

1                    **Enhancing de/hydrogenation kinetics properties of the Mg/MgH<sub>2</sub>**  
2                    **system by adding ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) alloys via ball milling**  

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1 **Abstract**

2 Magnesium (Mg)-based alloys have already been widely studied as the hydrogen storage materials  
3 because of their high reversible hydrogen storage capacity, low cost, and light weight, etc. However, the  
4 poor de/hydrogenation kinetic properties dramatically hinder the practical applications. In this work, the  
5  $MgH_2-ANi_5$  (A = Ce, Nd, Pr, Sm, and Y) composites have been prepared by a high-energy ball milling,  
6 which can effectively refine the particle size thus improving the kinetic properties. Experimental results  
7 reveal that the  $MgH_2-ANi_5$  composites mainly consist of  $Mg_2NiH_4$ ,  $MgH_2$  and Rare earth (RE) hydride,  
8 which will be dehydrogenated to form  $Mg_2Ni$ , Mg and stable RE hydride reversibly. Accordingly, the  
9 as-milled  $MgH_2-ANi_5$  (A = Ce, Nd, Pr, Sm, and Y) composites with various A-elements can respectively  
10 contribute a reversible hydrogen storage capacity of 6.16 wt%, 5.7 wt%, 6.21 wt%, 6.38 wt%, and 6.5 wt%  
11 at a temperature of 300 °C, and show much better kinetic properties in comparison with the pure  $MgH_2$   
12 without any additive. In-situ formed  $Mg_2Ni$  and stable RE hydride (such as  $CeH_{2.73}$  and  $YH_2$ ) might act as  
13 effective catalysts to significantly improve the hydrogen storage properties of  $MgH_2$ . The present work  
14 provides a guideline on improving the kinetic properties of the Mg-based hydrogen storage alloys.

15 **Keywords:** Mg-based hydrogen storage alloy; kinetic properties;  $ANi_5$ ; Additives;

16

## 1 **1. Introduction**

2 Hydrogen is one of the most promising clean energy resources because of its high energy density,  
3 environmental friendliness, and renewability.<sup>[1]</sup> However, there is a huge challenge to store and transport  
4 hydrogen. Apart from the hydrogen storage in gaseous and liquid states, solid-state hydrogen storage has  
5 been considered as the most reliable safe and practical solution.<sup>[2-4]</sup> In particular, Magnesium (Mg)-based  
6 alloys are considered one of the most promising solid-state hydrogen storage materials due to their high  
7 hydrogen storage capacity (e.g., 7.6 wt% in the case of MgH<sub>2</sub>), abundance, low cost and light weight.<sup>[5]</sup>  
8 Nevertheless, the high thermodynamic stabilities ( $\Delta H = 75$  kJ/mol), sluggish kinetics ( $E_a = 156$  kJ/mol)  
9 and poor reversible cycling properties greatly hinder their practical applications.<sup>[6, 7]</sup> For example, the  
10 catalyst-free MgH<sub>2</sub> starts to desorb hydrogen at a temperature as high as 350 °C with rather slow kinetics  
11 due to the existence of a surface oxide layer<sup>[8]</sup> and the quite small H diffusion coefficient between Mg and  
12 MgH<sub>2</sub>.<sup>[7, 9]</sup>

13 In order to overcome these drawbacks, numerous efforts have been made to enhance the hydrogen  
14 storage performance of MgH<sub>2</sub>, such as the addition of catalysts to enhance the kinetic properties,<sup>[10, 11]</sup> the  
15 combination of metal or metal hydride to improve the thermodynamic stabilities,<sup>[12, 13]</sup> and the reduction of  
16 particle size, etc. Particularly, additives or catalysts have been explored extensively because of their striking  
17 effects in improving the hydrogen storage performance of MgH<sub>2</sub>.<sup>[14, 15]</sup> Accordingly, combining MgH<sub>2</sub> with  
18 additives or catalysts such as metal,<sup>[16]</sup> hydrides,<sup>[17, 18]</sup> metal halides,<sup>[19, 20]</sup> metal oxides,<sup>[11, 21, 22]</sup>  
19 carbon-based materials<sup>[23, 24]</sup> and nanosized alloys<sup>[25]</sup> have been explored. More specifically, adding some  
20 transition metals, which are located in Group IIIB-VB and Period 4-6 in the period table, can enhance the  
21 ability to form stable hydrides under relatively moderate temperature and pressure,<sup>[26-28]</sup> and also enhance  
22 hydrogen storage kinetic properties. For example, G. Liang, et al.<sup>[29]</sup> studied the effect of the addition of

1 LaNi<sub>5</sub> on the hydrogen storage properties of mechanically milled MgH<sub>2</sub>/Mg, finding that the ternary  
2 Mg–Ni–La alloy has much better absorption and desorption kinetics than the binary Mg–La and Mg–Ni  
3 alloys. Pavel et al.<sup>[30]</sup> synthesized nanocomposites of MgH<sub>2</sub>-transition metallic hydrides (ScH<sub>2</sub>, YH<sub>3</sub>, TiH<sub>2</sub>,  
4 ZrH<sub>2</sub>, VH, and NbH), demonstrating that these transition metallic hydrides can not only lead to the easier  
5 combination of hydrogen atoms during desorption but also form coherent interfaces between MgH<sub>2</sub> and  
6 transition metallic hydrides that favor the later nucleation. Ouyang et al.<sup>[31]</sup> prepared the CeH<sub>2.73</sub>-MgH<sub>2</sub>-Ni  
7 nanocomposites with in-situ formed stable CeH<sub>2.73</sub> which can catalyze the hydriding/dehydriding process  
8 by combining with Ni to Mg/MgH<sub>2</sub>. Notably, this in-situ formed nanocomposites structure can effectively  
9 suppress Mg/MgH<sub>2</sub> grain growth and enable the material to maintain its high performance after more than  
10 500 cycles. In addition, the primary-precipitated metal Mg phase on the surface of MgH<sub>2</sub> can act as  
11 nucleate precursors and CeH<sub>2.73</sub> remains stable during absorption/desorption process, serving as a hydrogen  
12 pump, which is similar to the dehydrogenation steps and factors controlling desorption kinetics of Mg-Ce  
13 hydrogen that was referred by Xie et al.<sup>[32]</sup> It has also been found that RE-based alloy co-doping Ce-Y  
14 fabricated by Yong et al.<sup>[33]</sup> can release hydrogen completely in 42 min at 340 °C, 100 min at 320 °C, 320  
15 min at 300 °C, respectively. While Zhang et al.<sup>[34]</sup> reported that MgH<sub>2</sub>-5 wt%Ni<sub>3</sub>C composites can release  
16 the hydrogen of 6.3 wt%, 6.2 wt% and 3.3 wt% in 20 min at 325 °C, 300 °C, and 275 °C, respectively.

17 The above description indicates clearly that the addition of suitable catalysts, especially the transition  
18 RE-based metals or compounds, can effectively improve the kinetic performance of Mg-based hydrogen  
19 storage alloys. In this work, a series of transition and RE elements have been chosen to form the  
20 MgH<sub>2</sub>-ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) nanocomposites by high-energy ball milling to improve the  
21 hydrogen storage kinetic properties of Mg-based alloy. The results show that as-milled nanocomposites  
22 exhibit a faster dehydrogenation rate and better kinetic properties in comparison with the pure Mg/MgH<sub>2</sub>

1 system. The present work provides a helpful guideline on improving the kinetic properties of the Mg  
2 content-based hydrogen storage alloys.

## 3 **2. Experimental details**

### 4 *2.1 Preparation of MgH<sub>2</sub>-ANi<sub>5</sub> composites*

5 The states of raw alloy materials are shown in the table 1. Commercial MgH<sub>2</sub> powders (20 μm, 98%  
6 purity) were directly used without any other processing and ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) pieces were  
7 melted by arc melting. MgH<sub>2</sub> (95 wt%) and ANi<sub>5</sub> (5 wt%) were weighed and manually mixed in desired  
8 weight fraction using a stainless-steel dipper which contributed to a uniform distribution of the composition.  
9 It is worth noting that the theoretical hydrogen storage capacity of the mixture is 7.2 wt%. The high-energy  
10 ball milling was employed to process the mixture including MgH<sub>2</sub> and different ANi<sub>5</sub> under the 2.5 MPa  
11 hydrogen atmosphere which was a mixture of 5% hydrogen and 95% argon. The ball milling process was  
12 conducted with a ball-to-powder mass ratio of 30:1, the rotational speed was 1200 r/min, and every 30 min  
13 milling followed by 30 min interval for rest. Note that all operations were performed in the glovebox under  
14 the protection of high purity argon atmosphere to prevent the oxidation of the samples.

15 Table 1

16 Information of raw materials.

Material	Purity	Form	Size /μm(mesh)
MgH <sub>2</sub>	98.0%	Powder	≤20.0
CeNi <sub>5</sub>	99.9%	Granule	≤187.5 (80)
NdNi <sub>5</sub>	99.9%	Granule	≤187.5 (80)
SmNi <sub>5</sub>	99.9%	Granule	≤187.5 (80)
YNi <sub>5</sub>	99.9%	Granule	≤187.5 (80)
PrNi <sub>5</sub>	99.9%	Granule	≤187.5 (80)

### 17 *2.2 Characterizations*

18 The phase constitutes of the as-milled compounds were characterized by X-Ray diffraction (XRD,

1 DX-2700) which is equipped by a Philips X'Pert MPD X-ray diffractometer with Cu K $\alpha$  radiation ( $\lambda =$   
2 0.154 nm). The morphologies, particle sizes and chemical compositions of the samples were examined by  
3 scanning electron microscope (SEM-Zeiss Supra 40/VP). Differential Scanning Calorimetry (DSC)  
4 measurements were conducted to investigate the desorption behavior by using a Netzsch Jupiter 449C  
5 equipment under argon flow from room temperature to 450 °C at a heating rate of 5 °C/min.

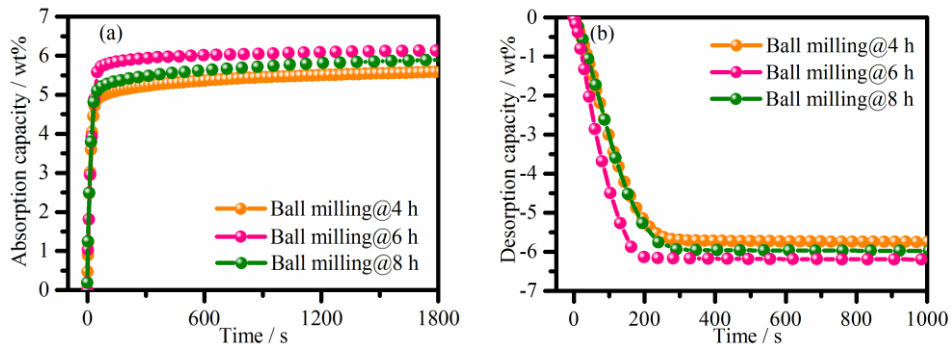
6 The hydrogen storage properties of all prepared samples were tested using a precise Sieverts-type  
7 apparatus Pro2000 equipped with the furnace for accurately controlling temperature within 2 °C.  
8 Specifically, the kinetic curves were measured at temperatures of 300 °C, 325 °C and 350 °C, respectively,  
9 under the hydrogen pressure of 2.5 MPa for the absorption processes while 0.1 MPa for the desorption  
10 processes. The thermodynamic properties at different temperatures were measured by pressure composition  
11 isotherms (P.C.I) using an Advanced Materials Corporation (AMC) gas reaction controller. The middle  
12 point of the measured P.C.I curve was taken as the plateau pressure to mathematically fit the enthalpy  $\Delta H$   
13 and entropy  $\Delta S$  during the absorption and desorption processing based on the van't Hoff plot.

### 14 3. Results and discussion

#### 15 3.1 Optimization of ball-milling time

16 Based on the previous work,<sup>[35]</sup> CeNi<sub>5</sub> and MgH<sub>2</sub> can be milled under a hydrogen atmosphere. It is  
17 worth noting that the ball-milling time is an important parameter to impact hydrogen storage  
18 performance.<sup>[36]</sup> On one hand, the composition of the sample will be not uniform if the milling time is not  
19 enough, which might make the milled sample not activated fully. On the other hand, too long-term milling  
20 process might aggravate the oxidation condition. Therefore, either deficient or excess ball-milling time will  
21 cause the loss of hydrogen storage capacity.<sup>[37, 38]</sup> In the present work, ball milling processes of  
22 MgH<sub>2</sub>-CeNi<sub>5</sub> sample with different time (i.e., 4 h, 6 h and 8 h) were conducted first to optimize ball-milling

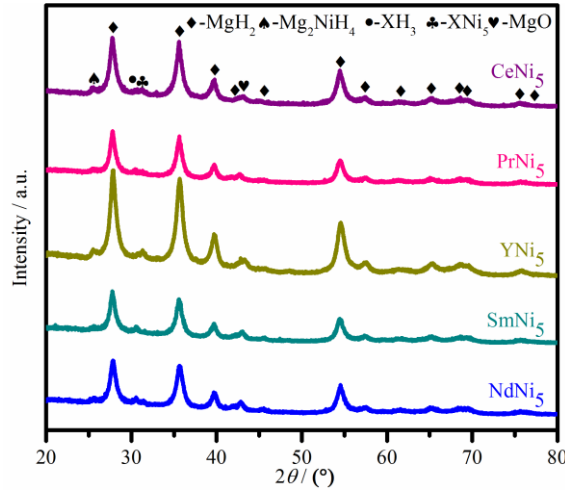
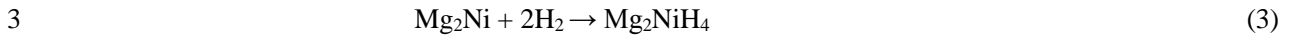
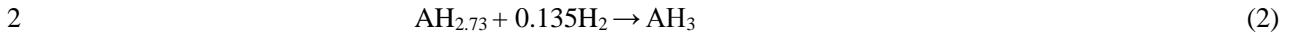
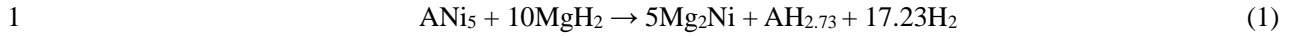
1 time based on the kinetic properties. Fig. 1(a) and (b) give respectively the absorption and desorption  
 2 kinetic curves of the  $\text{MgH}_2\text{-CeNi}_5$  sample with different ball-milling times at a temperature of  $320\text{ }^\circ\text{C}$ . The  
 3  $\text{MgH}_2\text{-CeNi}_5$  samples with a ball-milling time of 6 h own the highest absorption capacity and the fastest  
 4 hydrogen desorption rate, e.g., absorbing hydrogen capacity of 6.1 wt% within less than 350 s, which is  
 5 higher than that of 5.8 wt% in 4 h-milled samples and 5.6 wt% in 8 h-milled samples. Similarly, the sample  
 6 with a ball-milling time of 6 h also possesses the best desorption kinetic properties with the highest  
 7 desorption capacity and the fastest hydrogen desorption rate in comparison with 4 h-milled and 8 h-milled  
 8 samples, as shown in Fig. 1(b). The preliminary experimental results indicate that the ball-milling time of 6  
 9 h might be the optimum parameter, which will be adopted to process all  $\text{ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ )  
 10 samples and their hydrogen storage properties have been investigated in the following sections.



11  
 12 Fig. 1. Absorption (a) and desorption (b) kinetic curves of  $\text{MgH}_2\text{-CeNi}_5$  with different ball-milling times at  
 13 the temperature of  $320\text{ }^\circ\text{C}$ .

14 *3.2 Phase transition during de/hydrogenation processes*

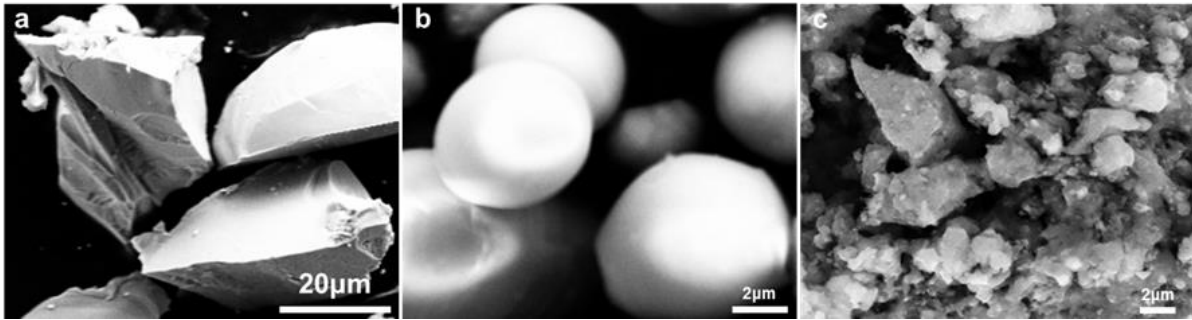
15 Fig. 2 shows the XRD patterns of as-milled  $\text{MgH}_2\text{-ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ ) composites,  
 16 revealing that the milled composites possess multiphase structures, including the  $\text{MgH}_2$  phase,  $\text{Mg}_2\text{NiH}_4$   
 17 phase,  $\text{AH}_3$  phase and some  $\text{ANi}_5$  phase left. The hydrogenation pathways during the ball milling process  
 18 can be therefore described as follows<sup>[39]</sup>



4  
5 Fig. 2. The XRD patterns of as ball milled  $\text{MgH}_2\text{-ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ ) composites.

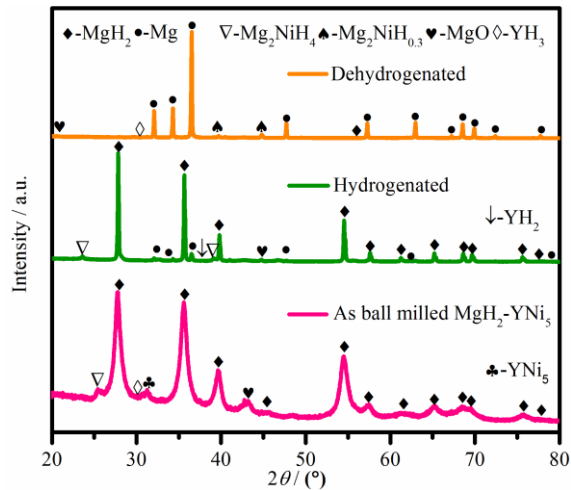
6 Fig. 3(a) and (b) exhibit the SEM images of one of the initial melted  $\text{YNi}_5$  alloys with the particle size  
7 ranging from 20-40  $\mu\text{m}$  and the commercial  $\text{MgH}_2$  powder with the particle size of 2-10  $\mu\text{m}$ , respectively.  
8 After the ball milling process, the particle size of the obtained  $\text{MgH}_2\text{-YNi}_5$  composites is refined, as the  
9 agglomerated particle composing of small granules ranging from nanoscale to 10  $\mu\text{m}$  in the corresponding  
10 SEM image shown in Fig. 3(c). The milled composites with refined microstructure will induce numerous  
11 defects, which would act as the diffusion path of hydrogen and nucleation sites for the de-/hydrogenation  
12 processes. Besides, it's worth noting that hydrogen atoms existing in the lattice interstitial site of lattice  
13 during hydrogenation may cause high lattice stress and expansion. Nonetheless, the nanocrystalline and  
14 amorphous structures can be kept under this saturated hydrogenation state, meaning the excellent structural  
15 stability of the as-milled composites.





1  
2 Fig. 3. The SEM images of (a) melted  $\text{YNi}_5$  alloy (b) commercial  $\text{MgH}_2$  powder and (c) as-milled  
3  $\text{MgH}_2$ - $\text{YNi}_5$  composites.

4 To figure out the phase changes of the composites during hydrogenation and dehydrogenation  
5 processes,  $\text{MgH}_2$ - $\text{YNi}_5$  is selected as a representative, which will be characterized by XRD after fully  
6 hydrogenated and dehydrogenated as shown in Fig. 4. Combine with Fig. 2, XRD patterns of as-milled  
7  $\text{MgH}_2$ - $\text{YNi}_5$  composite possess multiphase structures, including the phase of  $\text{MgH}_2$ ,  $\text{Mg}_2\text{NiH}_4$ ,  $\text{YH}_3$ , and  
8 some  $\text{YNi}_5$  left. The XRD peaks become strong and sharp obviously after the hydrogenation cycles, which  
9 indicates that the particle sizes become bigger and the crystallinity is also increased. Besides, it can be seen  
10 that  $\text{MgH}_2$  and  $\text{Mg}_2\text{NiH}_4$  are dehydrogenated to form  $\text{Mg}$  and  $\text{Mg}_2\text{NiH}_{0.3}$ , respectively. Notably, RE  
11 hydrides  $\text{YH}_3$  can only dehydrogenate partially to form stable phases such as  $\text{YH}_2$  which always remain  
12 unchanged in the following whole de/hydrogenation processes.<sup>[40]</sup> As mentioned above, these stable phases  
13 serve as a hydrogen pump for controlling desorption kinetics of hydrogen storage alloys.<sup>[32]</sup> Besides, it is  
14 worth noting that a small amount of  $\text{MgO}$  phase is also detected in these alloys. The appearance of  $\text{MgO}$  is  
15 believed to be originated from some unavoidable testing process exposed to the air environment.

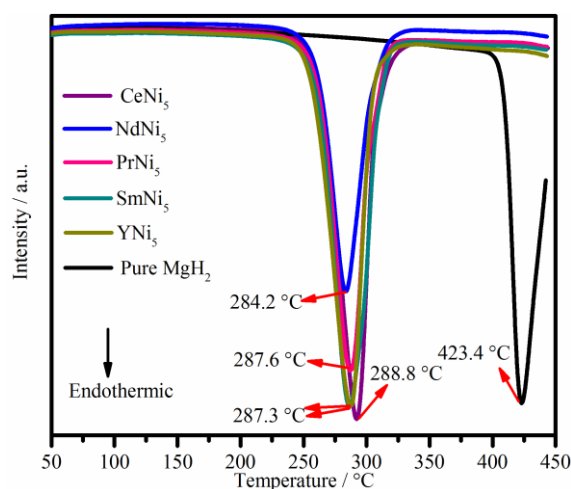


1  
2 Fig. 4. The de/re-hydrogenation XRD pattern and its initial XRD pattern of MgH<sub>2</sub>-YNi<sub>5</sub> composite.

3 *3.3 Hydrogen absorption/desorption kinetics*

4 The non-isothermal dehydrogenation performance of MgH<sub>2</sub>-ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) alloys  
5 were investigated by DSC. The temperature-programmed desorption curve of saturated hydride alloys at a  
6 heating rate of 5 K/min is illustrated in Fig. 5. In each closed chamber, the mass of the sample is set equal  
7 to avoid the effect of desorption temperature from incremental pressure.

8 Compared with the dehydrogenation peak temperature of 423.4 °C of pure MgH<sub>2</sub> without any  
9 treatment, it is shown that those of as-milled MgH<sub>2</sub>-ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) alloys are decreased  
10 to be 288.8 °C, 284.2 °C, 287.6 °C, 287.3 °C and 287.3 °C respectively. This suggests that the addition of  
11 ANi<sub>5</sub> alloys can effectively lower the desorption temperature of MgH<sub>2</sub>, which might be ascribed to the  
12 weakened Mg-H bond caused by the electronic exchange reaction between RE elements and MgH<sub>2</sub>.<sup>[41]</sup>

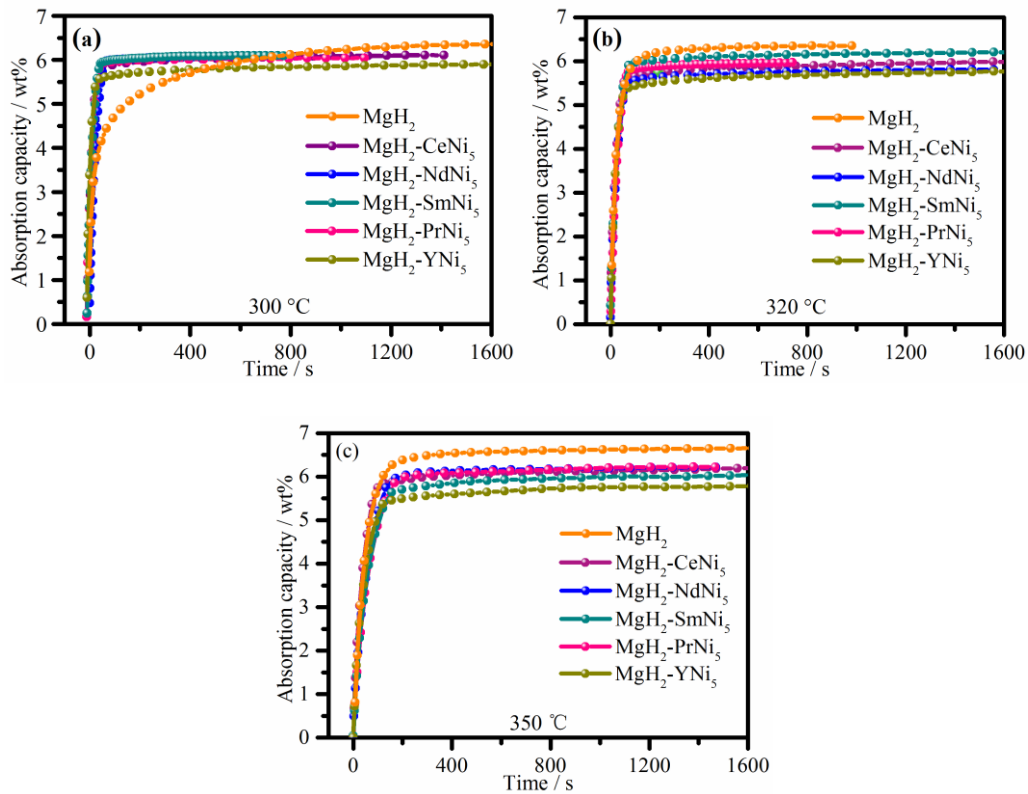


1  
2 Fig. 5. The DSC curves of as-milled  $\text{MgH}_2\text{-ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ ) alloys.

3 To inspect the influence of different  $\text{ANi}_5$  alloys on kinetic properties of  $\text{MgH}_2$ , activation procedure  
4 was applied to the samples before conducting kinetics experiments. This procedure included several  
5 hydrogen absorption and desorption cycles which were done at  $300\text{ }^\circ\text{C}$  and under an initial  $2.5\text{ MPa}$  for  
6 absorption and  $0.1\text{ MPa}$  for desorption.

7 The absorption kinetic properties of as-milled  $\text{MgH}_2\text{-ANi}_5$  composites were operated at  $300\text{ }^\circ\text{C}$ ,  $320$   
8  $^\circ\text{C}$  and  $350\text{ }^\circ\text{C}$ , respectively, under  $2.5\text{ MPa}$ , as shown Fig. 6(a-c), where the absorption kinetic curve of  
9 pure  $\text{MgH}_2$  processed by the same ball milling parameters is also provided for comparison. Notably, a rapid  
10 hydriding rate exhibits in all samples of achieving the almost saturated hydrogen absorption capacities  
11 within several minutes, after which there is nearly no increase in hydrogen absorption capacity. Specifically,  
12 five as-milled  $\text{MgH}_2\text{-ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ ) composites samples can reach the saturated  
13 hydrogen capacities of  $6.09\text{ wt\%}$ ,  $6.07\text{ wt\%}$ ,  $6.26\text{ wt\%}$ ,  $6.1\text{ wt\%}$  and  $5.92\text{ wt\%}$ , respectively, at the  
14 temperature of  $300\text{ }^\circ\text{C}$  within  $9\text{ min}$ , showing the better absorption kinetic properties, compared with that of  
15 pure ball-milled  $\text{MgH}_2$  which can reach a higher capacity after a quite long time. When the absorption  
16 temperatures are increased to  $320\text{ }^\circ\text{C}$  and  $350\text{ }^\circ\text{C}$ , however, it is found that the saturated hydrogen capacities  
17 and corresponding kinetics of five  $\text{MgH}_2\text{-ANi}_5$  ( $A = \text{Ce, Nd, Pr, Sm, and Y}$ ) composites are both worse than

1 those of pure ball-milled  $\text{MgH}_2$ . The experimental result in Fig. 6 indicates that the catalytic effect of  $\text{ANi}_5$   
2 alloys on  $\text{MgH}_2$  particularly works at a relatively lower temperature level which will be also reflected in the  
3 following sections. These hydrogenation curve characteristics might be attributed to the mechanism that a  
4 surface-near hydride layer is formed within the initial few minutes so that the diffusion of hydrogen  
5 through this layer becomes a rate-limiting factor.<sup>[42]</sup>



6  
7  
8 Fig. 6. The kinetic curves of hydrogen absorption of  $\text{MgH}_2$ - $\text{ANi}_5$  composites at different temperatures of (a)  
9 300 °C, (b) 320 °C and (c) 350 °C respectively.

10 In addition to the hydrogenation kinetics, Fig. 7(a-c) gives the dehydrogenation kinetic curves of the  
11 as-milled  $\text{MgH}_2$ - $\text{ANi}_5$  composites samples at temperatures of 300 °C, 320 °C and 350 °C, respectively,  
12 under 0.1 MPa. Different from the hydrogenation kinetics, the addition of the  $\text{ANi}_5$  leads to the dramatic  
13 improvement in dehydrogenation kinetics of  $\text{MgH}_2$ - $\text{ANi}_5$  composites for all temperature ranges, compared  
14 with that of pure milled  $\text{MgH}_2$ , as demonstrated clearly in Fig. 7(a-c). Note that the dehydrogenation

1 capacity of as-milled  $\text{MgH}_2\text{-ANi}_5$  composites samples decreases slightly with temperature increasing.

2 The hydrogen storage properties and phase about all the ball-milled samples are summarized in table 2.

3 Taking the experimental result at the temperature of 300 °C as an example, it is found that five as-milled

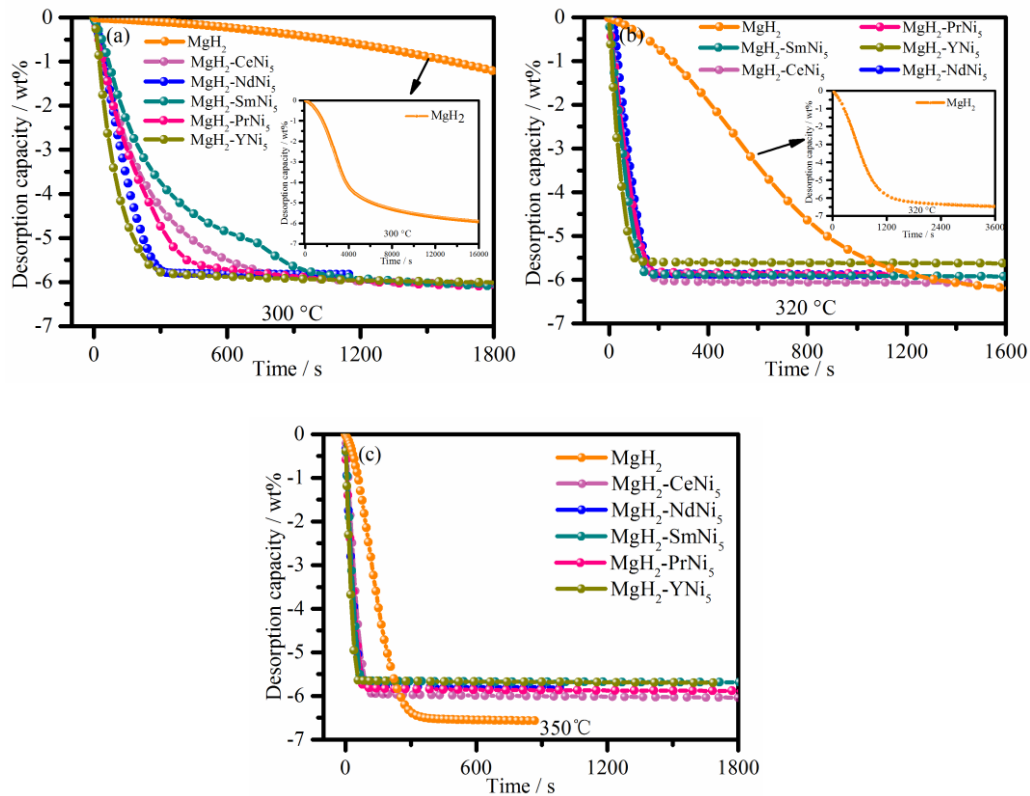
4  $\text{MgH}_2\text{-ANi}_5$  (A = Ce, Nd, Pr, Sm, Y) can desorb hydrogen capacities of 6.16 wt%, 5.7 wt%, 6.21 wt%, 6.38

5 wt% and 6.5 wt%, respectively, within 600 seconds, which are higher than that of 2.4 wt% in the pure

6 as-milled  $\text{MgH}_2$ . When the temperatures are increased to 320 °C and 350 °C, the as-milled  $\text{MgH}_2\text{-ANi}_5$

7 composites can still denote the better dehydrogenation kinetics than the pure ball-milled  $\text{MgH}_2$  which only

8 possesses the higher final desorption hydrogen capacities in a longer time.



10

11 Fig. 7. The kinetic curves of hydrogen desorption of  $\text{MgH}_2\text{-ANi}_5$  composites at different temperatures of (a)

12 300 °C, (b) 320 °C and (c) 350 °C respectively.

13 The decline in the final desorption capacity with increasing temperature in as-milled  $\text{MgH}_2\text{-ANi}_5$

14 composites might be attributed to the rapid growth of grains at higher temperatures which give rise to the

1 decrease of hydrogen capacity and sluggish diffusivity of hydrogen in hydrides. It has been well known that  
 2 the hydrogenation process of MgH<sub>2</sub> is dominated by the following three critical steps: 1) H<sub>2</sub> molecules  
 3 decomposing into H atoms on the surface of the alloy, 2) H atoms diffusing along grain boundaries, and 3)  
 4 hydrogenation of Mg atoms for transforming into MgH<sub>2</sub> molecules.<sup>[30]</sup> It is convinced that the decomposing  
 5 energy of H<sub>2</sub> molecules into H atoms dominates the hydriding rate of Mg and it is fairly high in Mg/MgH<sub>2</sub>  
 6 system.<sup>[43]</sup> In the present work, the Mg<sub>2</sub>NiH<sub>4</sub> embedded on the surface of the matrix and the stable RE  
 7 hydrides existed in the MgH<sub>2</sub>-ANi<sub>5</sub> is incorporated to serve as hydrogen pumps, which may make it easier  
 8 for hydrogen atoms to move through the metal matrix, thereby obviously speeding up the reaction rate of  
 9 hydrogen absorption and desorption, as shown in Fig. 6-7.

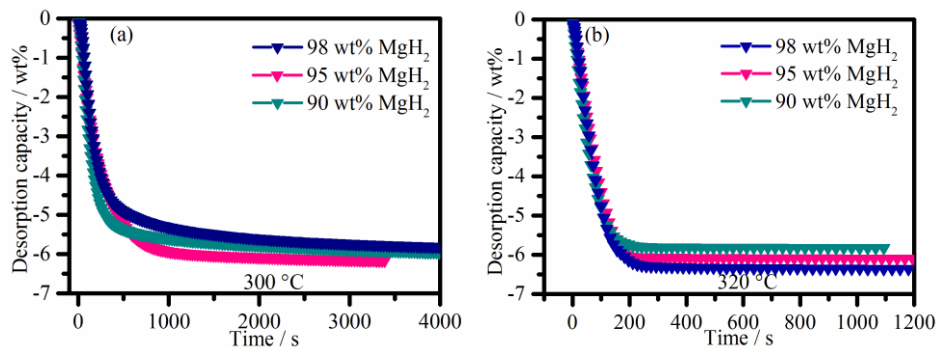
10 Table 2

11 Summary of phase and hydrogen storage capacity about different ball milling samples.

Composite	Main phase after ball-milling	H <sub>2</sub> absorption capacity (wt%) at 2.5MPa			H <sub>2</sub> desorption capacity (wt%) at 0.1 MPa		
		300 °C	320 °C	350 °C	300 °C	320 °C	350 °C
		MgH <sub>2</sub>	MgH <sub>2</sub>	6.41	6.75	6.65	5.82
MgH <sub>2</sub> +CeNi <sub>5</sub>	MgH <sub>2</sub> ; Mg <sub>2</sub> NiH <sub>4</sub> ; CeH <sub>3</sub>	6.09	5.98	6.21	6.16	6.08	6.05
MgH <sub>2</sub> +NdNi <sub>5</sub>	MgH <sub>2</sub> ; Mg <sub>2</sub> NiH <sub>4</sub> ; NdH <sub>3</sub>	6.07	5.80	6.22	5.71	5.92	5.80
MgH <sub>2</sub> +SmNi <sub>5</sub>	MgH <sub>2</sub> ; Mg <sub>2</sub> NiH <sub>4</sub> ; SmH <sub>3</sub>	6.10	6.20	6.02	6.38	5.96	5.72
MgH <sub>2</sub> +YNi <sub>5</sub>	MgH <sub>2</sub> ; Mg <sub>2</sub> NiH <sub>4</sub> ; YH <sub>3</sub>	5.92	5.80	5.78	6.50	5.64	5.70
MgH <sub>2</sub> +PrNi <sub>5</sub>	MgH <sub>2</sub> ; Mg <sub>2</sub> NiH <sub>4</sub> ; PrH <sub>3</sub>	6.26	5.97	6.21	6.21	5.85	5.90

12 Furthermore, as-milled MgH<sub>2</sub>-CeNi<sub>5</sub> composite with different weight fractions of MgH<sub>2</sub> was chosen as  
 13 an example to dissect the catalytic effect of ANi<sub>5</sub> alloy on the kinetic properties of Mg/MgH<sub>2</sub> system. Fig. 8  
 14 (a) and (b) give the dehydrogenation kinetic curves of MgH<sub>2</sub>-CeNi<sub>5</sub> composite with various MgH<sub>2</sub> weight  
 15 fraction (90 wt%, 95 wt% and 98 wt%) tested at temperatures of 300 °C and 320 °C, respectively. As for the  
 16 dehydrogenation curves at the temperature of 300 °C shown in Fig. 8(a), it can be obtained that the

1 desorption hydrogen capacity of the as-milled  $\text{MgH}_2\text{-CeNi}_5$  composite increases from 5.58 wt% to 6.16 wt%  
 2 in 15 min with the weight fraction of  $\text{MgH}_2$  increasing from 90 wt% to 95 wt%, while it decreases to 5.97  
 3 wt% in 30 min once the weight fraction of  $\text{MgH}_2$  continually increases to 98 wt%. When the temperature  
 4 goes up to 320 °C, however, the desorption hydrogen capacity of the as-milled  $\text{MgH}_2\text{-CeNi}_5$  composite in  
 5 Fig. 8(b) keeps increases from 5.8 wt%, 6.1 wt% to 6.4 wt% in 10min when the weight fraction of  $\text{MgH}_2$   
 6 increases from 90 wt%, 95 wt% to 98 wt%, respectively. This might be due to that the lower temperature is  
 7 more beneficial to activate the catalysis effects for improving the desorption kinetics.



8  
 9 Fig. 8. The dehydrogenation kinetics curves of  $\text{MgH}_2\text{-CeNi}_5$  composite with various  $\text{MgH}_2$  weight fraction  
 10 (90 wt%, 95 wt% and 98 wt%) tested at temperatures of (a) 300 °C and (b) 320 °C.

11 Finally, as-milled  $\text{MgH}_2\text{-YNi}_5$  composite was chosen as representative to inspect the effect of  $\text{ANi}_5$   
 12 alloys on the de/hydrogenation thermodynamic properties of the  $\text{Mg/MgH}_2$  system. Fig. 9 gives the P.C.I.  
 13 curves of  $\text{MgH}_2\text{-YNi}_5$  composite at various temperatures of 280 °C, 300 °C and 320 °C, respectively. Seen  
 14 from each PCI curve, there only contains one flat hydrogen platform demonstrating that only one phase  
 15 participates in the hydrogenation process, which is consistent with the DSC curve. Obviously, the fairly flat  
 16 absorption and desorption pressure plateaus correspond to the formation and dissociation of  $\text{MgH}_2$ . Based  
 17 on the plateaus of pressure in Fig. 9, thermodynamics parameters, enthalpy  $\Delta H$  and entropy  $\Delta S$  can be  
 18 derived from the van't Hoff equation as follow<sup>[44]</sup>

$$\ln\left(\frac{P_{H_2}}{P_0}\right) = \frac{\Delta H}{RT} - \frac{\Delta S}{R} \quad (4)$$

where  $P_0$  is  $1.01325 \times 10^5$  Pa,  $R$  is the mole gas constant, and  $P_{H_2}$  is the equilibrium plateau pressure corresponding to  $MgH_2$ . The enthalpy change  $\Delta H$  and entropy change  $\Delta S$  can be easily obtained respectively from the slopes and intercepts of the linearly fitting, as summarized in Fig. 9. According to Figure. 9, It's worth noting that the dehydriding reaction enthalpy is 78.23 kJ/mol and hydriding reaction enthalpy is -81.77 kJ/mol which are a little bit larger than the enthalpy 75 kJ/mol mentioned in the introduction. The increase in enthalpy of this alloy is due to the mixing of rare earth hydrides which have higher stability and higher enthalpy than  $MgH_2$ , this effect is also called the ‘‘Cocktail’’ effect.<sup>[45]</sup> The same phenomenon can be observed in many other similar systems, for example, the  $Mg_{90}Ce_5Y_5$  system,<sup>[46]</sup> the  $Mg_{88}Y_{12}$  system<sup>[47]</sup> and the Mg-Nd/Gd composite.<sup>[48]</sup>

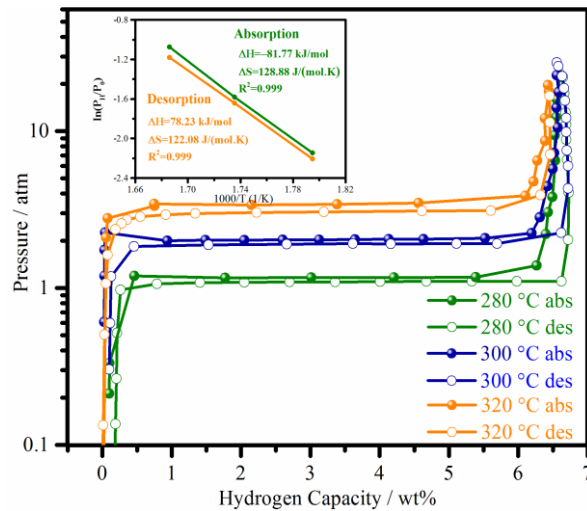


Fig. 9. P.C.I. curves and Van't Hoff plots of as-milled  $MgH_2$ - $YNi_5$  composite at temperatures of 280 °C, 300 °C and 320 °C respectively.

#### 4. Conclusions

In summary, five  $MgH_2$ - $ANi_5$  ( $A = Ce, Nd, Pr, Sm, \text{ and } Y$ ) composites have been synthesized by mechanical ball milling to enhance the hydrogen storage properties of Mg/ $MgH_2$  system, especially the



1 de/hydrogenation kinetic properties. The dehydrogenation temperature has been reduced from 423.4 °C in  
2 the pure MgH<sub>2</sub> without any additive to 288.8 °C, 284.2 °C, 287.6 °C, 287.3 °C and 287.3 °C respectively, in  
3 the as-milled MgH<sub>2</sub>-ANi<sub>5</sub> (A = Ce, Nd, Pr, Sm, and Y) composites. Particularly, as-milled MgH<sub>2</sub>-ANi<sub>5</sub> (A =  
4 Ce, Nd, Pr, Sm, and Y) composites can completely dehydrogenate within 600 s at the temperature of 300 °C,  
5 which exhibits excellent dehydrogenation kinetic performance. Besides, it is found that ANi<sub>5</sub> (A = Ce, Nd,  
6 Pr, Sm, and Y) could lead to a better catalytic effect on the desorption performance even at relatively lower  
7 temperatures of 300 °C. When changing the weight fraction of the MgH<sub>2</sub>, it is revealed that MgH<sub>2</sub>-CeNi<sub>5</sub>  
8 composite with 95 wt% MgH<sub>2</sub> can contribute to the highest desorption hydrogen capacity of 6.16 wt% in  
9 15 min. Our results provide a guideline or strategy in the enhancement of light metal-based hydrogen  
10 storage materials by adding transition metallic catalysts.

11

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18

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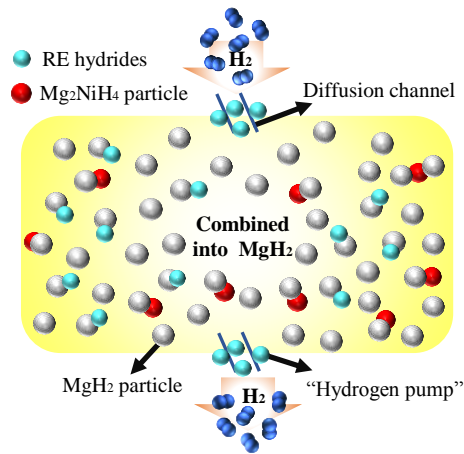
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- 15  
16

1 TOC Graphic:



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In-situ formed  $Mg_2Ni$  and stable RE hydride small particles are attached to the surface to form a diffusion channel together with the defect, and also serving as a hydrogen pump so that the kinetic properties of  $MgH_2$  can be improved significantly.