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Discussion of "Study on Asphalt-Cement Materials for Seismic Isolation 1 Layer of Shield Tunnels" by Qi Yang, Ping Geng, Liangjie Wang, Bingbing 2 Zhao, and Pingliang Chen. (DOI:10.1061/(ASCE)MT.1943-5533.0004466) 3 4 Xi Jiang, Ph.D., M.ASCE 5 6 Research Scientist, Dept. of Civil and Environmental Engineering, University of Tennessee, Knoxville, TN 37996. Email: xjiang29@vols.utk.edu 7 8 Yumeng Zhang, Ph.D., M.ASCE 9 Postdoctoral Fellow, College of Civil Engineering, Tongji University, Shanghai, 200092, 10 China. Email: zhangym@tongji.edu.cn 11 12 Jiwang Jiang, Ph.D., M.ASCE 13 14 Postdoctoral Research Fellow, 422 School of Transportation, Southeast University Rd., Jiangning District, Nanjing, Jiangsu 211189, China. 15 16 Email: jiang jiwang@hotmail.com 17 Xuehui Zhang, Ph.D., M.ASCE 18 Postdoctoral Research Fellow, Department of Geoscience and Engineering, Delft University 19 of Technology, Delft, the Netherlands. 20 21 Email: X.Zhang-10@tudelft.nl 22 Zhen Leng, Ph.D., M.ASCE 23 Associate Professor, Dept. of Civil and Environmental Engineering, Hong Kong Polytechnic 24 University, Hung Hom, Kowloon, Hong Kong. 25 26 ORCID: https://orcid.org/0000-0002-7797-1134. Email: zhen.leng@polyu.edu.hk 27 28

29 The authors have presented a comprehensive investigation on asphalt-cement (A-C) materials for seismic isolation layer of shield tunnels based on laboratory tests and numerical simulations. 30 The physical and mechanical properties of the A-C materials such as fluidity, consistency, and 31 ultimate compressive strength were studied and the influence of the mass ratio of 32 cement/asphalt on these properties was investigated as well. The results show that the fluidity, 33 consistency, and compressive strength of A-C materials increased with the content of cement % 34 35 (by weight). In addition, the cement/asphalt mass ratio of 50% was considered the optimum for the seismic isolation layer since experimental results revealed no obvious deformation was 36 37 found before peak stress, and few cracks on the specimens' surface were observed after the loading process. Then, the A-C materials with a 50% ratio of cement/asphalt were further 38 investigated by using FLAC 3d numerical simulations, in which the A-C materials were applied 39 40 to a field shield tunnel (Shantou Bay Undersea Tunnel) with an outer diameter of 14.0 m 41 located in a hard-soft stratum. In the numerical simulation, the EI Centro earthquake wave (3.12 Hz), the Wenchuan earthquake wave (1.02 Hz), and the Artificial earthquake wave (1.47 42 Hz) were used to investigate the anti-seismic capacity of the A-C-based isolation layer in the 43 shield tunnel. The horizontal displacement and principal stress of the segmental linings were 44 studied to evaluate the effectiveness of the seismic isolation layer. The simulation results show 45 that the A-C based seismic isolation layer could significantly reduce the maximum principal 46 stresses of the tunnel near the hard-soft stratum junction. And the reasonable fortified length 47 of the A-C seismic isolation layer in this study was 3.5 times the tunnel diameter from the 48 stratum junction to both sides. The discussers highly appreciate the work of the authors and 49 would like to provide some comments regarding the experimental process, results, and analysis. 50 51 Synchronous backfill grouting is of great importance to the safety of shield tunnelling. Many construction accidents of shield tunnelling are due to improper grouting, especially in water-52

rich ground strata, resulting in water inrush, mud bursting, leakage, corrosion, segments 53 faulting, and even a disastrous tunnel collapse (Liang et al. 2022; Ye et al. 2020, 2021; Ying et 54 al. 2022). In this study, the authors used a cationic fast-cleft and slow-coagulate emulsified 55 asphalt to make A-C samples. The discussers recommended the authors explain why you chose 56 cationic emulsified asphalt to make seismic isolation layer. Based on the previous literature, 57 the asphalt emulsion type has a significant effect on the properties of cement-emulsified asphalt 58 59 mortar (CEAM) (Jiang et al. 2021). The cationic emulsified asphalt-based CEAM would have a low elastic modulus and strengths. And the anionic emulsified asphalt-based CEAM exhibits 60 61 a relatively high elastic modulus and better mechanical performance (Wang et al. 2015). Therefore, specifying the rationale for choosing emulsified asphalt type could provide a 62 valuable reference for other similar studies. 63

The auxiliary additives such as water reducer, defoamer, and viscosity modifying agent play an important role in controlling the properties of CEMA. In this study, the 8013HPWR earlystrength & high-performance water reducer was used to make testing specimens. It is worthwhile that the authors could explain how to choose the auxiliary additives like superplasticizers in this study to guarantee the stable and proper performance of the CEMAbased isolation layer in the shield tunnelling.

The mechanical properties of A-C based grouting materials depend on the hydration of cement and the demulsification of asphalt emulsion. The above interactive and counterbalancing process results in the characteristics of the final phased CEAM. Therefore, the preparation technology is imperative to the performance of the CEAM-based seismic isolation layer. The agglomeration of emulsified asphalt, cement particles, and other raw materials should be avoided. In addition, the sequences in which the different materials are added are also critical. The feeding (preparation) order should be taken care of to minimize the direct contact of emulsified asphalt and dry cement particles to avoid emulsified asphalt demulsifying in advance, and cement and sand are wrapped in the asphalt membrane. Therefore, could the authors introduce the experience of how to ensure the properties of A-C materials during specimen preparation?

The size effect of specimens on the properties of CEAM-based materials also needs to be 81 82 focused on (Jiang et al. 2023). The nominal strength of laboratory-size specimens differs from that of larger structural members used in real construction structures (Kim and Yi 2002). The 83 difference in the nominal strength is a direct consequence of energy release into a finite-size 84 fracture process zone. The size effect is quite apparent in the compressive failure of quasi-85 brittle materials such as concrete. Therefore, it is worth studying the size effect in cementitious 86 materials. In this study, 70.7 mm×70.7 mm×70.7 mm cubic A-C samples were used to conduct 87 properties tests. Will the properties of CEAM in the backfill grouting of actual shield tunnelling 88 construction match the laboratory test results? Do we need to introduce surplus coefficients to 89 ensure the quality of CEAM during the practical application? The discussers believe the authors 90 could provide a reasonable explanation for this question. 91

The grouting mechanism, especially the diffusion theory of penetration grouting in shield 92 93 tunnelling is of great importance to the safety and stability of shield tunnelling (Li et al. 2022a; b; Liu et al. 2021). When the grouts are injected into the ground, it triggers soil expansion and 94 95 excess pore water pressure which significantly disturb the surrounding area of the shield tunnel. In addition, the interface between the soil and grouts changes with the ongoing diffusion of 96 pressurized grouts, influencing the stability of the shield tail voids and further negatively 97 affecting the safety of shield tunnelling. Therefore, reliable grouts diffusion mechanisms shall 98 be developed to address the aforementioned issues. In this study, the diffusion properties of the 99 A-C based materials were not considered to simplify the simulation analysis. However, 100

improper control of grouts diffusion behind the segmental linings may result in safety concerns, and inadequate grouting could negatively affect the grouting quality, weakening the antiseismic ability of the A-C based seismic isolation layer in the shield tunnelling. Therefore, the diffusion theory of penetration grouting in shield tunnelling is recommended to be considered in the future study, contributing to the accuracy of numerical simulations. The discussers would like to ask for opinions on this aspect.

The practical application value of the A-C based backfill grouts should be the priority 107 consideration in this study. The matching criteria between the properties of grouts and the 108 corresponding geological conditions should be established. In this study, the hard-soft stratum 109 was used as the geological condition to numerically investigate the anti-seismic function of the 110 A-C materials during shield tunnelling. However, the authors did miss the critical geological 111 information, such as the seismic conditions of the project site (Shantou Bay area). And what is 112 the relationship between earthquake frequency and geology? The clarification could help add 113 practical value to this study. In addition, is the A-C material suitable for real shield tunnelling 114 construction? Will the A-C based grouts pollute the grouting pipes and surrounding formations? 115 The pumpability of the grouts also determines the grouting quality, influencing the quality of 116 the seismic isolation layer. The discussers believe the authors could provide a reasonable 117 explanation for these questions. 118

Shield tunnelling has been the dominant tunnel construction method for many countries such as Japan, the United States, and China, especially in soft soil areas, due to its advantages of a fast construction schedule, low disturbance to the surrounding environment, and a high-level automation (Huang et al. 2022a; b; Zhang et al. 2022). The authors' research is of great value to the technical advances and promotion of shield tunnelling technology. The discussers believe

- the authors would complete more comprehensive and valuable studies after reviewing and
- answering the above discussions and questions.

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