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Spatial Analysis of the Development Potential of a Commercial District: A Case of Hong Kong

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26	
27	Abstract

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29 With large-scale urbanization globally, the world is facing environmental problems brought 30 about by high-density cities. To achieve sustainable development in Hong Kong, especially for the 31 heavily loaded Cross Harbour Tunnel district, The Hong Kong Polytechnic University proposes a 32 Green Deck over the Cross Harbour Tunnel to enhance the neighbouring environments. Green 33 belts, buildings, and a new exhibition centre are planned for this deck. This will require an increase 34 in the guest capacity of nearby hotels in the Tsim Sha Tsui East (TSTE) area. This study therefore investigated the development potential of the 23 existing buildings in TSTE and the environmental 35 36 impact brought about by the increase of PR/BH in that area. Spatial analyses of solar exposure, 37 wind ventilation, and air temperature were conducted based on four different scenarios with 38 various PR/BH; human thermal comfort brought about by PR/BH changes were also measured. A 39 comparison of different scenarios revealed no significant changes in the surrounding environment. 40 The study concludes that there is potential for PR/BH relaxations in TSTE to increase spaces to 41 meet increased population flow. 42

43 *Keywords:* Development potential, Green Deck, High-density city, Spatial analysis, Urban 44 microclimate, Thermal comfort

45

46 **1. Introduction**

47 With the continuous growth of global urban areas, they are facing enormous challenges in 48 terms of land supply and the heat island effect, as well as environmental problems such as traffic 49 noise and exhaust pollution. Hong Kong is a typical densely populated city with high-rise buildings. 50 To achieve sustainable development in Hong Kong, particularly for the heavily loaded Cross 51 Harbor Tunnel district, The Hong Kong Polytechnic University (HKPU) has proposed an 52 innovative solution that involves constructing a Green Deck (HKPU, 2015) over the Cross Harbor 53 Tunnel plaza to enhance the immediate and neighboring environments. A comparison of the Green 54 Deck blueprint and the current Cross Harbor Tunnel plaza is presented in Fig. 1. The Cross Harbor 55 Tunnel is a cross-sea tunnel connecting Hong Kong Island and Kowloon Peninsula, which is one 56 of the busiest tunnels in the world. While providing convenient transportation in the Hung Hom 57 district, the Cross Harbor Tunnel also brings huge traffic congestion, environmental pollution, and noise problems. The proposed 43,000m² deck will accommodate various entertainment, cultural 58 59 and sports facilities, including a convention and exhibition center, while solving existing problems 60 in this area. It will not only provide people with a green resting space, but also help to promote the 61 sustainable development of Tsim Sha Tsui, especially Tsim Sha Tsui East (TSTE) and Hung Hom. 62 As a result of the proposed Green Deck and the convention and exhibition center, more tourists, 63 participants in conferences and other activities, and local residents will visit this area. Since most 64 visitors will choose to stay in nearby hotels, TSTE will undoubtedly be their first choice. This study therefore rigorously examines the development potential of TSTE with its current carrying 65 66 capacity of 23 existing buildings, including six hotels.

Development potential in Hong Kong is mainly controlled by Lease Conditions, Outline
Zoning Plans (OZPs) and Building (Planning) Regulations (BPR), all of which inevitably impose

69 restrictions on the plot ratio (PR) and building height (BH) of individual land zones. Hong Kong 70 has been struggling to develop every piece of land in downtown areas to its maximum potential 71 and so the development of the Green Deck project will bring unprecedented opportunities to TSTE. 72 To meet the increased high passenger flow, it is necessary to ensure enough living and working 73 spaces in TSTE, which currently has a building gross floor area (GFA) of 842,585.105m² for 23 74 buildings. Elevating the development potential of built-up region through minor relaxation of the 75 maximum PR/BH restrictions is a viable option for increasing living and working spaces within a 76 short timeframe. Although minor relaxation of PR/BH restrictions may be a possible way to 77 accommodate more people, its impact on the surroundings must be carefully analyzed.

Development intensity is generally explored through an Environmental Impact Assessment (EIA), as it is subject to the public's tolerance to changes in the environment. The TSTE area is a tourist check-in point, which is close to the Victoria harbor, Avenue of Stars, Hong Kong Coliseum, and famous shopping malls. Therefore, the extent to which this relaxation to the area will be acceptable to the public is rigorously analyzed in this study.

83 This paper investigates the development potential of the 23 existing buildings (including six 84 hotels) in the TSTE area and the environmental impact brought about by the PR/BH increase in 85 this area. Various spatial analyses including solar exposure, wind ventilation, and air temperature 86 are conducted through 3D building models of four different scenarios with various PR/BH, and 87 the thermal comfort of different scenarios is also calculated and compared. A comparison of the 88 four scenarios leads to a discussion and conclusions. The results of this study provide vivid design 89 sketch and science-based suggestions for urban planners or decision makers in relation to the 90 development of TSTE, and assist them in making better informed decisions. Moreover, 3D 91 visualization and scenario analysis in our study could help the non-professional public understand

92 the developing land and its future development, which is beneficial to the community engagement.
93 The same or similar planning model can be easily applied to urban renewal projects in other
94 districts of Hong Kong or similar initiatives in other high-density cities such as New York and
95 Tokyo.

96 2. Literature Review

97 The development potential of urban areas is one of the most important study topics in urban 98 planning. Most relevant studies are dedicated to providing scientific findings to support and to 99 guide the proper consideration of land use, building and facility renewal/development, culture, and 100 heritage preservation for improving social benefit without damaging the environment. In this 101 regard, some scholars have focused on the use of fundamental data (e.g., spatial characteristics, 102 financial data, political documents, environmental data and socio-economic data) to explore the 103 impact of urban development on the environment and to analyze the development feasibility of a 104 city or urban area. This study adopts the same focus and has a few relevant studies on exploring 105 the surrounding environmental impact after minor relaxation of the maximum PR/BH restrictions. 106 Although previous similar studies have integrated geographic information systems (GIS) for 107 assessing air ventilation and visual permeability etc., they have mainly focused on the use of 2D 108 GIS. Since the spatial distribution of land units in the real world is three-dimensional, 3D GIS can 109 help us to see the real world portrayed in true perspective and thereby make better-informed 110 decisions. One such research by Terzi and Bölen (2012) focused on the feasibility of urban 111 development strategies (i.e. market-led development, conservative-led development and fiscal 112 incentives-led development) for dealing with urban sprawl while preserving the environment in 113 Istanbul. Three other studies (Stevens et al., 2007; Tayyebi et al., 2011; He et al., 2018) were 114 dedicated to the modelling of urban expansion. All four studies made use of 2D spatial analysis

115 technology to deal with the potential of urban sprawl rather than 3D spatial analysis technology 116 (3DSAT). The latter technology was developed from the former by adding a vertical dimension to 117 the original two horizontal dimensions in spatial analysis. Since three dimensions enable 118 representation and visualization of real-world space better than two dimensions, many urban 119 development studies have been conducted using 3DSAT. The viability of using 3DSAT to study 120 urban development has been touched upon by Ranzinger and Gleixner (1997), Pullar and Tidey 121 (2001), Zhang et al. (2004), Mak et al. (2005), Thill et al. (2011), Leszek (2015), and Guo et al. 122 (2017, 2020), all of whom achieved effective results that help with making urban planning 123 decisions. The increased application of 3DSAT for urban development has resulted in the 124 following proposed tools based on 3DSAT: a GIS tool for urban climate evaluation (Li et al., 2004) 125 and for community engagement in urban planning (Foth et al., 2009); an original 3D GIS 126 methodology developed by Wong et al. (2011) for investigating the wall effect caused by the 127 proliferation of tall buildings along the coast of Kowloon in Hong Kong; a platform for assisting 128 decision making in urban development projects (Isaacs et al., 2011); an integrated approach for 129 assessing residential development (Xu & Coors, 2012); and a framework for assessing the 130 development potential of Liuzhou city in China (Xia et al., 2016). Although the above mentioned 131 researchers tried to introduce 3D GIS to their studies, however, they only applied this technology 132 into urban planning, landscape, and development control. Few people used 3D modelling and GIS 133 technology to do the research focus on the changes of PR/BH for the buildings and their related 134 impacts to the environment nearby. The tool used in Xia's study is similar to the one used in this 135 study, however, they only considered land use suitability, economic feasibility, and landscape 136 visibility. There are obvious differences in respect of the urban situation, socio-economic 137 conditions, and the scale of the study area. Hong Kong is a high-density city with many skyscrapers

and so the development of its urban areas involves different environmental issues. Although TSTE
is a relatively small-scale urban region, it is nevertheless important that the proposed development
be implemented as soon as possible in order to help maintain Hong Kong as one of the world's
leading financial centers.

Studies have shown that an urban microclimate is affected by many factors, such as the interrelated elements of air temperature and wind ventilation. Croker found that wind could bring hot air to shaded areas to increase the air temperature in those areas, and at the same time wind can bring cold air to exposed areas, thereby reducing the air temperature there (Croker,1956). As the density of urban development increases, urban canyons usually appear in densely populated urban areas with high-rise buildings (Wang et al., 2011). Air temperature and ventilation influence heat exchange and consequently affect the comfort of pedestrians (Bottillo et al., 2014).

149 People are subject to the combined effects of meteorological elements and use temperature to 150 indicate whether the environment is hot or cold. Energy exchange continuously occurs between 151 humans and the atmosphere, and the body maintains a constant temperature through its own 152 temperature regulation centre; if the human body feels uncomfortable it will lead to a 153 corresponding stress response (Zhang, 2015). However, few studies have focused on assessment 154 of the thermal comfort of people subjected to urban microclimate change. The exemplar of such 155 studies was conducted by Mayer who used ENVI-met to simulate the spatiotemporal distribution 156 of different levels of thermal comfort within the Rieselfeld quarter of the city of Freiburg in 157 Germany on a typical summer day in 2007 (Mayer et al., 2008). Therefore, human thermal comfort 158 is also a key factor considered in this study.

Development of the Green Deck project and its environmental influence can be addressed in
 terms of solar exposure, wind ventilation, air temperature, and human thermal comfort changes.

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161 Similar research was conducted by Guo et al. (2017, 2020) on PR/BH relaxation and related 162 analyses using 3D spatial analysis technology in the Kai Tak Development Area (KTDA) of Hong 163 Kong. However, since most of the KTDA was still under construction, all the 3D building models 164 of different scenarios were generated based on the blueprints (EKEO, 2012). TSTE is a very 165 different situation in that it is an existing commercial and tourism district and as such all the 166 simulated renovations are based on existing buildings. Therefore, in addition to paying special 167 attention to environmental impact factors and microclimate changes, insolation radiation energy 168 and human thermal comfort analysis are added in this study to understand the energy changes and 169 human feelings changes respectively after relaxation of the PR/BH in the study area. This will help 170 with better adapting to sustainable development.

171 Although many previous related studies applied 3D GIS and related software to the 172 development potential of urban areas, only a few of them focused on relaxation of PR/BH. The 173 success of the KTDA study provides a useful insight into the application of 3D GIS and spatial 174 analyses for assessing the development potential of TSTE. This research therefore investigates the 175 development potential of relaxing PR/BH restrictions of the existing 23 buildings, especially the 176 six hotels, in the TSTE area through 3D GIS and spatial analyses.

177 **3. Research Methodology**

178 **3.1 Framework of this Study**

The research framework, shown in Fig. 2 below, is in two major parts: 1) Data collection and 3D modelling and, 2) 3D spatial analyses. The 3D building models of the TSTE study area are generated using Digital Terrain Model (DTM) and building and infrastructure models according to the OZPs and BPR. To meet the needs of the research, four scenarios of the models with various PR/BH are created. In particular, 3D spatial analyses include effects on solar exposure, wind 184 ventilation, and air temperature based on various 3D models. Based on the results of wind 185 ventilation and air temperature for different scenarios, thermal comfort is calculated. For each 186 analysis, a comparison is made among the four scenarios to lead the final discussion and conclusion.

187

3.2 Study area and data collection

188 The study region and DTM is shown in Fig. 3. The inner boundary is the focus study area 189 including TSTE, HKPU, and Hung Hom Station areas. The outer area is the potential boundary of 190 the affected adjacent area within a 500 m radius covering Tsim Sha Tsui, Jordan, Whampoa and 191 Victoria Harbor. Refer to the previous study, Wang et al., Alexakis and Sarris (2010) also applied 192 500 m butter area in their studies. Therefore, considering the area of the TSTE, surrounding land 193 use types, and the area affected by the study area, a 500-meter buffer area is created. There are six 194 hotels out of 23 buildings in the study region. In this study, the six hotels are the focus objects to 195 check the carrying capacity after the Green Deck has been built.

196 The 3D spatial data including 3D buildings, roads, and DTM can be obtained from the Lands 197 Department in Hong Kong (Lands Department, 2016). However, as some of the available data is 198 not up to date, the data does not always identically match the current situation. For example, the 199 data for some parts of the Royal Garden Hotel and the New World Centre do not match the actual 200 current situation. Such 3D buildings are developed based on the current latest situation. The other 201 non-spatial collected data relates to the updated approved building plans including Site Class, Zone, 202 Site Area, PR, GFA, Site Coverage (SC) and BH of the existing six hotels in TSTE (see Table 1), 203 which are available from the Buildings Department (BD, 2017). The data is considered when relaxing the maximum PR/BH restrictions and make appropriate determinations of designing and 204 205 developing effective scenarios for 3D spatial analyses.

206 **3.3 Generation of four scenarios**

207 The maximum PR/BH restrictions are shown in the Lease Conditions proposed by The Land 208 Registry (LR, 2017), OZPs proposed by the Town Planning Board (TPB, 2016), and the BPR 209 proposed by the Buildings Department (BD, 2012). Specifically, the OZPs are statutory plans 210 prepared by the TPB under the Town Planning Ordinance and show land zonings and major road 211 systems for each planning scheme area. The OZPs (S/K1/28) are one of the most important 212 regulations when considering PR/BH relaxation. There are four major types of zones in the study 213 area: Commercial (C), Open Space (O), Government, Institution or Community (G/IC), and Other 214 Specific Uses (OU). The use of each zone is also restricted by the maximum BH. The BPR is made 215 under the Buildings Ordinance, which statutorily governs the planning, design and construction of 216 buildings. The BPR is another important regulation in the consideration of the PR/BH relaxation. 217 The BPR regulates the sites of buildings. These regulations classify the sites of buildings into three 218 classes - Classes A, B, and C with different definitions. These regulations restrict the maximum 219 PR/SC in terms of a building's site and height (described in regulations 20 and 21).

220 With careful consideration of the maximum PR/BH/SC restrictions, the relaxation of the 221 maximum PR restrictions in OZPs is increased from 12 to 15 under the BPR, and the maximum 222 BH restriction in the Lease Conditions is modified from the current BH (prevailing 51.5 meters) 223 to the maximum under OZPs (80 to 95 meters). With consideration of the foregoing, four 224 hypothetical scenarios with different PR/BH of the 23 buildings in TSTE are developed as shown 225 in Fig. 4. Scenario 1 (S1) is the current situation, which uses the current PR/BH of the buildings; 226 Scenario 2 (S2) is developed by maintaining the current SC, only partially increasing the PR to the 227 maximum under BPR and by increasing the BH to the maximum under OZPs; Scenario 3 (S3) is 228 developed by increasing the PR to the maximum under BPR with maintaining the current SC; and

229 Scenario 4 (S4) is developed by rebuilding all the buildings to the maximum PR under BPR and 230 the maximum BH under OZPs. By following the four hypothetical scenarios, the 3D buildings are 231 developed. The three scenarios S2, S3, and S4 are all reach the maximum PR and BH only with 232 the different building shape, roof shape, SC, and the complexity and difficulty of reconstruction. 233 The completed building models are shown in Fig. 5. However, the roof shape in S2 is difference 234 form other three scenarios. The reason is that only part of the current building (one of the building 235 facades) has been increased to the maximum PR/BH. The side facing the southeast was chosen to 236 be raised to the maximum PR/BH, because it faces Victoria Harbor and so most of the rooms could 237 have a sea view, which has extremely high commercial value.

238 **3.4 Simulation model for solar exposure analysis**

The effects of solar exposure in terms of time (hourly) on the direct insolation (excluding the diffused insolation) and the radiation energy of the insolation around the surface (land and building facades) of TSTE are investigated by using a simulation model. The solar exposure for each of the four individual scenarios is simulated. The parameters of the simulation include the date and time of simulation, coordinates of TSTE, and the solar azimuth and altitude (see Table 2).

244 Based on these parameters, the simulatoin model is applied in generating the footprint of 245 shadow volume, which is represented by a bundle of sunlight (see Fig. 6a) blocked by the buildings. 246 The generated footprints of building shadow are used as the impact boundaries (Fig. 6b) 247 respectively in the summer and winter solstices. All the 3D buildings/roads within these 248 boundaries are used as input for the simulation. The simulation is implemented based on Ecotect 249 analysis software, which is an environmental analysis tool widely used in the study of daylight 250 assessment, thermal performance, and acoustic simulation for building planning and design (Yang 251 et al., 2014; Thuesen, 2010; Wang et al., 2011; Peng, 2016). The results of the simulation include

the cumulative exposure time and radiation distributed on the 3D surface within the impactboundaries in the summer and winter solstices.

254 **3.5** Microclimate model for analysing wind ventilation

255 Wind flow significantly impacts the living environment and plays an important role in urban 256 climates, renewable energy development, and crisis management related to outward wind flow. 257 Airflow Analyst (version 1.4) is software that helps to analyze wind ventilation, which is based on 258 GIS and spatial data to simulate complex surrounding airflow movements. It uses a fluid dynamics 259 algorithm, 3D Computed Fluid Dynamics (CFD), which is a core element for a highly accurate 260 airflow analysis and was developed and tested at Kyushu University. It is the first software to 261 integrate CFD with GIS and is available as third-party extension software of the ArcGIS (version 262 10.6.1). Therefore, terrain and 3D building datasets prepared in ArcGIS can be directly used in 263 Airflow Analyst without any re-modelling of spatial data. Airflow technique of wind flow 264 estimation is used and validated in different studies to simulate wind speed (Li, 2011; Uchida et 265 al., 2011a, 2011b, 2011c; Uchida & Ohya, 2008, 2011).

A Digital Elevation Model (DEM) with a 2-meter spatial resolution and 3D models were used to simulate airflow in the study area using Airflow Analyst. The monthly means of wind direction and wind speed from Star Ferry Automatic Wind Station were acquired from the Hong Kong Observatory (HKO). Three computational grids were generated, corresponding to 3D scenarios (S1, S2, S3, and S4), and then subsequent fluid analysis, visualization and analysis of the results were performed.

3.6 Microclimate model for analysing air temperature

273 Simulation of air temperature is conducted by ENVI-met, which is a popular microclimate 274 model that can simulate the microenvironment of a study region and is widely applied in the study

275 of the relationships between urban design and microclimates (Toggweiler & Key, 2001; Emmanuel 276 & Fernando, 2007; Fahmy & Sharples, 2009; Ng et al., 2012; Li et al., 2016; Jamei & Rajagopalan, 277 2017; Morakinyo et al., 2017). The simulation of ENVI-met considers the interaction among soil, 278 vegetation and atmosphere based on theories of fluid dynamics and thermodynamics, with a few 279 pre-requisites including a steady temperature and no heat storage in the buildings (ENVI-met, 280 2017). These conditions result in a simulation that focuses only on the physical influence instead 281 of the anthropogenic effect. The capability of ENVI-met in simultaneous calculation of 282 meteorological conditions, soil and vegetation processes, and surface energy fluxes with a broad 283 range of urban configurations can also improve the simulation of an urban micro-climate (B.M, 284 2011; Jamei & Rajagopalan, 2017). Therefore, in this study, ENVI-met 4.1 was applied to simulate 285 the spatial patterns and air temperature distribution in the TSTE region with different building 286 designs (S1, S2, S3, and S4). The completed ENVI-met model of the study area is shown in Fig. 287 7. The expected results of the research will provide the basis for future development that take a 288 climate conscious urban design method. This model requires initial weather information, including 289 the direction and speed of wind, relative humidity, air temperature, and special humidity at a 290 specific date and time (see Table 3). Two seasons (summer and winter) were examined according 291 to the meteorological parameters and the climatological database of Star Ferry Automatic Wind 292 Station. Two typical days 11-July-2016 and 13-Jan-2016, which represent normal weather 293 conditions in summer and winter respectively, were selected to represent the two seasons.

The average air temperatures were 29.8°C for summer, and 16.0°C for winter (see Table 4). During the comparison of scenarios, S1 acts as a reference, while S2, S3, and S4 act as observations. Comparison values are calculated by deducting the reference values from the observation values.

298 **3.7** Thermal comfort to the surrounding environmental changes

299 Thermal comfort is an important scientific basis for measuring the rationality of 300 building/urban planning. The factors affecting thermal comfort mainly include four environmental 301 factors (air temperature, air velocity, air relative humidity, and mean radiant temperature) and two 302 human factors (the rate of metabolism of human body and the body clothing thermal resistance). 303 This study analyzed the changes in thermal comfort environmental factors brought about by 304 various building design scenarios with different PR/BH. To measure the degree of perceived 305 changes in the surrounding environment by the residents living in and nearby the area, three related 306 indexes were introduced: mean skin temperature (MST), apparent temperature (AT), and thermal 307 comfort index (TCI). All three indexes are related to air temperature, wind speed, and relative 308 humidity, but only air temperature and wind speed were changed according to the different PR/BH 309 for various scenarios.

310 3.7.1 Mean skin temperature

Under naked conditions, the temperature of the human skin surface responds well to the comfort of weather. When the surface temperature is between 35° C to 37° C, people will feel hot. It is commonly considered that 33° C to 34° C is most suitable, while 31° C to 32° C will cause a cold feeling. The formula for calculating the body surface temperature can be obtained by the following estimation process.

316 When the human body temperature T is 37° C, skin layer thickness d is 5mm, T_s is skin 317 surface temperature, and T_a is air temperature, the heat transferred from the human body to the 318 skin Q should be (Koichiro, 1961):

$$Q = k \times \frac{T - T_s}{d} \times S \tag{1}$$

Where k is coefficient of heat conductivity, which is approximately equal to $2.0921 \times 10-3J/$ (cm-1 · s · °C), and S refers to an area of skin equal to 1 m². The heat generated by the human body (Q) needs to be transmitted to the atmosphere to stabilize the body temperature and may include radiation, transmission and evaporation. Therefore, the following formulas can be established.

$$Q = Q_{radiation} + Q_{transmission} + Q_{evaporation}$$
(2)

325
$$Q_{radiation} \approx 20.92 \times (T_s - T_a)$$

326
$$Q_{transmission} \approx 87.03 \times \overline{V} \times (T_s - T_a)$$

327
$$Q_{evaporation} \approx 18.74 \times \overline{V} \times (E_s - r \times E_a)$$

Where the unit of temperature is $^{\circ}C$, V is the wind speed at the height of the human body, E_s is the saturated water vapour pressure on the surface of the human skin, E_a is the saturated water vapour pressure corresponding to the temperature, r is the relative humidity of the air, and the unit of Q is kJ/m²·h.

Based on equations (1) and (2), equation (3) can be calculated as follows:

333

$T_{\rm s} = T - Q \times d/k \tag{3}$

334 3.7.2 Apparent temperature

AT is the temperature equivalent perceived by humans, which is a heat index invented in the late 1970s and extended in the early 1980s by an Australian researcher named Robert Steadman who took four environmental factors into consideration: temperature, vapour pressure, wind speed, and relative humidity. According to Steadman's study (Steadman, 1984), the formula (4) for calculating AT is:

$$AT = 1.07T + 0.2e - 0.65V - 2.7 \tag{4}$$

341
$$e = \frac{RH}{100} \times 6.105 \times exp \frac{17.27T}{237.7 + T}$$

Where AT is apparent temperature (°C), T is temperature (°C), e is vapor pressure (hPa), V means wind speed (m/s), and RH is relative humidity.

344 3.7.3 Thermal comfort index

345 TCI is another topic that reflects human's satisfaction with the surrounding environment. 346 When the heat produced by human metabolism is allowed to consume or dissipate, thermal 347 neutrality is maintained, thereby maintaining a balance with the surrounding environment. 348 Although there are great differences from individual to individual in terms of physiological and 349 psychological satisfaction, main factors that directly affect thermal comfort can be divided into 350 two categories. One category is personal factors, which are characteristics of the occupants such 351 as metabolic rate and clothing level; the other category is environmental factors, which are 352 conditions of the thermal environment, namely air temperature, air speed, and humidity. Based on 353 Wu and Deng's study (2001), the equation for calculating TCI is:

354
$$I = 1.8 \times T + 0.55 \times (1 - RH) + 32 - 3.2V^{0.5}$$
 (5)

Where I means the thermal comfort index, T means temperature (°C), RH is relative humidity,
and V means wind speed (m/s).

357 4. Impact analysis and results

358 4.1 Solar exposure analysis and results

The solar exposure analysis for both summer and winter was investigated for the study area. Compared with winter, the solar exposure effect in summer is more obvious. Therefore, only the analysis and results for summer are presented and discussed in this paper; winter results can be 362 found in the research monograph (Shen et al., 2017). Fig. 8 shows the patterns of solar exposure 363 on 3D surfaces (shadow footprint and building facades) in terms of ten hourly sections (from cold 364 to warm colours) of direct insolation. The findings show that the buildings' roofs are exposed to 365 the sun for a longer time (around 9 to 10 hours) than the ground surfaces are (around 4 to 5 hours). 366 The reason is that the ground is shaded by the surrounding high-rise buildings for most of the time 367 during the day. To quantify the difference between four scenarios, the differences of the 368 corresponding pattern areas and the value of each individual pattern area of the four scenarios are 369 shown in Fig. 9. The difference between S2 and S1 is in the range of -10% to 2.5% for the time of 370 exposure. The reduced area is mostly in the (9, 10) hourly section. Specifically, the area exposed 371 by (9, 10) hour insolation in S1 is decreased by 10% with increasing PR/BH in S2, and the area 372 exposed by (8, 9) hour and (4, 5) hour insolation in S1 is increased by 2% and 2.5% in S2, 373 respectively. Similarly, the difference between S3 and S1 is in the range of -3% to 2% for the time 374 of exposure and the difference between S4 and S1 is in the range of -4.2% to 1.5% for the time of 375 exposure. All the trends of change are similar for the three difference lines. And the changes show 376 no significant impact of the PR/BH relaxation on the summer solar exposure. It is noted that the 377 difference between S2 and S1 is larger than others, a reasonable explanation being that the roof 378 area is much smaller than the other three scenarios due to differences in design among the four 379 scenarios; the additional increased building height in S2 also blocks the original roof area in S1. 380 Therefore, the roof areas that received the longest sunlight hours (around 9 to 10 hours) were 381 significantly reduced in S2 compared to S1. However, the roof shape is similar in S1, S3, and S4 382 because the increased buildings block part of the roof of the buildings that are lower than them and 383 part of the ground, meaning that the areas exposed by the longest sunline hours was slightly 384 decreased and the middle sunlight hours increased.

385 Fig. 10 shows ten sections of cumulative solar radiation energy in summer, while Fig. 11 show 386 the differences of the corresponding pattern areas and the value of each individual pattern area of 387 the four scenarios. The difference between S2 and S1 is in the range of -11% to 2% for the 388 cumulative radiation energy. The reduced area in S2 is mostly in (5760, $+\infty$) the Wh radiation 389 section, which corresponds to the longest sunlight hours. The area exposed by (2340, 2910) Wh 390 insolation in S1 is decreased by 2% compared to S1. The difference between S3 and S1 is in the 391 range of -3% to 1% and the difference between S4 and S1 is in the range of -5% to 2% for the 392 cumulative radiation energy. Both of the differences are similar, and they are smaller than the 393 difference between S2 and S1, with the trend similar to the sunline exposure.

The above results showing the overall situation of insolation in terms of time and radiation, indicate that the shading effect phenomenon becomes larger after PR/BH relaxation. The shading effect exists after mid-day and enhancement of the shading effect from the PR/BH relaxation has a positive impact on the life extension of facade materials. Furthermore, the shape and area of the building roof plays an important role in exposing the longest sunline hours.

399 **4.2 Wind Ventilation Analysis and Results**

400 Wind ventilation analyses were conducted and compared for both winter and summer. Since 401 wind speed in summer is relatively slower than in winter, only winter results are shown in this 402 paper. Accordingly, Fig. 12 shows the differences of four scenarios of winter wind speed at the 403 corresponding locations. The differences are mainly in the range of -1 m/s to 1 m/s between S2, 404 S3, S4, and S1 and only a small portion falls within the range of -5 m/s to -4 m/s or 4 m/s to 6 m/s. 405 As indicated by the shades near the buildings, wind speed is slightly increased in S4 in the TSTE 406 area. Compared to the other three scenarios, S4 is designed by rebuilding all the buildings to the 407 maximum PR/BH leading to a decrease in the area of most of the buildings and a subsequent 408 reduction in the SC. Therefore, the space between each building has increased accordingly and the 409 extra space can be used for green plants. This shows that widening the distance between buildings 410 in S4 permits more air flow in TSTE, which increases the wind ventilation in the area. Although 411 the wind speed patterns are similar for the four scenarios, increases of wind speed are more 412 prominent during the winter season when the wind is entering TSTE. However, since most of the 413 difference is within 1m/s, it can be concluded that there is no significant impact of the PR/BH 414 relaxation on the winter wind ventilation.

415 Distributions of wind flow direction during the winter season are shown in Fig. 13. As shown 416 in the figure, wind comes from the east and enters the TSTE area from gaps between the buildings 417 and circulates into the northern TSTE area (ellipse A), which is primarily located at the Urban 418 Council Centenary Garden area. This garden provides a significantly important corridor of wind 419 inflow to the TSTE regions during winter. However, the area highlighted with ellipse B indicates 420 that wind could not enter the TSTE area through the narrow gaps and would bounce back from the 421 buildings to become wind flow along the harbour rather than flowing into the area; this 422 phenomenon is enhanced in S2, S3, and S4. On the other hand, wind circulations inside the TSTE 423 area creates a strong outward wind flow from west to northeast and southeast, highlighted with 424 ellipse C, which seems to be reflected by the closely spaced building on the western side of Nathan 425 Road. It is evident that wind circulation is improved in S4 as compared to S1, S2, and S3 due to 426 the wider spaces between buildings.

427

4.3 Air temperature analysis and results

The simulation results of air temperature for each scenario were extracted at 1:00 am and 1:00 pm on the representative day of winter and summer seasons. Due to the high air temperature on summer afternoons, only the analysis and results during this time are presented in this section. In summer, the prevailing wind direction is from the west. As shown in Fig. 14, air temperatures on a summer afternoon range from $\leq 30.0^{\circ}$ C to $> 38.0^{\circ}$ C and the spatial patterns of the air temperature indicate warm to cold fringes from the southwest to the northeast. And, temperatures in TSTE, and most of the study areas (around 95%), lie in the temperature range of 32.0°C and 36.0°C in all scenarios.

436 Spatial patterns and distribution analysis of air temperature on summer afternoons are shown 437 in Fig. 15. A colour legend is designed to present changes in air temperature due to the changes in 438 building dimension corresponding to the different scenarios. The temperature range (-0.20°C to 439 0.20° C) is considered as insignificant, while changes in air temperature beyond this range, i.e., 440 below -0.20°C or above 0.20°C, are deemed as significant changes. There is no notable change in 441 S2 and S3 temperatures when compared to S1, with most of the area within an insignificant range 442 of -0.20°C to 0.20°C respectively. However, compared to S1, there is an uncharacteristic pattern 443 of change in S4 as a relatively higher temperature is observed in the southeast of the study area. 444 This might be due to the fact that the prevailing wind direction in summer is from the west and the 445 increased height in building increases and expands the air temperature regime. However, most of 446 the regions with increased temperature lie over the coastal region, away from the core study area.

447 **4.4** Thermal comfort analysis of the surrounding environmental changes

Three related thermal comfort indexes were calculated to measure the reaction of human feelings to the surrounding environmental changes brought about by minor relaxation of the maximum PR/BH in the study area. The air temperature and wind speed for various scenarios was obtained from the CFD simulation results in sections 4.2 and 4.3. The air temperature and wind speed of S1 and S4 were obtained from CFD simulation results and are shown in Table 5. S1 and S4 were taken as examples, because S1 is the original lowest PR/BH and S4 is a hypothetical case with the maximum RP/BH. The relative humidity for the winter and summer in 2016 are available
on the Hong Kong Observatory website at Star Ferry Automatic Wind Station, which is near the
study area (HKO, 2016). Three human feelings indexes, MST, AT, and TCI were calculated using
the equations listed in section 3.7 with the results shown in Table 6. The human comfort index
classification is shown in Table 7.

459 As can be seen from the human feeling indexes, AT is the most sensitive indicator. Therefore, 460 AT is referred to as the main index to verify the changes in human feelings brought about by 461 PR/BH changes of surrounding buildings. AT is much larger in summer (about 8°C) than the air 462 temperature, while the difference between AT and air temperature is small in winter (about 2°C). The large difference between AT and air temperature is mainly related to the high air temperature 463 464 in the summer, while the air can hold much more specific humidity due to the high air temperature 465 (see the term of e in Equation 4). After comparison, the difference between S1 and S4 on MST, 466 AT, and TCI are very small both in winter and summer. In short, there is a minor effect on human 467 feelings when the PR/BH of buildings are increased to the maximum. In Hong Kong, people will 468 feel comfortable in winter, while people will feel very hot or extremely hot in summer. This is the 469 reason why air temperature, wind ventilation, and heat island effects need to be considered when 470 conducting urban development or redevelopment.

471 **5. Discussion**

472 Solar exposure, wind ventilation, and air temperature were all analyzed in this study, along 473 with a comparison of calculated human thermal comfort in relation to surrounding environmental 474 changes. Some of the analyses in this study are similar to the ones in the pilot study of PR/BH 475 relaxation for residential/mixed use buildings in KTDA. However, the results represent the 476 development potential in TSTE where existing buildings, including six hotels, are in densely built 477 commercial zones rather than in residential zones that are still under construction as in the KTDA.
478 Therefore, the findings of this study are more representative of the issues in the compact
479 development of a high-density city and also more supportive of maintaining social-economic
480 development in a suitable manner.

481 This study used ENVI-met for simulating air temperature and wind ventilation in the TSTE 482 and surrounding areas. Notwithstanding the promising results, there are nevertheless limitations to 483 this study: (i) the study simulated the influence of PR/BH on air temperature and wind ventilation 484 only, we did not consider the impact of water bodies, vegetation, transport, and human activities 485 in this study. However, water bodies, vegetation, transportation and human activities will have 486 corresponding impact on the thermal environmental changes. Through verification and application 487 research with various configurations, the evaporative cooling effect from water surfaces in a 488 micro-environment was evaluated by Tominaga et al. in 2015. Finally, a numerical analysis was 489 carried out combining CFD and radiative heat transfer analysis to predict the thermal environment 490 around residential neighborhood with a pond. The results showed that the maximum temperature 491 decrease due to the water body was around 2 °C at the pedestrian level. Besides, Park et al. (2012) 492 investigated the mitigating effect of vegetation on the urban microclimate for decades. The results 493 revealed that the presence of four sidewalk trees reduces the wind speed inside the canopy by up 494 to 51%. Trees along the sidewalk also decrease the globe temperature; the reduction is attributed 495 mainly to the decrease in radiation flux resulting from the shade they cast. The development of 496 Green Deck project and its influence can also be addressed in terms of transportation. In the past, 497 the relationship between "built environment" and people's travel behavior has been explored and 498 confirmed (Ni and Loo, 2012). To express the built environment, one way is to adopt the yellow 499 boundary 3Ds (Density, Diversity, and Design) first advanced by Cervero and Kockelman (1997).

500 Furthermore, Yue et al. (2008) used remote sensing and GIS technologies to research on the 501 relationship between the spatial-temporal change of thermal environment and human activities in 502 Shanghai. They applied Spatial Principal Component Analysis (PCA) methodology to analyze the 503 spatial pattern of the urban thermal environment and its influencing factors. The results revealed 504 urban construction density, population density, industry distribution, types of underlying surface, 505 and urban landscape diversity were the main factors affecting the urban thermal environment in 506 downtown area of Shanghai; (ii) meteorological data were obtained from the nearest observation 507 stations in the TSTE area instead of from the specific sites being considered; and (iii) default rather 508 than specific values were applied for soil properties and water content. Although as a consequence 509 of the limitations the simulation results may not be accurate enough for absolute quantification, 510 they are sufficiently accurate for studying relative differences. Furthermore, although ENVI-met 511 may not be capable of deriving rigorous quantitative results at a specific time, it can nevertheless 512 accurately depict the trend of changes (Maggiotto et al., 2014).

The findings show that the potential of GFA increases among TSTE's 23 buildings is 208,493.297 m², as shown in Fig. 16. Taking the six hotels as an example, the GFA increased from 207,220m² to $260,261m^2$ after PR/BH relaxation, with a net increase of $53,041m^2$. The number of rooms for the six hotels increased by 892, which together can hold 1,784 more guests. It should be noted that the effects of traffic capacity and noise were not analyzed in this study.

518 6. Conclusions

519 This study was carried out against the background of the Green Deck plan. It investigated the 520 development potential of TSTE in terms of the PR/BH relaxation of buildings for increasing the 521 capacity of living and working spaces to meet the increased population flow whilst preserving the 522 environment. The impacts of the PR/BH relaxation on the environment of the study area were assessed in respect of solar exposure, wind ventilation, and air temperature. The analyses and thecorresponding results are as follows.

525 (1) In summer and winter solstices, the effect of the PR/BH relaxation on solar exposure was 526 analyzed, both of which have extreme duration of solar exposure. However, for 527 representative purposes only the results in summer were shown in this paper. The patterns 528 of solar exposure in terms of sections of time and cumulative radiation energy were 529 generated for S1, S2, S3, and S4. The differences (S1 vs S2, S3, and S4) of the 530 corresponding pattern areas indicate the enhancement of shading near the building footprint 531 areas and this effect is positive for the life extension of facade materials; it was also found 532 that the shape and area of the building roof seriously affect the longest sunline hours and 533 corresponding radiation energy. Compared to S1, the areas exposed by sunline hours 534 between 9 to 10 hours sharply declined in S2, while slightly decreasing in S3 and S4. 535 Correspondingly, the areas exposed by sunline hours between 3 to 5 hours are slightly 536 increased in S2, S3, and S4. The trend of radiation energy is similar.

(2) Wind ventilation was simulated in S1, S2, S3, and S4 respectively in summer and winter.
However, only the results in winter were shown in this paper. The comparison (S1 vs S2,
S3, and S4) shows a small range of wind speed change from -1 m/s to 1 m/s for both seasons
and the S4 is more ventilated (higher wind speed) for the wind as the SC of the buildings
is narrowed, which release more space between buildings. The wind direction is not
significantly changed after the relaxation.

(3) Air temperature was analyzed in S1, S2, S3, and S4 respectively in both day (1:00 pm) and
night (1:00 am) and in both summer and winter. Similarly, only the summer afternoon
results were present in this paper. The differences (S1 vs S2, S3, and S4) imply a minus

23

range of air temperature change [-0.2°C, 0.2°C], which is a not insignificant zone of change,
for both time and seasons from S1 to S2, and S3. The southwest area has a change by more
than 0.4°C from S1 to S4 in summer as the speed of the west wind carrying heat to TSTE
is improved by the widened spacing between buildings. A relatively higher temperature is
observed in the southeast of the study area which is close to Victoria Harbour.

(4) MST, AT, and TCI were indexes used to represent the human thermal comfort reaction to
changes in the surrounding environment of the study area. There is no significant difference
between S1 and S4 for all three indexes both in winter and summer. However, a large
difference was found between AT and the initial air temperature in summer, since the
temperature and specific humidity are much higher at that time. It can therefore be
concluded that AT is the most sensitive of the three indicators.

In summary, an appropriate relaxation of the PR/BH in the study area has no significant negative impact on environmental issues or people. On the contrary, the increased GFA and associated hotel rooms could alleviate the problem of increased tourists in the area resulting from construction of the proposed Green Deck. Furthermore, the research methodology employed in this study is suitable for application to other districts in Hong Kong or other high-density cities with the similarity throughout the world.

563 Acknowledgements

The authors wish to thank the Research Grants Council, the Innovation and Technology Commission, the Policy Innovation and Co-ordination Office of the Government of the Hong Kong Special Administrative Region, the Research Institute for Sustainable Urban Development, and The Hong Kong Polytechnic University for the funding support to the research which has contributed to the preparation of this paper.

569 Data availability statement

- 570 All the data support the findings of this study are available from the corresponding author
- 571 upon rational request.

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706 Figure captions list

- 707 **Fig. 1.** Comparison of Green Deck blueprint (a) and Cross Harbour Tunnel plaza (b)
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Tables list

No	Building	Site	Zono	Site area	PR	GFA	SC (9/)	BH	0 (N	ZPs Iax)	BI (M	PR ax)
190.	name	class	Zone	(m ²)	(total)	(m ²)	SC (70)	(m)	PR	BH (m)	PR	SC (%)
1	Kowloon Shangri-La			4000.000	11.599	4638 3.644	74.079	47.10				
2	InterContinent al Grand Stanford			2479.000	10.540	2612 8.660	75.000	47.00		80.0		
3	New World Millennium	C	С	2850.000	11.832	3371 8.948	74.253	47.96	12		15	65
4	The Royal Garden	C		2219.600	14.993	3327 8.630	74.960	62.60			15	05
5	Regal Kowloon Hotel			2560.000	12.401	3174 6.004	74.767	49.00		95.0		
6	Hotel ICON		G/IC	4000.000	8.991	3596 4.050	64.960	107.00	-	111.5		

Table 1. Buildings plan for the six hotels in the study area

 Table 2. Parameters of simulating the solar exposure in TSTE

	sinialading the solar exposure in 15	11
Parameter	Winter Solstice (22-Dec-2013)	Summer Solstice (21-Jun-2013)
Time	8:40 - 16:00	7:15 - 17:32
Coordinates	22.30° for Latitude	114.10° for Longitude
Azimuth	127°SE - 232°SW	72°ENE - 288°WNW
Altitude	20°	20°

Table 3. Configuration setting in ENVI-met

Initial Configuration	11-Jul-2016 (Summer)	13-Jan-2016 (Winter)
Start Time of Simulation	7:00am	7:00am
Total Simulation Time (Hour)	24	24
Wind Speed in 10m Above Ground (m/s)	2.70	3.42
Wind Direction (degree)	West (260°)	East (100°)
Initial Atmosphere Temperature (°C)	27.50	15.45
Specific Humidity in 2500m (g water/kg air)	10.42	5.24
Relative Humidity in 2m (%)	83	85

Meteorologi	cal	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	D
Average Wind S	Speed	29.4	4 21.3	3 22.8	17.1	20.2	18.0	19.2	17.1	18.9	26.3	27.0	2
Prevailing W Direction (deg	′ind gree)	60	20	50	40	70	220	230	60	80	70	70	
Average Ai Temperature (ir (°C)	16.0) 15.5	5 17.5	23.6	26.7	29.4	29.8	28.4	27.9	26.8	22.3	
Date				13-Janu	ary-2016					11-Jul	y-2016		
Average Wind S	Speed			3.	.42					2.	70		
(m/s) Prevailing W Direction (deg	vind gree)			10)0°					26	i0°		
Table 5. Ini	itial v	alues o	of air tei	nperatur	e, wind	speed	and rel	ative h	umidit	у			
		Date	1	Air temper	rature (°C))	Wind sp	eed (m/s	s)	Rela Humid	itive ity (%)		
				S1	S4		S1	S4			_		
	13 Jan	uary 20	16 1	9.798	19.79	0.	.9352	1.03	25	8	5		
	(M 11 Ji	uly 2016	3	3.6725	34.062	0.	7325	0.75	34	8	3		
	(Su	immer)											
	ıman	feeling	s index	es - MS'	Г. АТ. а	nd TC	T						
Table 6. Hu		MST	(°C)	AT	(°C)	<u> </u>	TCI		Hum	an feelii	igs		
Table 6. Hu Date		S1	S4	S 1	<u>S4</u>	S 1	S1		S1		<u>54</u>		
Table 6. Hu Date	:016		10.20	01.01	21 73	66.91	66.02	Con	ortable	C	C	le	
Table 6. Hu Date 13 January 2 (winter)		19.32	19.30	21.81	21.75	00.84	00.83	Con	nonaon	e Co	miortat		
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer)	16)	32.69	33.06	41.55	42.14	89.37	90.01	Ve peo uncor	ery hot, ple feel very mfortabl	E E ho fee unc	xtremel ot, peopl el extren omforta	y le ne <u>ible</u>	
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer)	16) <u>Iman</u>	19.32 32.69	33.06	41.55	42.14	89.37 Bai et a	90.01 1., 200	Ve peo unco 9]	ery hot, ple feel very mfortabl	E ho fee e unc	xtremel ot, peop el extrer omforta	y le ne lble	
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com	16) <u>1man</u> nfort in	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific	42.14 cation [H	89.37 Bai et a	90.01 1., 200	Ve peo <u>unco</u> 9] Tł	ery hot, ple feel very mfortabl	E ho fee e unc	xtremel ot, peop el extren omforta	y le ne ble_	
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com	16) 1man nfort in 90	19.32 32.69 <u>comfor</u> ndex C	33.06 rt index Grade of	41.55 classific physiolog Level 9	42.14 cation [E	89.37 Bai et a	90.01 11., 200	Ve peo uncor 9] Th hot, pec	ery hot, ple feel very mfortabl nermal p	E ho fee erceptic	xtremel ot, peop el extrem omforta	y le ne <u>ble</u>	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com	16) <u>1man</u> nfort in)0)0)	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8	42.14 cation [F	89.37 Bai et a	90.01 al., 2009 ctremely Very	Ve peo uncor 9] Th hot, pec hot, pec	ery hot, ple feel very mfortabl nermal p pple feel ople feel	E ho fee e unc erceptic extremo very un	xtremel ot, peop el extrer omforta	y le <u>ble</u> omfortal table	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9] [79-8] (70-8)	16) <u>1man</u> nfort in 90 90) 85) 70)	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7	42.14	89.37 Bai et a	90.01 etremely very	Ve peo uncoi 9] Th hot, pec hot, pec	ery hot, ople feel wery mfortabl nermal p ople feel ople feel	E E ho fee e unc erceptic extreme very un uncom	xtremel ot, peop el extrer omforta on ely uncco fortable	y le <u>ble</u> omfortal table	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9] [79-8] [79-8] [70-7]	16) <u>1man</u> nfort in 90 90) 85) 79)	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7 Level 6	42.14	89.37 Bai et a	90.01 90.01 al., 200 stremely Very A little	Ve peo uncor 9] Th hot, pec hot, pec hot, sor	ery hot, pple feel very mfortabl nermal p ople feel ople feel pple feel pple feel	E ho fee e unc erceptic extremo very un uncom: le feel u	xtremel ot, peop el extren omforta on ely unco comfor fortable incomfo	y le <u>ble</u> omfortal table	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9] [79-8] [70-7] [60-7]	16) <u>1man</u> nfort in) 0 90) 85) 79) 70)	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7 Level 6 Level 5	42.14	89.37 Bai et a	90.01 al., 200 stremely Very A little	Ve peo uncor 9] Th hot, pec hot, pec hot, sor	ery hot, pple feel very mfortabl nermal p ople feel ople feel ople feel ople feel comfo	E ho fee e unc erceptic extreme very un uncom le feel u rtable	xtremel ot, peop el extren omforta on ely unco comfor fortable incomfo	y le ne ble	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9] [79-8] [70-7] [60-7] [50-6]	16) <u>1man</u> nfort in 90 90) 85) 79) 70) 50)	19.32 32.69 <u>comfor</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7 Level 6 Level 5 Level 4	42.14	89.37 Bai et a	90.01 90.01 al., 200 atremely Very A little Coo	Ve peo uncor 9] Th hot, pec hot, pec Hot, pec	ery hot, ple feel very mfortabl nermal p pple feel pple feel pple feel me peop Comfo people	E ho fee e unc erceptic extreme very un uncom ile feel u rtable feel unc	xtremel ot, peop el extren omforta on ely unco comfor fortable incomfor	y le ne <u>ble</u> omfortal table ortable	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9 [79-8 [70-7 [60-7 [50-6 [40-5	16) <u>1man</u> nfort in 90 85) 79) 70) 50) 50)	19.32 32.69 <u>comfoi</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7 Level 6 Level 5 Level 4 Level 3	42.14	89.37 Bai et a	90.01 al., 200 atremely Very A little Coo A little	Ve peo <u>unco</u> 9] Th hot, pec Hot, pec hot, sor ol, some cold, m	ery hot, ople feel very mfortabl permal p ople feel ople feel me peop Comfo people	E ho fee erceptic extremo very un uncom ile feel u rtable feel unc ble feel u	xtremel ot, peop el extrer omforta ely unco fortable incomfor omforta uncomfo	y le <u>ble</u> omfortal table ortable ble ortable	ble
Table 6. Hu Date 13 January 2 (winter) 11 July 201 (Summer) 11 July 201 (Summer) Table 7. Hu Thermal com >=9 [85-9 [79-8 [70-7 [60-7 [50-6 [40-5 [25-4	16) <u>1man</u> nfort in 2 0 2 0 3 0	19.32 32.69 <u>comfoi</u> ndex (33.06 rt index Grade of	41.55 classific physiolog Level 9 Level 8 Level 7 Level 6 Level 5 Level 4 Level 3 Level 2	42.14	89.37 Bai et a Ex	90.01 90.01 stremely Very A little Coo A little	Ve peo uncor 9] Th hot, pec hot, pec hot, pec hot, some cold, m Cold, pe	ery hot, ople feel very mfortabl nermal p ople feel ople feel ople feel me peop Comfo people :	E E ho fee e unc erceptic extreme very un uncom ile feel u rtable feel unc ble feel u	xtremel ot, peop el extrer omforta ely unco fortable uncomfor omforta uncomfor	y le ne <u>ble</u> omfortal table ortable ble	ble

Table 4. Meteorological elements and climatological database by HKO in 2016