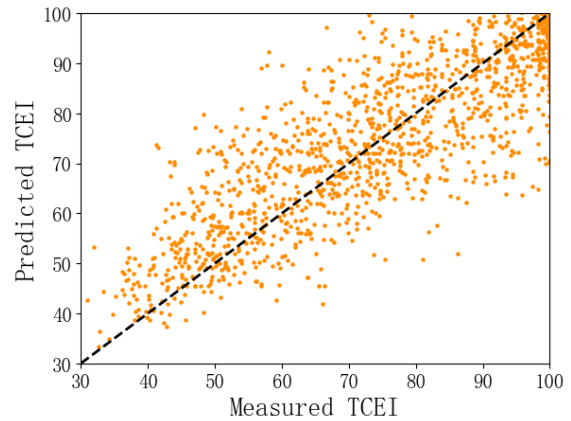
6 Table 3 Model evaluation results.

Dataset	Evaluation metrics	ANN			RFR		
		Without LAS	With LAS	Improvement (%)	Without LAS	With LAS	Improvement (%)
Training	R-square	0.8442	0.8541	1.17	0.8813	0.8836	0.26
	MAE	5.4839	5.2891	3.55	4.6660	4.6029	1.35
	RMSE	7.7317	7.4820	3.23	6.7494	6.6847	0.96
	Sample size	6895					
Testing	R-square	0.7495	0.7517	0.29	0.7902	0.7916	0.18
	MAE	7.2086	7.1888	0.27	6.3703	6.3240	0.73
	RMSE	9.8510	9.8073	0.45	9.0133	8.9835	0.33
	Sample size	1700					

7

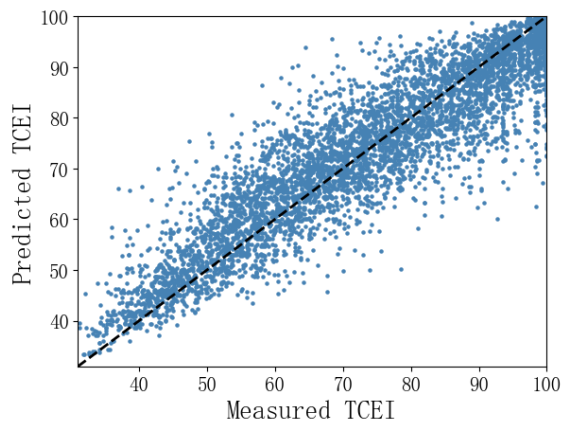


(a)

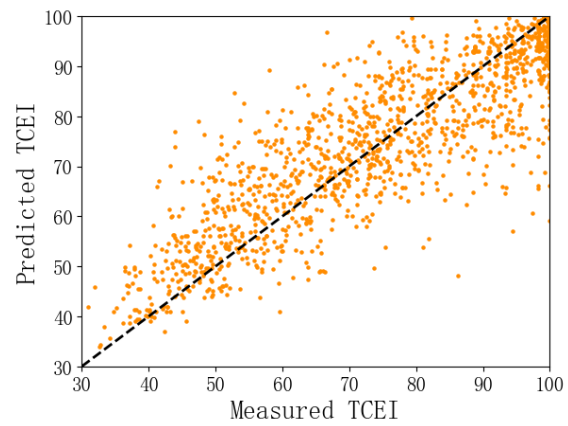


(b)





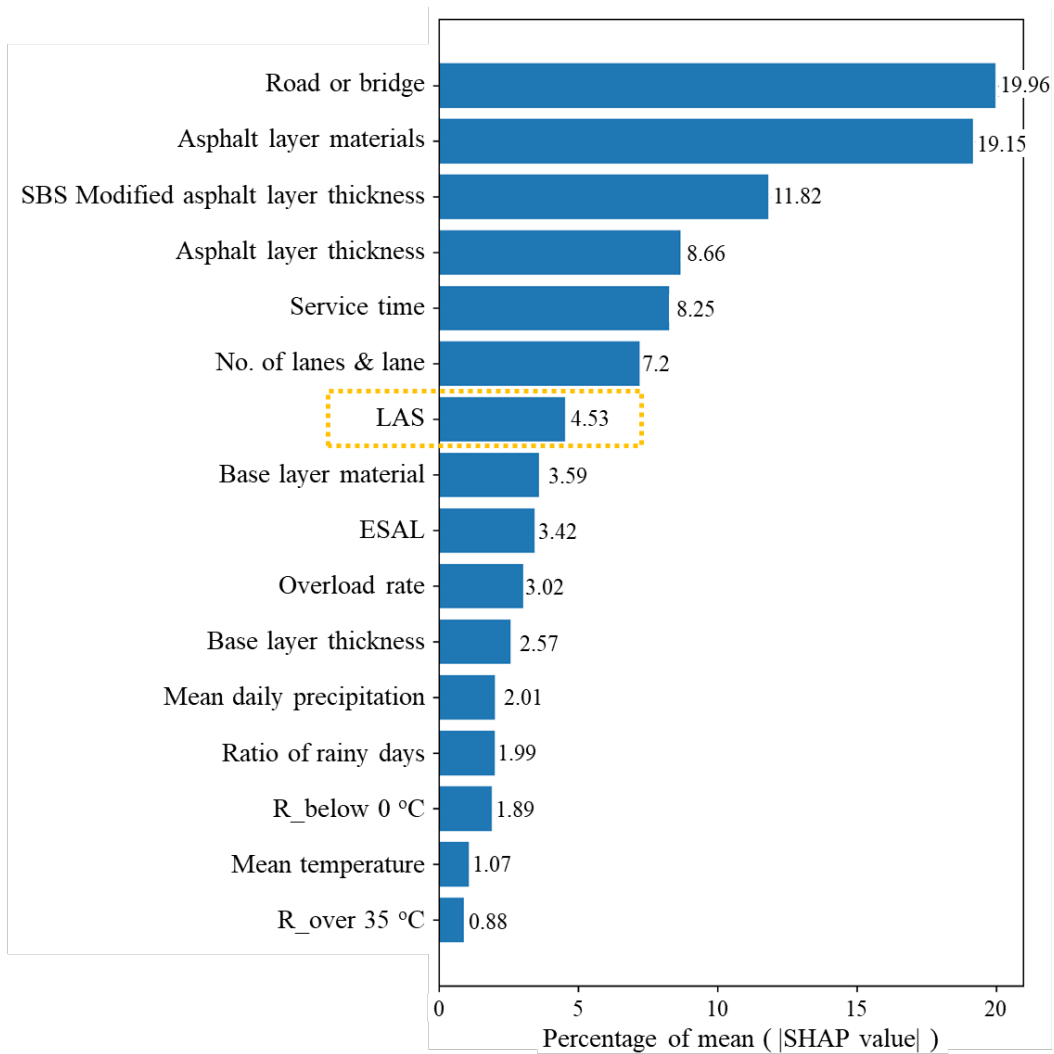
(c)



(d)

1 Figure 6. Measured against predicted TCEI values: (a) training data of ANN model, (b) testing data  
 2 of ANN model, (c) training data of RFR model, and (d) testing data of RFR model.

3 SHAP estimates the global importance of a feature as the average of the absolute SHAP values  
 4 for each feature across the data. The higher the mean absolute value of SHAP, the more important the  
 5 variable is. Figure 7 normalizes the SHAP values by calculating the percentage of the mean absolute  
 6 SHAP values for each feature. The features are ranked from the most important to the least important.  
 7 As can be seen in Figure 7, the location of the pavement (road or bridge) and the structural and material  
 8 properties of the asphalt pavement layer have the greatest influence on the long-term pavement  
 9 cracking performance. This is because reflective cracking is one of the major distresses of semi-rigid  
 10 base asphalt pavements. Hence, road pavements with semi-rigid base usually have more transverse  
 11 cracks than bridge pavements with steel or concrete deck base. The performance of asphalt layers also  
 12 significantly affects the speed of upward propagation of transverse cracks. Among the three traffic-  
 13 related indicators, the LAS index contributed the most in forecasting long-term pavement cracking  
 14 conditions, even more than the common traffic indicators such as ESAL and overload rate. This  
 15 demonstrates the importance of including loading sequence metrics in pavement performance models.  
 16



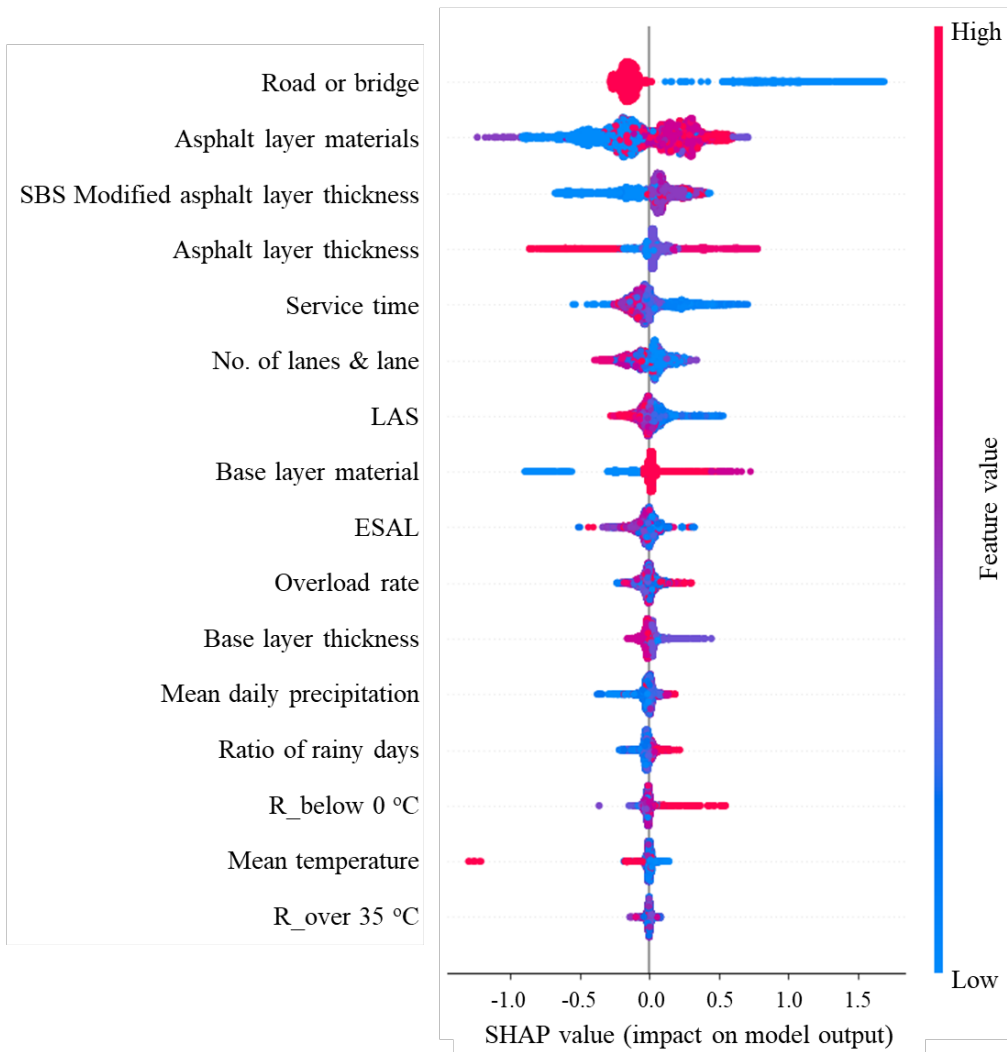
1

2 Figure 7. SHAP importance plot.

3 *4.1.3 The effect of LAS on pavement cracking condition*

4 Figure 8 depicts the SHAP values of every feature for every data sample, where the features are ranked  
 5 from top to bottom according to their importance. The position of the point on the horizontal axis is  
 6 determined by the SHAP value, and the colour represents the value of the feature, with red being high  
 7 and blue being low. The SHAP value could be regarded as the marginal contribution of every feature  
 8 for every data sample. Thus, Figure 8 illustrates how different values of each feature would affect the  
 9 model output. For example, a thicker SBS modified asphalt layer increases the predicted TCEI value,  
 10 which corresponds to a milder cracking condition. Moreover, a higher LAS index lowers the predicted

1 TCEI value, i.e., the traffic load of first heavy and then light will aggravate pavement cracking.  
 2 Conversely, a light-to-heavy loading sequence prolongs pavement service life. This provides a basis  
 3 for transport agencies to develop vehicle load limit policies, especially for newly built or maintained  
 4 road pavements. Meanwhile, Figure 8 also indicates that after ten years of pavement service, the  
 5 negative effects of heavy ESALs and overload rates on pavement cracking become insignificant, but  
 6 the negative effects of large LAS values are quite obvious. This also emphasizes the importance of  
 7 including loading sequences in long-term pavement performance predictions.

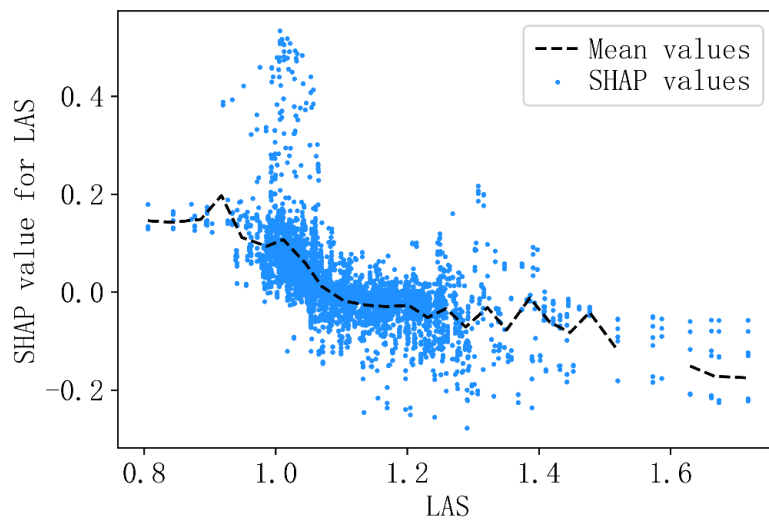


8

9 Figure 8. SHAP summary plot.

10 Figure 9 shows a scatter plot of SHAP values versus LAS index values for all samples in the

1 dataset. It implies the effect of the LAS index on the model output throughout the whole dataset. As  
2 SHAP value represents the contribution of a feature to the change in the model output, the plot below  
3 depicts the change in TCEI values as the LAS index changes. A significant negative correlation can  
4 be observed in Figure 9. When the LAS index is less than one, the SHAP value tends to increase  
5 slightly with decreasing LAS, implying that a lower LAS index may improve the cracking performance  
6 of the pavement. When the LAS index is greater than one, the SHAP value decreases sharply with  
7 increasing LAS, indicating that early heavy traffic loading will significantly jeopardize the long-term  
8 cracking performance of the pavement.

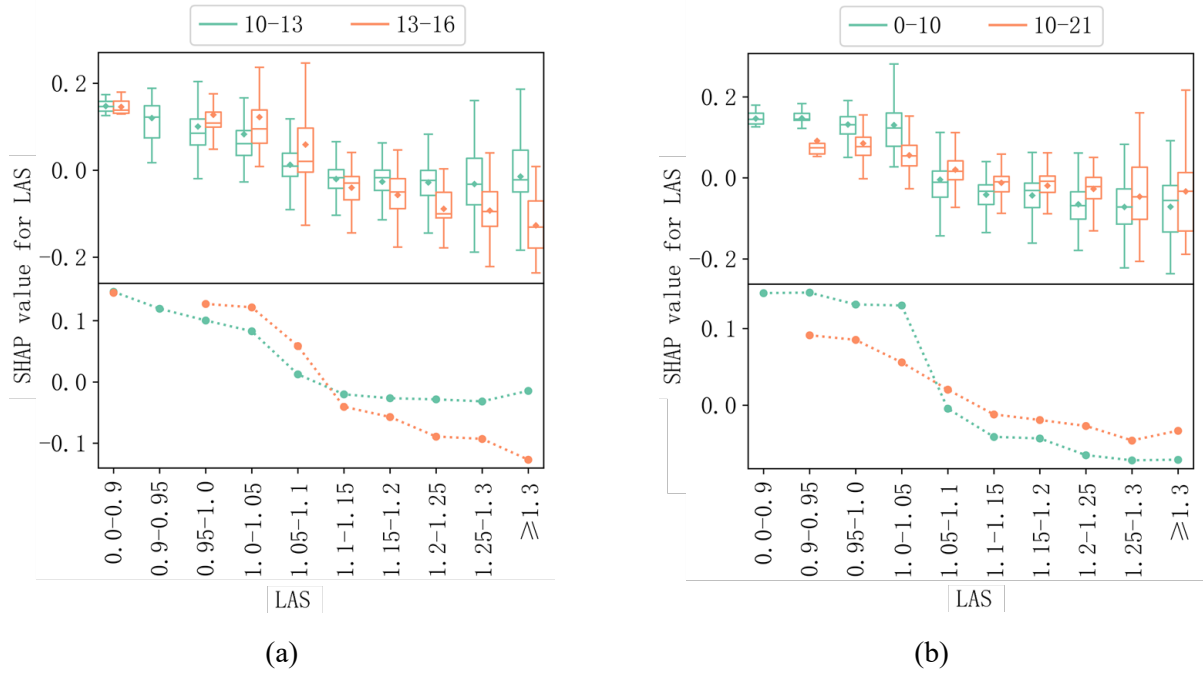


9

10 Figure 9. SHAP dependency plot for the LAS index.

11 The vertical dispersion in Figure 9 indicates the interactions of the LAS index with other  
12 features. To illustrate these interactions more clearly, the interacting variables and LAS index were  
13 first divided into groups. The vertical distribution of SHAP values for each group is then plotted using  
14 a box plot, as shown in Figure 10. The bottom half of Figure 10 is a line graph of the mean SHAP  
15 values, corresponding to the positions of the diamond symbols in the top half of Figure 10. It can be  
16 found that the effect of LAS index on the pavement cracking condition is greater for the road sections  
17 with relatively long service time and thin SBS modified asphalt layers. In other words, segments with  
18 longer service time were more sensitive to the traffic loading sequence. The modification of asphalt

1 mixtures may mitigate the adverse impacts of heavy traffic loads in early stages.



2 Figure 10. Interaction effects between the LAS index and (a) service time and (b) SBS modified  
 3 asphalt layer thickness.

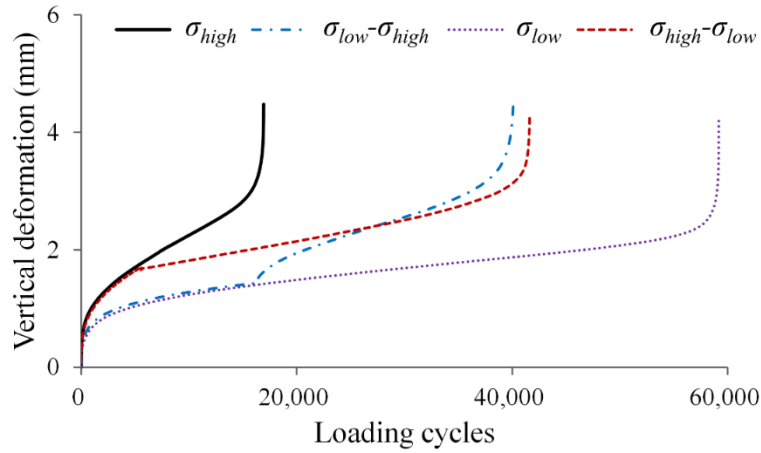
#### 4 4.2 Investigation of the loading sequence effect in laboratory

##### 5 4.2.1 Fatigue curves of the two-block SCB test

6 Figure 11 illustrates the fatigue curves obtained in the SCB constant amplitude fatigue test at two stress  
 7 ratios and in the two-block SCB test at two loading sequences. The vertical deformation curves of SCB  
 8 specimens exhibit three stages under constant amplitude cyclic loading conditions: firstly, they  
 9 accumulate rapidly with increasing loading cycles, then they grow steadily at an almost constant rate,  
 10 and finally they accelerate in a non-linear mode until specimen failure. The fatigue failure criterion  
 11 was the inflection point of the secondary and tertiary stage. It can be found that, in the first block, the  
 12 deformation curves of the two-block SCB test and the SCB constant amplitude test at the same stress  
 13 ratio almost overlap. In the second block, the deformation curves with loading sequences of  $\sigma_{high}-\sigma_{low}$   
 14 and  $\sigma_{low}-\sigma_{high}$  have much lower and higher growth rates than those with loading sequences of  $\sigma_{high}$  and

1  $\sigma_{low}$ , respectively.

2



3

4 Figure 11. Fatigue curves of asphalt mixture specimens under different loading conditions.

5 4.2.2 Non-linear fatigue damage accumulation

6 In the two-block SCB fatigue test, applying  $N_1$  cycles with a stress amplitude of  $\sigma_1$  to specimen with a  
7 corresponding fatigue life endurance of  $N_{f\sigma_1}$ , is equivalent to consuming  $N_1/N_{f\sigma_1}$  of the fatigue  
8 resistance (Schijve, 2009). This assumption also holds for the second block, so the accumulated  
9 damage variable ( $D_{sum}$ ) was defined as the sum of  $N_1/N_{f\sigma_1}$  and  $N_2/N_{f\sigma_2}$ . Table 4 presents the  $D_{sum}$   
10 values of asphalt mixture specimens under two different loading sequences. According to the classic  
11 Miner's rule,  $D_{sum}$  should be equal to one under the linear cumulative damage hypothesis. However,  
12 the  $D_{sum}$  values of both loading sequences are not equal to one, suggesting that the asphalt mixture  
13 presents a non-linear fatigue damage accumulation characteristic. The  $D_{sum}$  value is less than one when  
14 the loading sequence is  $\sigma_{high}-\sigma_{low}$ , otherwise, the  $D_{sum}$  value is greater than one. This implies that a  $\sigma_{low}-$   
15  $\sigma_{high}$  sequence with  $D_{sum}$  greater than one may prolong the longevity and delay the crack propagation  
16 of asphalt mixtures. The results of the laboratory tests were consistent with the field validation results,  
17 which further demonstrated the effect of loading sequence on the cracking performance of asphalt  
18 pavements.

19 Table 4  $D_{sum}$  of the asphalt mixture under two loading sequences.

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Loading sequence	$N_1$	$N_2$	$N_{f\sigma 1}$	$N_{f\sigma 2}$	$D_{sum}$
$\sigma_{high}-\sigma_{low}$	5,080	36,563	18,502	56,722	0.918
$\sigma_{low}-\sigma_{high}$	17,751	27,124	56,722	18,502	1.902

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1 **4.3 Discussion**

2 By combining the results of field and laboratory investigations, it can be concluded that a light-to-  
3 heavy loading sequence could prolong pavement service life, whereas a heavy-to-light sequence is  
4 detrimental to pavement cracking performance and may shorten the fatigue life of asphalt mixtures.  
5 Both field and laboratory results indicate that transport agencies need develop effective policies to  
6 prohibit the concentration of heavy traffic loads on individual road segments in the early stages of  
7 pavement service (i.e., after new construction or maintenance). Moreover, for long-term pavement  
8 cracking performance, the effect of loading sequence is more significant than the number of loading  
9 repetitions and overload rate. Its negative effects can be further exacerbated by longer service time and  
10 thinner modified asphalt layers. Hence, more attentions should be paid to segments with high LAS  
11 values, long service time, and thin modified asphalt layers to ensure timely maintenance.

12 **5 Conclusions**

13 In this study, the traffic loading sequence effect on the cracking performance of semi-rigid base asphalt  
14 pavements was investigated from both field and laboratory perspectives. Field validation was  
15 performed by applying simple graphic displays and advanced ML techniques to extract useful  
16 information from field pavement performance data. The two-block SCB tests were then conducted to  
17 further validate the loading sequence effects on the non-linear fatigue damage accumulation of asphalt  
18 mixtures.

19 A load amplitude sequence (LAS) index, built upon the variation of axle overload rates over  
20 the analysis period, was proposed and proved to be effective in characterizing the traffic loading  
21 sequence of in-service asphalt pavements. The graphic displays of the field pavement performance  
22 evolution under various combinations of LAS and ESAL levels demonstrate that a larger LAS value

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1 would increase the deterioration rate of pavement transverse cracking.

2 Both the ANN and RFR models have a relatively high accuracy, with the RFR model  
3 marginally outperforming the ANN model. The incorporation of the LAS index slightly improved the  
4 performance of the two models. The LAS index ranks high in the importance plot of the RFR model  
5 and is even more important than the other two traffic-related variables, indicating that the loading  
6 sequence has a significant impact on the prediction and development of pavement cracking conditions.  
7 The SHAP value analysis confirms that the heavier traffic loads in early stages are detrimental to the  
8 long-term pavement cracking performance. Moreover, this effect will be further exacerbated for  
9 pavement segments with longer service time or thinner SBS modified asphalt layers.

10 The  $D_{sum}$  values of asphalt mixtures under the loading sequence of  $\sigma_{high}-\sigma_{low}$  and  $\sigma_{low}-\sigma_{high}$  are  
11 greater and less than one, respectively, indicating that loading sequence starting with a higher stress  
12 may shorten the fatigue life of the asphalt mixture. In contrast, a light-to-heavy loading sequence would  
13 prolong the longevity of the asphalt pavement, which is consistent with the field validation results.

14 Finally, despite the contributions of this study, there are still some limitations that could be  
15 addressed in future work. For example, more complex load amplitude sequence indexes can be  
16 developed to characterize the entire time series of field traffic loads. Accordingly, more loading  
17 conditions may be considered in the variable amplitude fatigue test to prompt the better understanding  
18 of the non-linear fatigue damage accumulation of asphalt mixture.

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1 **Disclosure statement**

2 No potential conflict of interest was reported by the authors.

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