

# Model Predictive Control of Microgrids – An Overview

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**Abstract**—The development of microgrids is an advantageous option for integrating rapidly growing renewable energies. However, the stochastic nature of renewable energies and variable power demand have created many challenges like unstable voltage/frequency and complicated power management and interaction with the utility grid. Recently, predictive control with its fast transient response and flexibility to accommodate different constraints has presented huge potentials in microgrid applications. This paper provides a comprehensive review of model predictive control (MPC) in individual and interconnected microgrids, including both converter-level and grid-level control strategies applied to three layers of the hierarchical control architecture. This survey shows that MPC is at the beginning of the application in microgrids and that it emerges as a competitive alternative to conventional methods in voltage regulation, frequency control, power flow management and economic operation optimization. Also, some of the most important trends in MPC development have been highlighted and discussed as future perspectives.

**Keywords** —Model predictive control, microgrid, primary control, secondary control, tertiary control, hierarchical control

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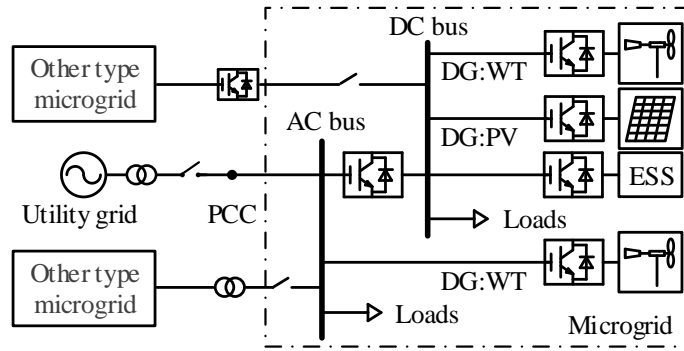
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2 **1. Introduction**

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4 Over the past decades, renewable energy systems (RESs) have been rapidly developed due to ecological,  
5 social, economic and political forces and interests, such as the widely installed photovoltaic systems (PVs) and  
6 wind turbine systems (WTs) [1-3]. In order to better integrate distributed generations (DGs) into the utility grid,  
7 microgrids have emerged as a promising solution to interconnect RESs, energy storage systems (ESSs) and loads  
8 through various power electronics interfaces [4-8].

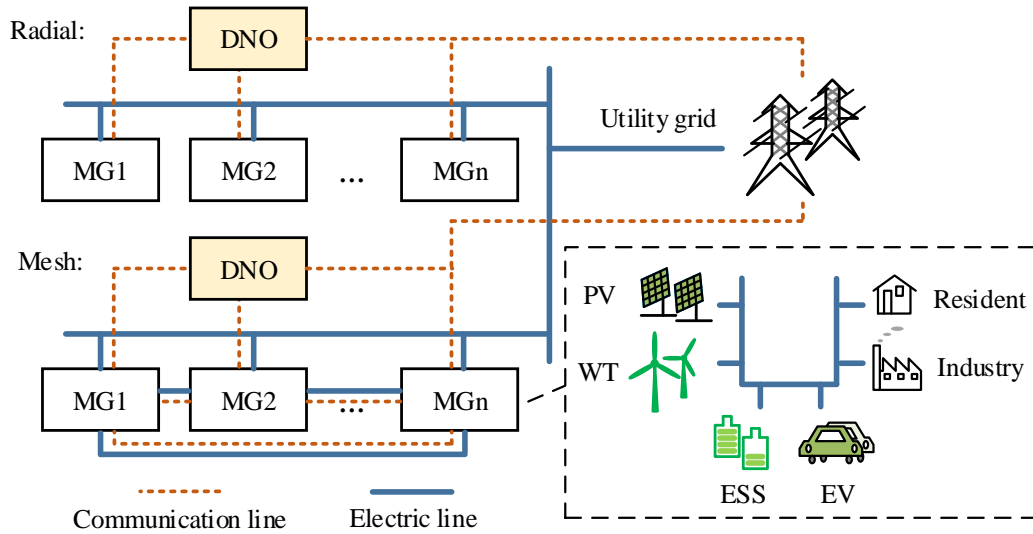
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11 For the sake of interaction with the utility grid, the microgrid has the capacity to operate in grid-tied mode  
12 acting as a controllable single unit or in an islanded mode as a self-sufficient autonomous system. Microgrids  
13 can be classified, according to the main common buses, into dc, ac, and hybrid types. Fig. 1 (a) shows the  
14 configuration of converter-interfaced microgrids with distributed RESs and ESSs. As shown, a microgrid can be  
15 connected with other types of microgrids through various converters. Also, it can link to the upstream grid via  
16 the point of common coupling (PCC). Fig. 1 (b) depicts the diagram of interconnected microgrids. It shows that  
17 microgrids can be interconnected in radial or mesh topology, using distribution network operator (DNO) to  
18 govern the power flow. In each microgrid, PV, WT, ESS, electric vehicle (EV), resident and industry systems  
19 can be accommodated.

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22 Currently, droop control methods are widely researched and adopted for the power sharing inside a microgrid,  
23 endowing an ability to eliminate critical communication links among DGs [9-11]. However, conventional droop  
24 control suffers from poor transient performance, inherent conflict between the precision of power sharing and the  
25 deviations of frequency/voltage, etc. Recently, hierarchical control of microgrids is foreseen to play a  
26 particularly important role [6][10][12][13]. Hierarchical control has the advantages of maintaining the strength  
27 of droop control, wiping out frequency&voltage deviations and guiding the power flows to/from the utility grid.  
28 Generally, hierarchical control consists of three levels, namely primary control, secondary control and tertiary  
29 control. These layers are distinguished by different communication bandwidths and time responses. Primary  
30 control is the fundamental layer that stabilizes system frequency and voltage, and shares loads with the fast  
31 response. Secondary control offsets the deviations of frequency/voltage derived from the primary control, aiming  
32 to recover the voltage/frequency to the rated values in steady state and to achieve utility grid connection. Tertiary  
33 control concerns the power flow among microgrid clusters, or between microgrids and upstream grid with  
34 additional functions like power planning and economic optimal scheduling.

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(a) Configuration of converter-interfaced microgrids.



(b) Diagram of interconnected microgrids

Fig. 1. Microgrids

In the primary control, the power sharing methods, together with cascaded inner current and outer voltage feedback loops, are frequently used [6]. Nevertheless, this kind of cascade linear control (CLC) has main drawbacks such as [14-16]: 1) system performance is highly dependent on control parameters; 2) system status is sensitive to external noises and load changes; 3) trial-and-error based iterative tuning procedure results in a less effective application; 4) an additional step with the pulse-width modulation (PWM) regulator is needed. Consequently, the design of more advanced control strategies has gained great attention in global academic and research communities to address the high penetration of RESs. Besides, the conventional CLC methods still show less intelligence and flexibility to address the complexities and uncertainties from the high penetration of RESs, leading to power quality reductions and stability concerns [14][17-19].

For secondary control, it mainly has centralized and distributed/decentralized categories [7][13][20]. The centralized one requires a central controller to densely collect, process and deliver signals, causing the possible single point of failure. In contrast, the distributed type based on local controller collecting local information can avoid such failure and enables scalability. With the rapid development of DGs and microgrids, secondary control

1 tends to be implemented in the distributed manner. As for tertiary control, power flow management and relevant  
2 economic optimization of the microgrid interacting with other microgrids or the utility grid are the main  
3 objectives [21-23].  
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6 Recently, a promising method named model predictive control (MPC) or receding horizon control, clearly  
7 distinguished from conventional CLC principles, has been widely used in either DG systems equipped with  
8 power converters [24-27] or microgrids with multiple RESs [21][22][28-30]. In this context, the optimal control  
9 behaviors or scheduled commands are determined according to predefined cost functions or objective targets  
10 under different constraints. To sum up, MPC has many advantageous features [31][32]: 1) multiple constraints  
11 from control and physical perspectives can be explicitly and intuitively involved; 2) excellent dynamic  
12 performance with robust control system; 3) control signals can be produced directly giving a straightforward  
13 simplicity; 4) an open access is enabled to interface various solving algorithms, making complex optimization  
14 problem solvable and convenient. While these techniques have already been reported in existing literature, they  
15 are seldom summarized from the perspective of hierarchical microgrids. Besides, in microgrids, researchers need  
16 to face new challenges in the development of MPC with the consideration of RES intermittency, load sharing  
17 accuracy, circulating currents, grid stability, etc.  
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20 The purpose of this paper is to offer a thorough systematic review of the state-of-the-art MPC strategies  
21 applied to microgrids. The major contributions are listed below. 1) A comprehensive review of MPC used in  
22 microgrids has been conducted, covering two categories, converter-level MPC and grid-level MPC. 2) The two-  
23 level MPC strategies applied to the three layers of microgrid's hierarchical control architecture have been  
24 discussed. 3) The most important trends in MPC development have been highlighted and discussed, illustrating  
25 MPC is at the pilot stage in microgrid applications and it is foreseen to be a very competitive alternative to  
26 conventional methods.  
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28 The remainder of the paper is structured as follows. First, the basic principles of MPC on converter level and  
29 grid level are summarized. Then, a comprehensive investigation into recent MPC approaches in three layers of  
30 the hierarchical control architecture, including power converter control, frequency/voltage restoration and power  
31 flow management/economic optimization is conducted. Next, some of the challenges and limitations are  
32 discussed. Last but not least, possible future trends are pointed out.  
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## 35 **2. Basic Principle of Model Predictive Control**

36 Actually, MPC does not refer to a particular control approach, but rather to a set of control approaches that  
37 take full advantage of the system model under specific constraints to gain the control signals or commands  
38 through minimizing predefined cost functions or objective targets [33]. As for the MPC applied in microgrids, it  
39 can be apparently different in terms of converter level and grid level. In general, the former produces switching  
40 signals to drive the power converters while the latter determines the dispatching commands for DGs and  
41 controllable loads. However, these two levels have a similar control structure and design procedure based on the  
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2 common MPC architecture. On this point, it can be said there is no clear boundary between these two control  
3 levels.  
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5 Regarding the common control structure, predictive model, cost function and solving algorithm are three key  
6 ingredients of MPC [27][34]. While for the common design procedure, generally, developing the predictive  
7 model is the first step, followed by designing the cost function, and lastly setting the solving algorithm. Among  
8 them, constraints are usually formulated inside the cost function. In this section, converter-level and grid-level  
9 MPC methods are respectively investigated and studied.  
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## 14 15 2.1 Converter-level MPC

16 Existing MPC methods for converters can be classified into two sets: continuous control set MPC (CCS-MPC)  
17 and finite control set model predictive control (FCS-MPC) [25][35]. CCS-MPC generates continuous signals for  
18 the PWM regulator to drive converters, while FCS-MPC is built on the discrete behavior of converters and thus  
19 avoids the usage of PWM regulators. During these years, FCS-MPC has been extensively used in many  
20 applications [24][26].  
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26 As stated above, FCS-MPC is an important branch of the MPC family. Taking the one-horizon prediction, for  
27 instance, Fig. 2 shows the general principle of converter-level MPC. The predictive model is obtained from the  
28 discretization of *RLC* circuit dynamics through state variable acquirement that can be achieved by either  
29 measurement or estimation of voltage/current/power.  
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33 The predictive model can be represented by the following equation, through which the state variables at next  
34  $k+1$  instant  $\hat{\mathbf{x}}(k+1)$  can be acquired.  
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$$37 \quad \hat{\mathbf{x}}(k+1) = f(\mathbf{x}(k), \mathbf{u}(i)) \quad (1)$$

38 where  $\mathbf{x}(k)$  refers to RLC circuit dynamics at  $k$  instant;  $\mathbf{u}(i)$  refers to the converter switching states in a finite  
39 number;  $f(\cdot)$  is the function which follows Kirchhoff's voltage/current law.  
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44 The cost function considering the Euclidean distance between the predicted and the rated values is usually  
45 expressed as  
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$$48 \quad g = \sum \left( w_j \left| \mathbf{x}^* - \hat{\mathbf{x}}(k+1) \right| \right) \quad (2)$$

49 where  $\mathbf{x}^*$  is the control reference, i.e. the desired values of voltage, current, power, etc.;  $w_j$  is the weighting  
50 coefficients.  
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53 Since FCS-MPC considers limited switching states, solving the algorithm can be simple. Usually, exhaustive  
54 search algorithms are fully competent [36]. This is different from undermentioned grid-level MPC which usually  
55 employs a specific toolbox to help solve a more complex algorithm. It is worth mentioning that various converter  
56 topologies can be applicable in Fig. 2, including but not limited to dc-dc [37-39], dc-ac [40-42], ac-dc [43-45],  
57 ac-ac [46][47], multi-level converters [48-50], or the converters with complex topology [51-53].  
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1 During these years, converter-level MPC has been actively developed. Since a constant switching frequency is  
 2 generated, the most used derivatives of CCS-MPC are generalized predictive control (GPC) and explicit MPC.  
 3 In Refs. [54] and [55], GPC was both used with LCL filter for solving harmonic issues. In Ref. [56], a neutral  
 4 network core to build the input-output model was embedded in an explicit MPC for dc-dc converters. As for  
 5 FCS-MPC, those considering control time sequence are an important emerging branch. In Ref. [57], a deadbeat  
 6 technique was adopted to regulate currents during one control period, thus to better govern control time sequence.  
 7 Besides, in Ref. [58], a steady switching frequency and an improved steady-state performance were  
 8 simultaneously obtained by improving the FCS-MPC.  
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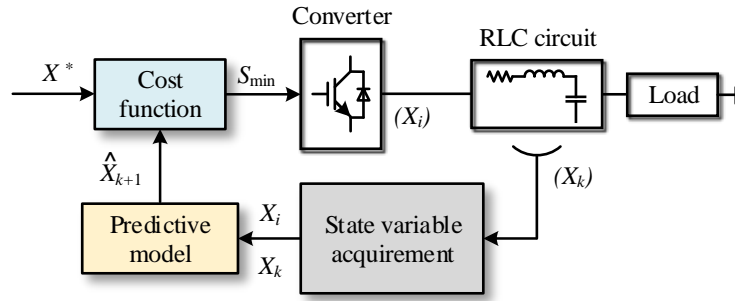


Fig. 2. Diagram of converter-level MPC.

## 2.2 MPC for Grid Level

36 Similar to converter-level MPC, the grid-level MPC also consists of predictive model, cost function and  
 37 solving algorithm. However, grid-level MPC aims to control system-level operating statuses (e.g. ESS capacity,  
 38 power flows within a microgrid or among networked microgrids). Grid-level MPC serves as an optimization  
 39 algorithm that is suitable to optimize the performance of constrained systems with multiple objectives. Fig. 3  
 40 illustrates the general diagram of grid-level MPC. As shown, the predictive model is built upon the system states  
 41 with possible forecasts, which formulates an expression for the future state prediction usually on the basis of  
 42 current/past states. More concretely, the forecasts/predictions of the predictive model can be various state  
 43 variables on a certain time-interval basis, like load demands, electricity prices, PV/WT generations, etc.  
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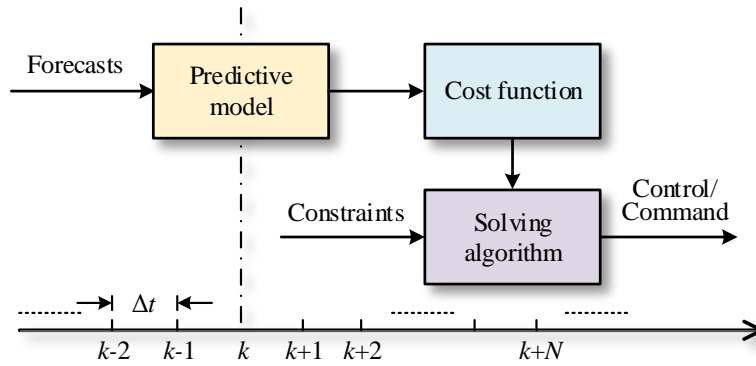


Fig. 3. Diagram of grid-level MPC.

Cost function design should reflect the concerns of the control objectives. Generally, the items in a cost function are in line with the multiple control or optimization targets. The predictions generated from the predictive model and possible desired targets are formulated into this cost function. During each sampling period, the optimal control/command sequence over a certain time horizon is computed for all the concerned parts of the whole system. Then, a group of system states is refreshed, resulting in an updated cost function, waiting for a further round of calculation to move the horizon one step forward. Grid-level MPC can provide a receding prediction horizon with a feedback mechanism that effectively reduces the impacts of uncertainties, thus making it more robust to disturbances.

Constraints should be considered in all involved DGs, power converters, power components, power lines, and the utility grid. Once the constraints are well formulated, the system performance can be improved with an ability to operate inside or near the constraint boundaries safely. The optimization problems taking constraints into account will then be solved by moving the time horizon window forward with the optimization problems being recalculated and solved again once new predictions are available.

The sampling interval  $\Delta t$  of a grid-level MPC can be ranged from several seconds to several hours and often larger than that of converter-level MPC. The time horizon is often determined according to multiple factors. For example, if the PV power output is recorded on a 1-min period basis, while the PV generation is predicted in every 30 minutes. In this case, the final sampling interval for the MPC is expected to be multiples of 30 minutes for a better match and precision.

The following steps can be summarized to implement the grid-level MPC: 1) first, system states and targets are utilized to form a receding model; 2) for a certain control horizon, an optimal control/command sequence is figured out for the next prediction period based on the data predictions; 3) implement the first step of the MPC considering all variables and constraints; 4) update all available states for the next period while moving one step ahead and repeating the optimization.

### 3. Microgrid Primary Control

The hierarchical control of microgrids stems from the three-layer control structure of large-scale power systems. In the hierarchy of microgrids, the fundamental level is the primary control which aims at maintaining the basic operation of the microgrid, thus providing a stable frequency/voltage supply and sharing the load demand properly. The followings are the brief descriptions of primary control and the associated MPC controllers that are mainly adopted for converter levels.

#### 3.1 Power Sharing Method

A brief overview of the widely used power sharing method, i.e. droop control, is discussed here. Equation (3) illustrates the mathematical droop characteristic in an ac microgrid.

$$\begin{cases} f = f^* - mP \\ E = E^* - nQ \end{cases} \quad (3)$$

where  $f^*$  and  $E^*$  are the rated values of ac bus frequency and voltage,  $P$  and  $Q$  the active and reactive powers,  $m$  and  $n$  the  $P$ - $f$  and  $Q$ - $E$  droop coefficients, respectively.

Since reactive power and frequency do not exist in dc microgrids, the droop control in dc microgrids is formulated in a way that dc voltage reference will be linearly reduced with the increase of output current, which is expressed as

$$E_{dc} = E_{dc}^* - i_{dc} R_d \quad (4)$$

where  $E_{dc}^*$  is the dc voltage reference,  $i_{dc}$  the converter output current,  $R_d$  the virtual resistance used to match the real line resistances.

#### 3.2 Virtual Impedance Method

Virtual impedance design is an effective way to reconstruct the system control output impedance, thus seeking a suitable application environment of droop methods and avoiding the use of real impedors. The design principle is described as

$$v_o^* = v_{ref} - Z_D(s) \cdot i_o \quad (5)$$

where  $v_{ref}$  is from droop equation (3) after a voltage synthesis (usually also after using a coordinate transformation),  $Z_D(s)$  the transfer function of virtual output impedance in  $S$  domain,  $i_o$  the output current.

In practice, the output impedance is usually modified to either inductive, or resistive, or capacitive, depending on the nature of the power feeder, the filter and the control strategy [9]. For instance, the conventional droop method, i.e. equation (3), is supposed to have an inductive output impedance thus to meet the assumption in its formula derivation. Actually, virtual impedance can be endowed with a wide range of functions. For example, it can be set to a required harmonic impedance at a certain frequency to enable harmonic sharing and damping [59].



1  
2 3.3 MPC in Primary Control

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4 For the MPC applied in primary control, most of the existing work focuses on replacing the cascaded voltage  
5 and current loops with MPC controllers. As for the islanded microgrids, the essential task is to provide a stable  
6 voltage supply, which leads to a voltage formulation in the cost function using MPC methods. In this case,  $v_o^*$  in  
7 (5) can be selected as the cost function reference for the MPC. For example, the schematic diagram of the MPC  
8 used in the primary control of an islanded ac microgrid is illustrated in Fig. 4 in which the CLC method is also  
9 used in the primary control of an islanded ac microgrid is illustrated in Fig. 4 in which the CLC method is also  
10 depicted. As shown, the measurement or the estimation from the circuit is used both for power calculation and  
11 MPC/CLC controllers. Then these controllers need the virtual impedance obtained from the droop control with  
12 the calculated powers. The main benefit of using MPC in a microgrid is the fast transient response to deal with  
13 the fluctuating power outputs from the renewable energies [17][60-63]. Moreover, the simplification of  
14 removing the PWM modulator is also achieved.

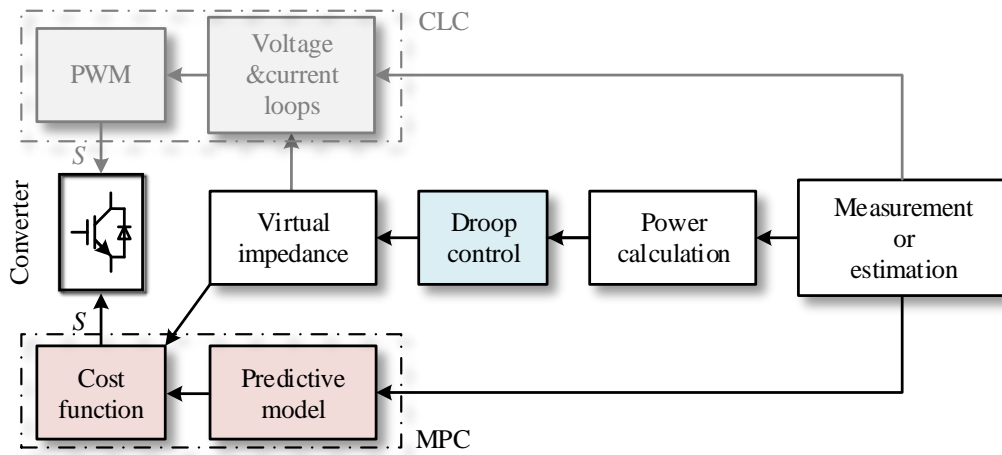


Fig. 4. MPC used in the primary control of an islanded ac microgrid.

44 When a microgrid works in grid-tied mode, the control target is changed to the regulation of power flow since  
45 the frequency and voltage are strongly fixed by the stiff utility grid. In this scenario, the converter-level MPC  
46 can incorporate the power flow into the cost function to replace the conventional power&current loops in CLC  
47 method, as depicted in Fig. 5. Also, it is straightforward for cost functions to formulate the rated active and  
48 reactive power values.

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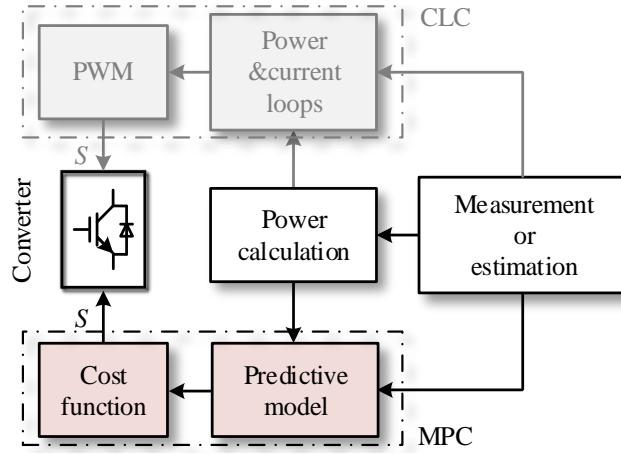


Fig. 5. MPC used in a grid-connected ac microgrid.

### 3.4 Predictive Model with Longer-Horizon Prediction

The converter-level MPC based on Euler forward approximation only has one step predictive horizon. For a longer-horizon prediction, the following steps are mostly adopted.

- 1) In  $k+1$  instant, we assume all predictive models can be denoted as (in state-space form)

$$\mathbf{x}(k+1) = A\mathbf{x}(k) + B\mathbf{u}(k) \quad (6)$$

where  $A$  and  $B$  are coefficients.

- 2) When one more step prediction is considered, it yields [64]

$$\mathbf{x}(k+2) = A\mathbf{x}(k+1) + B\mathbf{u}(k+1) \quad (7)$$

It should be noted that the above equation is also an effective way to compensate the one-step delay for a real digital implementation.

- 3) Then, to achieve a further prediction horizon  $N$  (integer and  $>2$ ), a linear extrapolation method can be employed [65]

$$\mathbf{x}(k+N) = \mathbf{x}(k+1) + (N-1)[\mathbf{x}(k+2) - \mathbf{x}(k+1)] \quad (8)$$

With this procedure, a longer-horizon prediction can be done to obtain additional merits such as system stabilization and reduced switching frequencies. However, it is noted that a longer-horizon prediction does not always ensure a better performance, which subjects to the accuracy of the predictive model [66].

### 3.5 Cost Function Optimization

The cost function reflects the control objectives and provides a criterion for selecting the optimal control set. In general, when the number of terms formulated in the cost function is not less than one, i.e. multiple targets are considered. Therefore, the weighting coefficients of each term need to be designed carefully. Different coefficient ratios generate different system performances. Normally, for different units and different values of the cost function terms, the coefficients are set to be divided by their references respectively to reach a

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2 normalized value if each term is equally treated. Otherwise, if one term needs to be treated with high priority, its  
3 coefficient will be set to a larger value to prioritize this objective. This kind of compensation along with the  
4 coefficients adjustment turns out to be a trial-and-error process which heavily relies on expert and experiential  
5 knowledge of the control target. As one advantageous way to optimize the weighting coefficients, intelligent  
6 algorithms can be employed. For instance, fuzzy logic control can be adopted to make the decision of selecting  
7 weighting coefficients, thus to obtain a better system performance [67-70].

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9 With regard to the control references in cost functions, they are usually set to constant or ideal values.  
10 However, sometimes the approximations of past-instant variables which change little will be chosen as the  
11 references, as expressed in (9). This can be seen in a converter-level MPC with a small sampling time (around  
12 tens of microseconds). For instance, the ac bus voltage in a grid-connected ac microgrid can be assumed  
13 unchanged during successive time instants since the bus is strongly fixed by the stiff grid.

$$24 \quad \mathbf{x}(k+1) \approx \mathbf{x}(k) \quad (9)$$

25 One way to make this approximation more precise for the above example of the ac bus voltage is to modify  
26 the  $k+1$  instant variable with a voltage compensation by using [71]

$$27 \quad v(k+1) = v(k)e^{j\omega T_s} \quad (10)$$

28 where  $\omega T_s$  means the one-interval ahead angle.

### 31 3.6 Circulating Current Suppression

32 The circulating current caused by the parallel operation of converters also exists in the system regulated by  
33 converter-level MPC methods. Although fast dynamic response and high robustness can be achieved when using  
34 converter-level FCS-MPC, owing to the variable switching frequency, circulating current cannot be completely  
35 neglected. Unnecessary circulating current will increase the converter power loss, reduce system efficiency and  
36 damage electronic device. Recently, some studies have investigated the alleviation of circulating current on  
37 converter level through improving the MPC algorithms. An approach to suppress the circulating current through  
38 adjusting the weighting coefficients of the cost function was proposed in Ref. [72], where the coefficients are set  
39 according to the circulating current based on a preset switching table. Also, the MPC switching states are  
40 grouped according to the contribution of alternative switching states to the circulating current magnitude. Thus,  
41 the cost function is solved by only selecting those current-suppressed voltage vectors to restrain the circulating  
42 current. In addition, since the variable switching frequency can cause circulating current, as mentioned  
43 previously, fixing the switching frequency can also mitigate the circulating current. For example, in Ref. [73],  
44 virtual state vectors were added to achieve a constant switching frequency for this purpose.

## 58 4. Microgrid Secondary Control

59 Currently, droop control is extensively used as an effective method for power sharing in primary control.  
60 However, it unavoidably results in frequency/voltage deviations in steady state due to its inherent control  
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1 limitations. To mitigate this problem, secondary control has been developed to eliminate deviations with the  
 2 purpose of improving voltage quality and being connected to the utility grid safely. In this section, MPC-based  
 3 secondary control is investigated and discussed.

#### 4.1 Secondary Control Principle

9 The basic principle of secondary control is to provide additional compensation with the ability to correct the  
 10 primary control reference, in other words, to shift the droop control characteristic curve to reach a new set point.  
 11 This process can be performed by

$$\begin{cases} f = f^* - mP + \Delta f \\ E = E^* - nQ + \Delta E \end{cases} \quad (11)$$

18 where  $\Delta f$  and  $\Delta E$  are the compensation signals.

21 Centralized and distributed methods are the two main categories of secondary control, which are compared in  
 22 Fig. 6. As depicted, centralized secondary control is mainly based on PI methods, which requires centralized and  
 23 complex communication networks to detect the PCC voltage and frequency, suffering from the possible single  
 24 point of failure and inferior reliability. Besides, centralized control is more sensitive to communication delay and  
 25 data loss, posing a risk to the system stability if the compensation signals delivered to primary control deviate  
 26 from required values. Distributed secondary control, in contrast, attracts more interests owing to its high  
 27 reliability and high stability. A sparse communication network with multiple agents is adequate to provide local  
 28 and neighboring information to implement the distributed secondary control. The diagram of distributed  
 29 secondary control using MPC is shown in Fig. 6. In comparison with centralized type, the buses information in  
 30 the DG and its neighbor DGs will be measured. In addition, distributed secondary control facilitates the plug-  
 31 and-play operation.

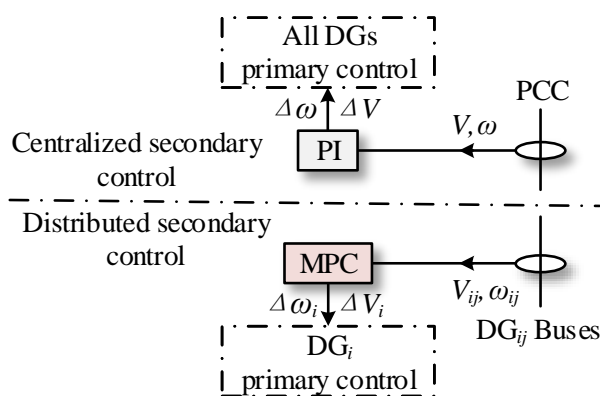


Fig. 6. Diagram of centralized and distributed secondary control.

## 4.2 MPC-Based Secondary Frequency/Voltage Control

For MPC-based secondary control, as previously mentioned, the aim is to produce the required compensation signals  $\Delta f$  and  $\Delta E$  for the droop-based primary control. In line with grid-level MPC architecture, here three key components should be defined: 1) Predictive model is built on the mathematical relationship between future states and past/current states basically from local and/or neighboring systems; 2) The elements of frequency/voltage should be included in cost function; 3) Using specific toolbox to simplify the programming and solving.

In Ref. [20], a MPC method was used for restoring the system frequency. Compared to PI methods, namely conventional PI method and an enhanced PI controller with Smith predictor (SP), it is proved that frequency can reach nominal values with a faster speed but fewer oscillations during load variations. In Ref. [74], a distributed MPC secondary control for both frequency and voltage regulation was developed. Local and neighboring information are required to form predictive models while YALMIP toolbox and Gurobj optimizer are applied as solvers. It is found that the grid-level MPC is robust to various disturbances and perturbations. Similarly, in Ref. [75], MPC was utilized in a distributed manner to realize secondary voltage control.

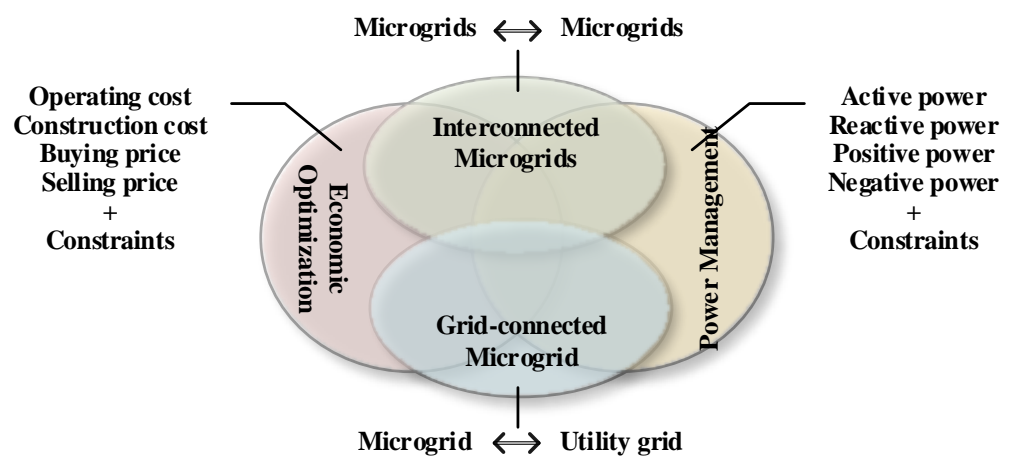
It is worth mentioning that, different from the voltage which varies along distribution line due to the effect of line impedances, the frequency is a global variable in an ac autonomous system. For isolated microgrids, they may present different operating frequencies. Secondary control for frequency compensation is therefore needed to further interconnect multiple microgrids into a microgrid cluster. In Ref. [76], a method using MPC was presented to control the frequency among multiple microgrids. It demonstrates that MPC is better than traditional PI controller when dealing with various disturbances and communication delays. In Ref. [77], a distributed secondary frequency control based on MPC method was proposed, where MPC is used to regulate the frequency by adjusting the voltages of voltage-sensitive loads with the consideration of bus voltage constraints.

## 4.3 Communication Delays

The frequency/voltage compensation signals are produced and delivered through data communication network with diverse bandwidths, capacities and rates. Thus, the network is prone to time delays, which impacts the information integrity and signal update as well as control effectiveness. As a result, the resilience and resistance of the system to communication delays should be considered as a design criterion. Otherwise, the microgrid performance could be compromised with secondary control. Usually, communication delays are time-varying, which increases regulation difficulty. A gain scheduling approach can be used to relieve the delay effect on system dynamic performance [78]. The fast transient response by using MPC in secondary control can also be influenced by the communication delays when the delay is close to a certain boundary, but the robustness can usually be guaranteed [20]. This phenomenon indicates that MPC can be effectively applied to systems as a secondary control even under a severe condition where the communication delays are unknown and complex.

1  
2 **5. Microgrid Tertiary Control**

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4 Tertiary control plays a crucial role in achieving flexible interaction among interconnected/networked  
5 microgrids or between the microgrid and utility grid. Addressing power flow and optimizing economic  
6 operations are the main focuses for this highest control level. In this context, grid-level MPC is mostly applied to  
7 solve the optimization problems with various constraints. Fig. 7 illustrates the main objectives of tertiary control,  
8 where four elements are overlapped with each other meaning that they all have common areas (see following  
9 subsections).  
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13 subsections).



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31 Fig. 7. Main objectives of tertiary control.

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35 **5.1 Tertiary Control Principle**

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37 In order to implement MPC control at a grid level, an integrated mathematical representation of all concerned  
38 parts inside or outside a microgrid is necessary. This is the first step to construct the predictive model with the  
39 consideration of various uncertainties and constraints. Next, a time series based method is used to formulate a  
40 future-value receding equation, which indicates the predicted states based on existing current states. Generally,  
41 forecasting information about DG outputs, electricity prices, and load demands will be involved. Key factors and  
42 emphasized components will be formulated in the cost function aiming to achieve power flow optimization,  
43 operating cost minimization and DG output efficiency maximization. The power flow management and  
44 optimization are the questions as to how the load demands should be shared among various power sources and/or  
45 energy storages, simultaneously giving full consideration to power loss minimization, power generation  
46 maximization and power storage optimization. The algorithm is usually solved by using a specific solver toolbox,  
47 which is similar to the secondary control.  
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57 The benefits of utilizing MPC for tertiary control in microgrids can be summarized as 1) multiple objectives  
58 can be involved in an intuitive and a direct way into the cost function with a straightforward quadratic  
59 summation; 2) various constraints can be comprehensively considered with suitably limited ranges; 3) an  
60 effective specific toolbox with a powerful solver is available to facilitate the algorithm solving process, which is  
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1 particularly useful in tertiary-level control with complex formulations and various constraints.

## 4 5.2 MPC-Based Power Management & Economic Optimization

6 In a practical schedule of power flows inside or outside microgrids, specific conditions must be met. Among  
7 them, pursuing economic interests is a prominent example. This economic optimization relevant to power  
8 management is common in the interaction between the microgrid and the power system. For instance, in Ref.  
9 [21], MPC was adopted for the power flow optimization of a grid-connected microgrid. Five cost-related parts  
10 are considered in the cost function, as expressed in (12), i.e. buying and selling prices of electricity (1st and 2nd  
11 terms), fuel consumption cost (3rd term), and generator start-up cost (4th term). Additionally, one more term  
12 regarding battery energy was also involved (5th term).

$$\begin{aligned}
 J^*(\zeta(k), \bar{\mathbf{P}}_{PV}(k), \bar{\mathbf{P}}_L(k), \bar{\mathbf{c}}_{Imp}(k), \bar{\mathbf{c}}_{Exp}(k)) = \\
 \min \sum_{i=0}^{N-1} [\underbrace{\Delta T \bar{c}_{Imp} P_{eImp}(k+i)}_{1st} - \underbrace{\Delta T \bar{c}_{Exp} P_{eExp}(k+i)}_{2nd} \\
 + \underbrace{\Delta T c_G \mathbf{F}^T \mathbf{k}_G(k+i)}_{3rd} + \underbrace{c_s c_G k_s(k+i)}_{4th}] - \underbrace{c_B V_{nom} Q \zeta(k+N)}_{5th}
 \end{aligned} \tag{12}$$

13 In (12),  $\zeta(k)$  is the state of charge (SOC) of the battery,  $\bar{\mathbf{P}}_{PV}(k)$  the PV generation forecasts,  $\bar{\mathbf{P}}_L(k)$  the load  
14 demand forecasts,  $\bar{\mathbf{c}}_{Imp}(k)$  the import price forecasts,  $\bar{\mathbf{c}}_{Exp}(k)$  the export price forecasts,  $N$  the number of  
15 samples,  $\Delta T$  the sampling time,  $P_{eImp}$  the import power from the grid,  $P_{eExp}$  the export power to the grid,  $c_G$  the  
16 cost of generator fuel,  $c_s$  the penalty of start-up fuel,  $c_B$  the stored energy value of the battery,  $V_{nom}$  the nominal  
17 voltage of the battery and  $Q$  the capacity of the battery.

18 To better dispatch the power energy, a whole microgrid considering power storages and power demands was  
19 modeled in Ref. [79] to build the MPC predictive model. A distributed MPC for microgrid power management  
20 was proposed in Ref. [80], which takes both economic and environmental impacts into the cost function. In Ref.  
21 [81], a distributed MPC considering the cost/benefit of energy sources, the cost from the imbalance between  
22 power supply and load demand, the cost of the power exchange with the main grid, and operation cost/benefit of  
23 batteries was developed to achieve an economic optimization. In Ref. [82], a novel distributed economic MPC  
24 approach was proposed to optimize microgrid users' benefits, where the cost of buying energies from or selling  
25 energies to the microgrid was formulated into the cost functions. In Ref. [83], a stochastic MPC method  
26 balancing microgrid power and predefining exchange power was developed to calculate the optimal power  
27 references for wind generators and electric vehicles.

## 56 5.3 Grid-level MPC for Islanded Microgrids

58 The operational optimization of an islanded microgrid is highly crucial due to not only the difficulty of  
59 internal regulation of uncertain and intermittent renewable energies but also the concern of operating cost and  
60 economic benefit. Therefore, a grid-level optimization for islanded microgrids is also needed.

63 In Ref. [84], a two-layer MPC was presented for the optimization of an islanded microgrid, where seasonal  
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1  
2 auto regression integrated moving average model (SARIMA) and exponential smoothing are used to form the  
3 predictive model, and discrete dynamic programming is adopted to execute the algorithm. In Ref. [85], MPC was  
4 used for the power flow optimization with a cost function considering the load consumption, power line loss, and  
5 battery discharge/charge. The algorithm is solved by using YALMIP toolbox with CPLEX solver. A two-layer  
6 distributed MPC scheme was proposed in Ref. [86] to regulate an islanded dc microgrid. The upper-layer MPC  
7 coordinates parallel dc-dc converters, while the lower-layer MPC manipulates wind generator controllers.  
8 Similarly in Ref. [87], MPC was utilized to control power flows coordinating with the ESS in an islanded  
9 microgrid. The power losses from line resistances, filter resistances and batteries are taken into account, the  
10 solving algorithms are using CPLEX solver and YALMIP toolbox.

#### 18 5.4 Grid-level MPC for Networked Microgrids

20 Networked microgrids, which are a cluster of electrically interconnected microgrids to accommodate more  
21 RESs and loads, now have become a growing concern. This networked architecture enables mutual peer power  
22 support among small ac/dc microgrids and promotes the usage of renewable energies [88]. To facilitate this  
23 interaction, DNO and distribution energy management system (DEMS) are usually necessary for  
24 generating/transmitting control commands and regulating power flows. In contrast to individual microgrids, the  
25 power coordination of networked microgrids becomes more complex, resulting in a higher demand for more  
26 efficient power optimization.

27 In Ref. [89], a centralized MPC was applied to coordinate the power flow among a microgrid network. The  
28 predictive model is constrained with an upper and a lower limits. The cost function has two parts, both related to  
29 the energy sold or purchased, the first one is about adjacent microgrids while the second one about the utility  
30 grid. In Refs. [90] and [91], MPC was used to minimize the operating expense and keep the power balance  
31 simultaneously under the uncertainties from both the supply and demand sides. The dynamic receding-horizon  
32 procedure of the MPC enables appropriate actions to address various constraints. A distributed MPC was  
33 proposed in Ref. [22] to maximize the economic benefit and simultaneously minimize the degradation of storage  
34 systems subjected to diverse constraints. These are solved by using TOMLAB/CPLEX solver.

35 For a better visualization and understanding, the above major MPC methods adopted in microgrids are  
36 summarized in Table 1, which are categorized in terms of control levels, control layers, predictive models, cost  
37 functions and solving algorithms.

38 Table 1 Summary of MPC methods in Microgrid Applications.

39 Control levels	40 Control layers	41 Predictive models	42 Objectives in cost functions	43 Solving algorithms	44 Relevant references (e.g.)
45 Converter-level	46 Primary control	47 Dynamics of converters and <i>RLC</i> circuits	48 Converter outputs: voltage, current, active power, reactive power, circulating currents	49 Exhaustive search (FCS-MPC, CCS-MPC)	50 Refs. [14], [17], [60-62]



Grid-level	Secondary control	Topology features, forecast and dynamics of DGs, ESSs, and load demand	Compensation of frequency and voltage, grid synchronization	Specific toolbox & solver (e.g. TOMLAB, CPLEX, YALMIP)	Ref. [74]
	Tertiary control		Power flows, operational cost, economic benefit, power loss, etc.		Refs. [22], [85], [87]

Besides, the highlights of reviewed representative MPC methods are compared in Table 2 where the applications, advantages and disadvantages are involved.

Table 2 Advantages and disadvantages of reviewed MPC methods.

MPC methods	Applications	Advantages	Disadvantages	Relevant references
Converter-level MPC voltage & power control	Interlinking converter	Enable stable operation of microgrids, flexible power regulation and grid support	Coordinated control under different cases is challenging	Ref.[14]
Converter-level MPC voltage & power control	dc-dc & dc-ac converters	dc-bus voltage shows less oscillation; inverters' power sharing is faster and smoother	Need more additional measurements	Ref.[17]
Converter-level MPC with virtual space vectors	Three-level neutral-point clamped inverters	Dynamic response is fast, controller design is simple and harmonic distortion is reduced	Increased cost of switching losses	Ref.[18]
Grid-level MPC considering communication delays	Restoring microgrid system frequency	Faster speed with fewer oscillations	Possible slightly slower dynamic performance	Ref.[20]
Grid-level distributed MPC with day-ahead operation	Maximize economic benefit and minimize storage system degradation	Improved economical benefits and maximized storage system lifetime	Different system constraints should be fulfilled	Ref.[22]
Grid-level distributed economic MPC	Coordinated stochastic multi-microgrids energy management	Successfully reduce the system operating cost with supply-demand balance	System-wide operating cost will be slightly higher than centralized scheme	Ref.[29]
Converter-level MPC current control	Bidirectional three-level dc/dc converter	Significantly reduced power switch and inductor ratings, significantly reduced inductor current ripple	Small dc-bus voltage-level fluctuations	Ref.[37]
Converter-level MPC with current and SOC constraints	Bidirectional single-inductor multiple-port converter	It has smaller size, less component and lower cost. It presents better performance when integrating into dc microgrids	Need a move-blocking technique and enumeration method	Ref.[51]
Converter-level MPC with improved cost function	Voltage source converter	Transient response is superior, system is robust to parameter variation and voltage supply is significantly improved	Lack of theoretical analysis of MPC stability	Ref.[62]
Grid-level distributed MPC	Secondary frequency and voltage regulation	Robust to various disturbances and perturbations	Specific solution algorithm is used which may limit the application	Ref.[74]
Grid-level distributed economic MPC	Economic optimization of the wind-photovoltaic-battery microgrid	System economic benefit and system stability are improved with less computation time	Dual-mode MPC method is used, which will be more complicated than the traditional method	Ref. [81]

Grid-level centralized MPC	Coordinate the power flow inside microgrid networks	Minimizing the exchange between microgrids and maximizing the utilization of renewable energy	Need the forecasting information about energy prices, production power, and loads	Ref. [89]
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## 6. Current challenges in Predictive Control in Microgrids

Although MPC presents many benefits in the hierarchical control of microgrids, it also has challenges and limitations that could degrade its control performance and limit its scalability. The following aspects about MPC predictive model, sampling interval, stability, and cost function design are covered. Besides, the possible solution for each challenge is provided.

### 6.1 Predictive Model

The modeling quality and accuracy of the predictive model directly impact control performances, in this sense, the development of predictive model is always fundamental and crucial [92]. Predictive model needs to build the connection between future output variables and current/past input variables. There are many ways to design predictive models, among them, discretization process is often used to discretize the model for a better controller application. Commonly, for converter-level MPC, Euler approximation (like Euler forward approximation) and Taylor series expansion are adopted. However, in either discretizing situation, there is always a tradeoff between the model accuracy and calculation complexity [93][94]. Thus, how to effectively balance this tradeoff is a challenge. This problem can be effectively solved by using a powerful processor. In such case, accurate model and fast algorithm solution can be both satisfied.

### 6.2 Sampling Interval

The design of the sampling interval is another issue if the predictive model is executed in a discretization manner, which is suitable for not only converter-level MPC but also grid-level MPC. For converter-level MPC, usually, zero-order holders and observers are utilized for the sampling [74][76]. For the implementation, observers have more flexibility and can possess more functionalities. In general, a better performance will be achieved when a smaller sampling time is set, however, which results in a heavier computational burden and a possible lower economic efficiency. While for grid-level MPC, as aforementioned, forecasts are generally needed. In terms of data acquisition, the precision of forecasts along with the errors between forecasts and actual values will impact the optimization accuracy. In order to reduce these effects, more accurate short-term predictions can be carried out to achieve better updates [95].

### 6.3 Stability

Stability is highly important for microgrids, especially operating in autonomous operation. So far, the stability analysis about the combination of droop control and CLC has been more mature and comprehensive than the combination of droop control and converter-level MPC. On the other hand, until now, converter-level MPC itself

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2 has still lacked a standard theoretical mode for the stability analysis. Even though Lyapunov concept has been  
3 applied to the analysis of converter-level MPC, extensive verification is still needed [27][96]. Currently, in order  
4 to evaluate the robustness and stability of converter-level MPC, the essential factors of RLC behaviors  
5 formulated in predictive models are tested. In these trials, the control parameters are continuously altered in the  
6 processor settings while maintaining the real components unvaried [62][71].  
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## 10 11 *6.4 Cost Function Design*

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13 As previously mentioned, usually, for an exhaustive control target, many items will be covered in the cost  
14 function. The items might be the active power and reactive power controls for a converter-level MPC under a  
15 microgrid grid-connected operation; and multi-factors like operational cost, voltage quality, power loss and  
16 economic benefit for a grid-level MPC. All these control objectives along with diverse constraints must be  
17 reflected in the cost function. In this case, the design, arrangement and allocation of these items become a real  
18 challenge.  
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24 In addition, how to effectively set the weighting factors of the polynomial cost function is still under  
25 development. For example, as stated in Ref. [97], just heuristically tuning the weighting coefficients, or simply  
26 setting the same value to the two objectives in the cost function is a questionable practice. Generally, this will  
27 deteriorate the current total harmonic distortion (THD) and the closed-loop performance. As aforementioned in  
28 Subsection 3.5, intelligent algorithms such as fuzzy logic control can be used to optimize the weighting  
29 coefficients.  
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## 36 **7. Future Trends**

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38 With the rapid increasing penetration level of RESs in the low voltage distribution network, the existing  
39 power system is in the transformation from centralized-control bulky systems to decentralized smart systems  
40 with the microgrids as building blocks. These new development trends and directions indicate the new  
41 requirements for superior control schemes. In this context, as previously stated, MPC will be competitive and  
42 promising to meet the urgent need of future grid. And the following areas will likely be the research focuses in  
43 the following years.  
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### 50 *7.1 New Mathematical Formulation*

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52 In fact, the mathematical model of MPC can be represented in either impulse response form, or transfer  
53 function form, or state-space form [98]. At present, predictive models are usually described in state-space forms.  
54 Actually, there exist other alternatives to rewrite the model state, like Laguerre functions used in Ref. [99]. The  
55 results show that this alternative method drastically reduces the number of optimizing variables without any  
56 degradation of transient response. On the other hand, for the grid-level MPC, the future-value receding model  
57 can be adopted for the predictive model like the controlled autoregressive moving average (CARMA) model in  
58 Ref. [100] which can produce steps-ahead prediction for multiple-input multiple-output systems, and the input-  
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2 output feedback linearization (IOFL) in Ref. [101] which facilitates the predictive model design without  
3 considering the prior steady-state operating point, as well as the SSARX model establishing an adaptive scheme  
4 to eliminate steady-state offsets in Ref. [94]. In addition, more complicated but more accurate MPC types like  
5 the nonlinear MPC which can better simulate the nonlinear and hybrid target can be considered for future  
6 applications[102][103].  
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## 10 11 *7.2 Holistic and Intelligent MPC Approaches*

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13 Currently, there is still a gap in MPC of microgrids between the research of power electronics and power  
14 systems. The existing research, on the one hand, focuses on the regulation of power converters, but the effect of  
15 the grid is seldom considered. On the other hand, system-level power flow control of the network with high PV  
16 penetration has been investigated, however, the details of converter topologies and their switching methods are  
17 not taken into account. There is a need to develop holistic MPC approaches that can deal with power converter  
18 control at the bottom and the power flow on the top. Meanwhile, MPC will incorporate with other methods such  
19 as fuzzy logic control and multi-agent system control to gain more control flexibility and intelligence.  
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## 26 27 *7.3 MPC in dc Microgrids*

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29 After losing the battle with ac distribution for centuries, now dc distribution is likely to win back with the fast  
30 development of power electronic converter technologies and proliferation of dc generation and dc loads. DC  
31 microgrids offer many advantages including higher efficiency and reliability [85][86]. Also, dc microgrids  
32 facilitate plug and play features and enable simpler integration of RESs. Therefore, dc microgrids and the  
33 associated MPC methods tend to be one of the major research areas in the next decades. For example, in a PV-  
34 dominant microgrid, in order to better manage power flows, an ESS system with bidirectional dc-dc conversion  
35 is also usually equipped. PV and ESS systems are interconnected via dc bus. Their associated dc-type converters  
36 can be regulated by using converter-level MPC control, while using grid-level MPC on top to coordinate their  
37 interactions.  
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## 45 46 *7.4 MPC in Networked Microgrids*

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48 Converter-level MPC techniques are relatively mature as they have been widely studied and applied in the  
49 primary control layer. However, grid-level MPC in the tertiary control layer dealing with power flow and  
50 economic operation still needs further development. In the future, islanded microgrids that are geographically  
51 adjacent to each other are more likely to be networked to constitute microgrid clusters with additional flexibility  
52 for resilient operations. Each microgrid in the network is able to choose when and how to be interconnected and  
53 to exchange power with others. Under this new grid architecture, new MPC strategies are highly desired to  
54 optimize the power flows within the microgrid cluster to achieve overall optimal economic power dispatch with  
55 general stability of load frequency and voltage.  
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## 8. Conclusion

In this paper, the state-of-the-art studies on the predictive control in microgrids have been reviewed. First, the basic principle of predictive control is presented. After that, recent converter-level and grid-level technologies are investigated. These predictive control approaches have been applied in three different control layers of the hierarchical control of microgrids. Major benefits, such as faster dynamic responses in lower control level and flexible integration of various objectives in higher control level, have been discussed. Also, the current challenges and limitations of predictive control have been analyzed. Finally, future perspectives of this emerging area have been pointed out. With the on-going development of power electronic techniques and the increasing penetration level of distributed renewable energies into the existing power network, the authors believe more advanced predictive control with new mathematical formulation and holistic intelligent scheme tends to play a significant role in microgrids, particularly in promising areas such as dc microgrids and networked microgrids.

## References

- [1] Blaabjerg F, Teodorescu R, Liserre M, Timbus A V. Overview of control and grid synchronization for distributed power generation systems. *IEEE Trans Ind Electron* 2006;53:1398–409. <https://doi.org/10.1109/TIE.2006.881997>.
- [2] Hu J, Li Z, Zhu J, Guerrero JM, Voltage stabilization: a critical step toward high photovoltaic penetration. *IEEE Ind. Electron. Mag* 2019; 13:17-14. <https://doi.org/10.1109/MIE.2019.2906844>.
- [3] Sinha S, Chandel SS. Review of recent trends in optimization techniques for solar photovoltaic-wind based hybrid energy systems. *Renew Sustain Energy Rev* 2015;50:755–69. <https://doi.org/10.1016/j.rser.2015.05.040>.
- [4] Lasseter RH. *MicroGrids*. Proc. IEEE Power Eng. Soc. Transm. Distrib. Conf., 2002.
- [5] Hatzigiargyriou N, Asano H, Iravani R, Marnay C. *Microgrids*. *IEEE Power Energy Mag* 2007;5:78–94. <https://doi.org/10.1109/MPAE.2007.376583>.
- [6] Guerrero JM, Vasquez JC, Matas J, De Vicuña LG, Castilla M. Hierarchical control of droop-controlled AC and DC microgrids - A general approach toward standardization. *IEEE Trans Ind Electron* 2011;58:158–72. <https://doi.org/10.1109/TIE.2010.2066534>.
- [7] Olivares DE, Mehrizi-Sani A, Etemadi AH, Cañizares CA, Iravani R, Kazerani M, et al. Trends in microgrid control. *IEEE Trans Smart Grid* 2014;5:1905–19. <https://doi.org/10.1109/TSG.2013.2295514>.
- [8] Hirsch A, Parag Y, Guerrero J. *Microgrids: A review of technologies, key drivers, and outstanding issues*. *Renew Sustain Energy Rev* 2018;90:402–11. <https://doi.org/10.1016/j.rser.2018.03.040>.
- [9] Guerrero JM, García de Vicuña L, Matas J, Castilla M, Miret J. Output impedance design of parallel-connected UPS inverters with wireless load-sharing control. *IEEE Trans Ind Electron* 2005;52:1126–35. <https://doi.org/10.1109/TIE.2005.851634>.
- [10] Rocabert J, Luna A, Blaabjerg F, Rodríguez P. Control of power converters in AC microgrids. *IEEE Trans Power Electron* 2012;27:4734–49. <https://doi.org/10.1109/TPEL.2012.2199334>.
- [11] Tayab UB, Roslan MA Bin, Hwai LJ, Kashif M. A review of droop control techniques for microgrid. *Renew Sustain Energy Rev* 2017;76:717–27. <https://doi.org/10.1016/j.rser.2017.03.028>.
- [12] Han Y, Li H, Shen P, Coelho EAA, Guerrero JM. Review of Active and Reactive Power Sharing Strategies in Hierarchical Controlled Microgrids. *IEEE Trans Power Electron* 2017;32:2427–51. <https://doi.org/10.1109/TPEL.2016.2569597>.
- [13] Unamuno E, Barrera JA. Hybrid ac/dc microgrids - Part II: Review and classification of control strategies. *Renew Sustain Energy Rev* 2015;52:1123–34. <https://doi.org/10.1016/j.rser.2015.07.186>.

- 1  
2 [14] Hu J, Xu Y, Cheng KW, Guerrero JM. A model predictive control strategy of PV-Battery microgrid under variable power  
3 generations and load conditions. *Appl Energy* 2018;221:195–203. <https://doi.org/10.1016/j.apenergy.2018.03.085>.
- 4  
5 [15] Barrero F, González A, Torralba A, Galván E, Franquelo LG. Speed control of induction motors using a novel fuzzy sliding-  
6 mode structure. *IEEE Trans Fuzzy Syst* 2002;10:375–83. <https://doi.org/10.1109/TFUZZ.2002.1006440>.
- 7  
8 [16] Kozák Š. From PID to MPC: Control engineering methods development and applications. 2016 *Cybern. Informatics, K I 2016 -*  
9 *Proc. 28th Int. Conf.*, 2016. <https://doi.org/10.1109/CYBERI.2016.7438634>.
- 10  
11 [17] Shan Y, Hu J, Li Z, Guerrero JM. A Model Predictive Control for Renewable Energy Based AC Microgrids Without Any PID  
12 Regulators. *IEEE Trans Power Electron* 2018;33:9122–6. <https://doi.org/10.1109/TPEL.2018.2822314>.
- 13  
14 [18] Alhosaini W, Wu Y, Zhao Y. An Enhanced Model Predictive Control Using Virtual Space Vectors for Grid-Connected Three-  
15 Level Neutral-Point Clamped Inverters. *IEEE Trans Energy Convers* 2019;34:1963–72.  
16 <https://doi.org/10.1109/TEC.2019.2923370>.
- 17  
18 [19] Verma AK, Gooi HB, Ukil A, Tummuru NR, Kollimalla SK. Microgrid frequency stabilization using model predictive  
19 controller. 2016 *IEEE PES Transm. Distrib. Conf. Expo. Am. PES T D-LA 2016, 2017*. <https://doi.org/10.1109/TDC->  
20 [LA.2016.7805637](https://doi.org/10.1109/TDC-LA.2016.7805637).
- 21  
22  
23 [20] Ahumada C, Cárdenas R, Sáez D, Guerrero JM. Secondary Control Strategies for Frequency Restoration in Islanded  
24 Microgrids With Consideration of Communication Delays. *IEEE Trans Smart Grid* 2016;7:1430–41.  
25 <https://doi.org/10.1109/TSG.2015.2461190>.
- 26  
27 [21] Clarke WC, Manzie C, Brear MJ. An economic MPC approach to microgrid control. 2016 *Aust. Control Conf. AuCC 2016,*  
28 *2017*, p. 276–81. <https://doi.org/10.1109/AUCC.2016.7868202>.
- 29  
30 [22] Garcia-Torres F, Bordons C, Ridao MA. Optimal economic schedule for a network of microgrids with hybrid energy storage  
31 system using distributed model predictive control. *IEEE Trans Ind Electron* 2019;66:1919–29.  
32 <https://doi.org/10.1109/TIE.2018.2826476>.
- 33  
34  
35 [23] Shan Y, Hu J, Guerrero JM. A Model Predictive Power Control Method for PV and Energy Storage Systems with Voltage  
36 Support Capability. *IEEE Trans Smart Grid* 2020;11:1018–29. <https://doi.org/10.1109/tsg.2019.2929751>.
- 37  
38 [24] Kouro S, Cortés P, Vargas R, Ammann U, Rodríguez J. Model predictive control - A simple and powerful Method to control  
39 power converters. *IEEE Trans Ind Electron* 2009;56:1826–38. <https://doi.org/10.1109/TIE.2008.2008349>.
- 40  
41 [25] Rodriguez J, Kazmierkowski MP, Espinoza JR, Zanchetta P, Abu-Rub H, Young HA, et al. State of the art of finite control set  
42 model predictive control in power electronics. *IEEE Trans Ind Informatics* 2013;9:1003–16.  
43 <https://doi.org/10.1109/TII.2012.2221469>.
- 44  
45  
46 [26] Vazquez S, Leon JI, Franquelo LG, Rodriguez J, Young HA, Marquez A, et al. Model predictive control: A review of its  
47 applications in power electronics. *IEEE Ind Electron Mag* 2014;8:16–31. <https://doi.org/10.1109/MIE.2013.2290138>.
- 48  
49 [27] Vazquez S, Rodriguez J, Rivera M, Franquelo LG, Norambuena M. Model Predictive Control for Power Converters and  
50 Drives: Advances and Trends. *IEEE Trans Ind Electron* 2017;64:935–47. <https://doi.org/10.1109/TIE.2016.2625238>.
- 51  
52 [28] Zhang Y, Fu L, Zhu W, Bao X, Liu C. Robust model predictive control for optimal energy management of island microgrids  
53 with uncertainties. *Energy* 2018;164:1229–41. <https://doi.org/10.1016/j.energy.2018.08.200>.
- 54  
55 [29] Kou P, Liang D, Gao L. Distributed EMPC of multiple microgrids for coordinated stochastic energy management. *Appl Energy*  
56 *2017*;185:939–52. <https://doi.org/10.1016/j.apenergy.2016.09.092>.
- 57  
58 [30] Hou J, Song Z, Hofmann H, Sun J. Adaptive model predictive control for hybrid energy storage energy management in all-  
59 electric ship microgrids. *Energy Convers Manag* 2019;198. <https://doi.org/10.1016/j.enconman.2019.111929>.
- 60  
61 [31] Mardani MM, Khooban MH, Masoudian A, Dragicevic T. Model Predictive Control of DC-DC Converters to Mitigate the  
62 Effects of Pulsed Power Loads in Naval DC Microgrids. *IEEE Trans Ind Electron* 2019;66:5676–85.  
63  
64  
65

- 1 <https://doi.org/10.1109/TIE.2018.2877191>.
- 2
- 3 [32] Shan Y, Hu J, Liu M, Zhu J, Guerrero JM. Model Predictive Voltage and Power Control of Islanded PV-Battery Microgrids  
4 with Washout Filter Based Power Sharing Strategy. *IEEE Trans Power Electron* 2020;35:1227–38.  
5 <https://doi.org/10.1109/tpel.2019.2930182>.
- 6
- 7 [33] Camacho EF, Bordons C. Model predictive control. *Adv. Textb. Control Signal Process.*, 2007, p. 1–401.  
8 <https://doi.org/10.1201/9781351170802-9>.
- 9
- 10 [34] Alessio A, Bemporad A. A survey on explicit model predictive control. *Lect. Notes Control Inf. Sci.*, vol. 384, 2009, p. 345–  
11 69. [https://doi.org/10.1007/978-3-642-01094-1\\_29](https://doi.org/10.1007/978-3-642-01094-1_29).
- 12
- 13 [35] Bordons C, Montero C. Basic Principles of MPC for Power Converters: Bridging the Gap between Theory and Practice. *IEEE*  
14 *Ind Electron Mag* 2015;9:31–43. <https://doi.org/10.1109/MIE.2014.2356600>.
- 15
- 16 [36] Nguyen HT, Jung JW. Finite control set model predictive control to guarantee stability and robustness for surface-mounted PM  
17 synchronous motors. *IEEE Trans Ind Electron* 2018;65:8510–9. <https://doi.org/10.1109/TIE.2018.2814006>.
- 18
- 19 [37] Zhang X, Wang B, Manandhar U, Beng Gooi H, Foo G. A Model Predictive Current Controlled Bidirectional Three-Level  
20 DC/DC Converter for Hybrid Energy Storage System in DC Microgrids. *IEEE Trans Power Electron* 2019;34:4025–30.  
21 <https://doi.org/10.1109/TPEL.2018.2873765>.
- 22
- 23 [38] Li Z, Cheng KW, Hu J, Modelling of basic dc-dc converters, 7<sup>th</sup> Int. Conf. on Power Electronics Systems and Applications –  
24 smart mobility, power transfer & security (PESA), Hong Kong 2017, p. 1-6. <https://doi.org/10.1109/PESA.2017.8277782>.
- 25
- 26 [39] Cunha RBA, Inomoto RS, Altuna JAT, Costa FF, Di Santo SG, Sguarezi Filho AJ. Constant switching frequency finite control  
27 set model predictive control applied to the boost converter of a photovoltaic system. *Sol Energy* 2019;189:57–66.  
28 <https://doi.org/10.1016/j.solener.2019.07.021>.
- 29
- 30 [40] Li X, Zhang H, Shadmand MB, Balog RS. Model Predictive Control of a Voltage-Source Inverter with Seamless Transition  
31 between Islanded and Grid-Connected Operations. *IEEE Trans Ind Electron* 2017;64:7906–18.  
32 <https://doi.org/10.1109/TIE.2017.2696459>.
- 33
- 34 [41] Guzman R, De Vicuna LG, Camacho A, Miret J, Rey JM. Receding-Horizon Model-Predictive Control for a Three-Phase VSI  
35 with an LCL Filter. *IEEE Trans Ind Electron* 2019;66:6671–80. <https://doi.org/10.1109/TIE.2018.2877094>.
- 36
- 37 [42] Nguyen HT, Jung JW. Disturbance-Rejection-Based Model Predictive Control: Flexible-Mode Design with a Modulator for  
38 Three-Phase Inverters. *IEEE Trans Ind Electron* 2018;65:2893–903. <https://doi.org/10.1109/TIE.2017.2758723>.
- 39
- 40 [43] Ma J, Song W, Wang S, Feng X. Model Predictive Direct Power Control for Single Phase Three-Level Rectifier at Low  
41 Switching Frequency. *IEEE Trans Power Electron* 2018;33:1050–62. <https://doi.org/10.1109/TPEL.2017.2681938>.
- 42
- 43 [44] Zhou D, Tu P, Tang Y. Multivector Model Predictive Power Control of Three-Phase Rectifiers with Reduced Power Ripples  
44 under Nonideal Grid Conditions. *IEEE Trans Ind Electron* 2018;65:6850–9. <https://doi.org/10.1109/TIE.2018.2798583>.
- 45
- 46 [45] Liu X, Wang D, Peng Z. Improved finite-control-set model predictive control for active front-end rectifiers with simplified  
47 computational approach and on-line parameter identification. *ISA Trans* 2017;69:51–64.  
48 <https://doi.org/10.1016/j.isatra.2017.04.009>.
- 49
- 50 [46] Liu Y, Liu Y, Ge B, Abu-Rub H. Interactive Grid Interfacing System by Matrix-Converter-Based Solid State Transformer with  
51 Model Predictive Control. *IEEE Trans Ind Informatics* 2020;16:2533–41. <https://doi.org/10.1109/TII.2017.2679137>.
- 52
- 53 [47] He Z, Guo P, Shuai Z, Xu Q, Luo A, Guerrero JM. Modulated Model Predictive Control for Modular Multilevel AC/AC  
54 Converter. *IEEE Trans Power Electron* 2019;34:10359–72. <https://doi.org/10.1109/TPEL.2019.2895224>.
- 55
- 56 [48] Makhamreh H, Sleiman M, Kukrer O, Al-Haddad K. Lyapunov-Based Model Predictive Control of a PUC7 Grid-Connected  
57 Multilevel Inverter. *IEEE Trans Ind Electron* 2019;66:7012–21. <https://doi.org/10.1109/TIE.2018.2879282>.
- 58
- 59 [49] Mohapatra SR, Agarwal V. Model Predictive Controller With Reduced Complexity for Grid-Tied Multilevel Inverters. *IEEE*  
60  
61  
62  
63  
64  
65

- 1 Trans Ind Electron 2019;66:8851–5. <https://doi.org/10.1109/TIE.2018.2866115>.
- 2
- 3 [50] Manoharan MS, Ahmed A, Park J-H. An Improved Model Predictive Controller for 27-level Asymmetric Cascaded Inverter  
4 Applicable in High Power PV Grid-Connected Systems. *IEEE J Emerg Sel Top Power Electron* 2019;1–1.  
5 <https://doi.org/10.1109/jestpe.2019.2935536>.
- 6
- 7 [51] Wang B, Xian L, Manandhar U, Ye J, Zhang X, Gooi HB, et al. Hybrid energy storage system using bidirectional single-  
8 inductor multiple-port converter with model predictive control in DC microgrids. *Electr Power Syst Res* 2019;173:38–47.  
9 <https://doi.org/10.1016/j.epsr.2019.03.015>.
- 10
- 11
- 12 [52] Dekka A, Narimani M. Capacitor Voltage Balancing and Current Control of a Five-Level Nested Neutral-Point-Clamped  
13 Converter. *IEEE Trans Power Electron* 2018;33:10169–77. <https://doi.org/10.1109/TPEL.2018.2810818>.
- 14
- 15 [53] Lei J, Feng S, Wheeler P, Zhou B, Zhao J. Steady-State Error Suppression and Simplified Implementation of Direct Source  
16 Current Control for Matrix Converter with Model Predictive Control. *IEEE Trans Power Electron* 2020;35:3183–94.  
17 <https://doi.org/10.1109/TPEL.2019.2928874>.
- 18
- 19
- 20 [54] Judewicz MG, Gonzalez SA, Fischer JR, Martinez JF, Carrica DO. Inverter-side current control of grid-connected voltage  
21 source inverters with LCL filter based on generalized predictive control. *IEEE J Emerg Sel Top Power Electron* 2018;6:1732–  
22 43. <https://doi.org/10.1109/JESTPE.2018.2826365>.
- 23
- 24 [55] Lima DM, Montagner VF, Maccari LA. Generalized predictive control with harmonic rejection applied to a grid-connected  
25 inverter with LCL filter. 14th Brazilian Power Electron. Conf. COBEP 2017, vol. 2018- Janua, 2017, p. 1–6.  
26 <https://doi.org/10.1109/COBEP.2017.8257372>.
- 27
- 28
- 29 [56] Chen J, Chen Y, Tong L, Peng L, Kang Y. A Back-Propagation Neutral Network based Explicit Model Predictive Control for  
30 DC-DC converters with High Switching Frequency. *IEEE J Emerg Sel Top Power Electron* 2020;1–1.  
31 <https://doi.org/10.1109/jestpe.2020.2968475>.
- 32
- 33 [57] Wang J, Tang Y, Lin P, Liu X, Pou J. Deadbeat Predictive Current Control for Modular Multilevel Converters with Enhanced  
34 Steady-State Performance and Stability. *IEEE Trans Power Electron* 2019;1–1. <https://doi.org/10.1109/tpel.2019.2955485>.
- 35
- 36 [58] Xiao D, Alam KS, Norambuena M, Rahman MF, Rodriguez J. Modified Modulated Model Predictive Control Strategy for a  
37 Grid-Connected Converter. *IEEE Trans Ind Electron* 2020;1–1. <https://doi.org/10.1109/tie.2020.2965457>.
- 38
- 39 [59] He J, Li YW, Munir MS. A flexible harmonic control approach through voltage-controlled DG-grid interfacing converters.  
40 *IEEE Trans Ind Electron* 2012;59:444–55. <https://doi.org/10.1109/TIE.2011.2141098>.
- 41
- 42 [60] Dragicevic T, Heydari R, Blaabjerg F. Super-high bandwidth secondary control of AC microgrids. *Conf. Proc. - IEEE Appl.*  
43 *Power Electron. Conf. Expo. - APEC*, vol. 2018- March, 2018, p. 3036–42. <https://doi.org/10.1109/APEC.2018.8341533>.
- 44
- 45 [61] Hu J, Shan Y, Xu Y, Guerrero JM. A coordinated control of hybrid ac/dc microgrids with PV-wind-battery under variable  
46 generation and load conditions. *Int J Electr Power Energy Syst* 2019;104:583–92. <https://doi.org/10.1016/j.ijepes.2018.07.037>.
- 47
- 48 [62] Dragicevic T. Model Predictive Control of Power Converters for Robust and Fast Operation of AC Microgrids. *IEEE Trans*  
49 *Power Electron* 2018;33:6304–17. <https://doi.org/10.1109/TPEL.2017.2744986>.
- 50
- 51 [63] Shan Y, Hu J, Chan KW, Fu Q, Guerrero JM. Model Predictive Control of Bidirectional DC-DC Converters and AC/DC  
52 Interlinking Converters-A New Control Method for PV-Wind-Battery Microgrids. *IEEE Trans Sustain Energy* 2019;10:1823–  
53 33. <https://doi.org/10.1109/TSSTE.2018.2873390>.
- 54
- 55 [64] Cortes P, Rodriguez J, Silva C, Flores A. Delay compensation in model predictive current control of a three-phase inverter.  
56 *IEEE Trans Ind Electron* 2012;59:1323–5. <https://doi.org/10.1109/TIE.2011.2157284>.
- 57
- 58 [65] Hu J, Zhu J, Dorrell DG. Model predictive control of inverters for both islanded and grid-connected operations in renewable  
59 power generations. *IET Renew Power Gener* 2014;8:240–8. <https://doi.org/10.1049/iet-rpg.2013.0078>.
- 60
- 61 [66] Hu J, Zhu J, Dorrell DG, “Model predictive control of grid-connected inverters for PV systems with flexible power regulation  
62  
63  
64  
65



- 1 and switching frequency reduction,” *IEEE Trans. Industry Applications*, 2015;51:587-8.
- 2
- 3 [67] Liu X, Wang D, Peng Z. Cascade-Free Fuzzy Finite-Control-Set Model Predictive Control for Nested Neutral Point-Clamped  
4 Converters With Low Switching Frequency. *IEEE Trans Control Syst Technol* 2018.  
5 <https://doi.org/10.1109/TCST.2018.2839091>.
- 6
- 7 [68] Li H, Lin M, Yang G. Fuzzy Logic Based Model Predictive Direct Power Control of Three Phase PWM Rectifier. *ICEMS*  
8 2018 - 2018 21st Int. Conf. Electr. Mach. Syst., 2018, p. 2431–5. <https://doi.org/10.23919/ICEMS.2018.8549359>.
- 9
- 10 [69] Aghdam MM, Aguilera RP, Li L, Zhu J. Fuzzy-based self-tuning model predictive direct power control of grid-connected  
11 multilevel converters. 2017 20th Int. Conf. Electr. Mach. Syst. *ICEMS 2017*, 2017.  
12 <https://doi.org/10.1109/ICEMS.2017.8056425>.
- 13
- 14
- 15 [70] Kayalvizhi S, Vinod Kumar DM. Load frequency control of an isolated micro grid using fuzzy adaptive model predictive  
16 control. *IEEE Access* 2017;5:16241–51. <https://doi.org/10.1109/ACCESS.2017.2735545>.
- 17
- 18 [71] Cortés P, Rodríguez J, Antoniewicz P, Kazmierkowski M. Direct power control of an AFE using predictive control. *IEEE*  
19 *Trans Power Electron* 2008;23:2516–23. <https://doi.org/10.1109/TPEL.2008.2002065>.
- 20
- 21 [72] Zhang Z, Chen A, Xing X, Zhang C. A novel model predictive control algorithm to suppress the zero-sequence circulating  
22 currents for parallel three-phase voltage source inverters. *Conf. Proc. - IEEE Appl. Power Electron. Conf. Expo. - APEC*, vol.  
23 2016- May, 2016, p. 3465–70. <https://doi.org/10.1109/APEC.2016.7468365>.
- 24
- 25
- 26 [73] Nguyen TT, Yoo HJ, Kim HM. Model Predictive Control of Inverters in Microgrid with Constant Switching Frequency for  
27 Circulating Current Suppression. *IEEE Reg. 10 Annu. Int. Conf. Proceedings/TENCON*, vol. 2018- Octob, 2019, p. 1566–71.  
28 <https://doi.org/10.1109/TENCON.2018.8650549>.
- 29
- 30 [74] Lou G, Gu W, Xu Y, Cheng M, Liu W. Distributed MPC-Based Secondary Voltage Control Scheme for Autonomous Droop-  
31 Controlled Microgrids. *IEEE Trans Sustain Energy* 2017;8:792–804. <https://doi.org/10.1109/TSTE.2016.2620283>.
- 32
- 33 [75] Guo Z, Li S, Zheng Y. Distributed model predictive control for secondary voltage of the inverter-based microgrid. *Chinese*  
34 *Control Conf. CCC*, 2017, p. 4630–4. <https://doi.org/10.23919/ChiCC.2017.8028085>.
- 35
- 36 [76] Wang X, Zhao Q, He B, Wang Y, Yang J, Pan X. Load frequency control in multiple microgrids based on model predictive  
37 control with communication delay. *J Eng* 2017;2017:1851–6. <https://doi.org/10.1049/joe.2017.0652>.
- 38
- 39 [77] Liu K, Liu T, Tang Z, Hill DJ. Distributed MPC-Based Frequency Control in Networked Microgrids with Voltage Constraints.  
40 *IEEE Trans Smart Grid* 2019;10:6343–54. <https://doi.org/10.1109/TSG.2019.2902595>.
- 41
- 42 [78] Liu S, Wang X, Liu PX. Impact of Communication Delays on Secondary Frequency Control in an Islanded Microgrid. *IEEE*  
43 *Trans Ind Electron* 2015;62:2021–31. <https://doi.org/10.1109/TIE.2014.2367456>.
- 44
- 45 [79] Nassourou M, Puig V, Blesa J, Ocampo-Martinez C. Economic model predictive control for energy dispatch of a smart micro-  
46 grid system. 2017 4th Int. Conf. Control. Decis. Inf. Technol. *CoDIT 2017*, vol. 2017- Janua, 2017, p. 944–9.  
47 <https://doi.org/10.1109/CoDIT.2017.8102719>.
- 48
- 49
- 50 [80] Zheng Y, Li S, Tan R. Distributed Model Predictive Control for On-Connected Microgrid Power Management. *IEEE Trans*  
51 *Control Syst Technol* 2018;26:1028–39. <https://doi.org/10.1109/TCST.2017.2692739>.
- 52
- 53 [81] Jia Y, Dong ZY, Sun C, Chen G. Distributed Economic Model Predictive Control for a Wind-Photovoltaic-Battery Microgrid  
54 Power System. *IEEE Trans Sustain Energy* 2019;1–1. <https://doi.org/10.1109/tste.2019.2919499>.
- 55
- 56 [82] Zhang X, Bao J, Wang R, Zheng C, Skyllas-Kazacos M. Dissipativity based distributed economic model predictive control for  
57 residential microgrids with renewable energy generation and battery energy storage. *Renew Energy* 2017;100:18–34.  
58 <https://doi.org/10.1016/j.renene.2016.05.006>.
- 59
- 60
- 61 [83] Kou P, Feng Y, Liang D, Gao L. A model predictive control approach for matching uncertain wind generation with PEV  
62 charging demand in a microgrid. *Int J Electr Power Energy Syst* 2019;105:488–99.  
63  
64  
65

- 1  
2 <https://doi.org/10.1016/j.ijepes.2018.08.026>.
- 3 [84] Sachs J, Sawodny O. A Two-Stage Model Predictive Control Strategy for Economic Diesel-PV-Battery Island Microgrid  
4 Operation in Rural Areas. *IEEE Trans Sustain Energy* 2016;7:903–13. <https://doi.org/10.1109/TSTE.2015.2509031>.
- 5  
6 [85] Morstyn T, Hredzak B, Agelidis VG. Dynamic optimal power flow for DC microgrids with distributed battery energy storage  
7 systems. *ECCE 2016 - IEEE Energy Convers. Congr. Expo. Proc.*, 2016. <https://doi.org/10.1109/ECCE.2016.7855059>.
- 8  
9 [86] Kou P, Liang D, Gao L. Distributed Coordination of Multiple PMSGs in an Islanded DC Microgrid for Load Sharing. *IEEE*  
10 *Trans Energy Convers* 2017;32:471–85. <https://doi.org/10.1109/TEC.2017.2649526>.
- 11  
12 [87] Morstyn T, Hredzak B, Aguilera RP, Agelidis VG. Model Predictive Control for Distributed Microgrid Battery Energy Storage  
13 Systems. *IEEE Trans Control Syst Technol* 2018;26:1107–14. <https://doi.org/10.1109/TCST.2017.2699159>.
- 14  
15 [88] Zhou X, Zhou L, Chen Y, Guerrero JM, Luo A, Wu W, et al. A microgrid cluster structure and its autonomous coordination  
16 control strategy. *Int J Electr Power Energy Syst* 2018;100:69–80. <https://doi.org/10.1016/j.ijepes.2018.02.031>.
- 17  
18 [89] Hajar K, Hably A, Bacha S, Elrafhi A, Obeid Z. An application of a centralized model predictive control on microgrids. 2016  
19 *IEEE Electr. Power Energy Conf. EPEC 2016*, 2016. <https://doi.org/10.1109/EPEC.2016.7771775>.
- 20  
21 [90] Yang X, He H, Zhang Y, Chen Y, Weng G. Interactive Energy Management for Enhancing Power Balances in Multi-  
22 Microgrids. *IEEE Trans Smart Grid* 2019;10:6055–69. <https://doi.org/10.1109/TSG.2019.2896182>.
- 23  
24 [91] Yang X, Zhang Y, He H, Ren S, Weng G. Real-Time Demand Side Management for a Microgrid Considering Uncertainties.  
25 *IEEE Trans Smart Grid* 2019;10:3401–14. <https://doi.org/10.1109/TSG.2018.2825388>.
- 26  
27 [92] Sedhom BE, El-Saadawi MM, Hatata AY, Alsayyari AS. Hierarchical control technique-based harmony search optimization  
28 algorithm versus model predictive control for autonomous smart microgrids. *Int J Electr Power Energy Syst* 2020;115.  
29 <https://doi.org/10.1016/j.ijepes.2019.105511>.
- 30  
31  
32 [93] Vaclavek P, Blaha P. PMSM model discretization for model predictive control algorithms. 2013 *IEEE/SICE Int. Symp. Syst.*  
33 *Integr. SII 2013*, 2013, p. 13–8. <https://doi.org/10.1109/sii.2013.6776649>.
- 34  
35 [94] Perez A, Yang Y. Adaptive model predictive control based on the steady state constrained ARX model. 2018 *IEEE Green*  
36 *Energy Smart Syst. Conf. IGESSC 2018*, 2018. <https://doi.org/10.1109/IGESC.2018.8745552>.
- 37  
38 [95] Ouammi A, Achour Y, Zejli D, Dagdougui H. Supervisory Model Predictive Control for Optimal Energy Management of  
39 Networked Smart Greenhouses Integrated Microgrid. *IEEE Trans Autom Sci Eng* 2020;17:117–28.  
40 <https://doi.org/10.1109/TASE.2019.2910756>.
- 41  
42 [96] Aguilera RP, Quevedo DE. Predictive control of power converters: Designs with guaranteed performance. *IEEE Trans Ind*  
43 *Informatcs* 2015;11:53–63. <https://doi.org/10.1109/TII.2014.2363933>.
- 44  
45 [97] Karamanakos P, Geyer T. Guidelines for the Design of Finite Control Set Model Predictive Controllers. *IEEE Trans Power*  
46 *Electron* 2019;1–1. <https://doi.org/10.1109/tpel.2019.2954357>.
- 47  
48 [98] Aldaouab I, Daniels M, Ordonez R. Model predictive control energy dispatch to optimize renewable penetration for a  
49 microgrid with battery and thermal storage. 2018 *IEEE Texas Power Energy Conf. TPEC 2018*, vol. 2018- Febru, 2018, p. 1–6.  
50 <https://doi.org/10.1109/TPEC.2018.8312078>.
- 51  
52  
53 [99] Ranga Sai Sessa VPSRV, Kesanakurthy SS. Model predictive control approach for frequency and voltage control of standalone  
54 micro-grid. *IET Gener Transm Distrib* 2018;12:3405–13. <https://doi.org/10.1049/iet-gtd.2017.0804>.
- 55  
56 [100] Jayachandran M, Ravi G. MPC based Secondary Control Strategy for an Islanded AC Microgrid under Linear Loads. *Proc. 4th*  
57 *Int. Conf. Electr. Energy Syst. ICEES 2018*, 2018, p. 644–51. <https://doi.org/10.1109/ICEES.2018.8443273>.
- 58  
59 [101] Lou G, Gu W, Sheng W, Song X, Gao F. Distributed model predictive secondary voltage control of islanded microgrids with  
60 feedback linearization. *IEEE Access* 2018;6:50169–78. <https://doi.org/10.1109/ACCESS.2018.2869280>.
- 61  
62 [102] Hausberger T, Kugi A, Deutschmann A, Eder A, Kemmetmüller W. A nonlinear MPC strategy for AC/DC-converters tailored  
63  
64  
65

1 to the implementation on FPGAs. IFAC-PapersOnLine, vol. 52, 2019, p. 376–81. <https://doi.org/10.1016/j.ifacol.2019.11.809>.  
2  
3 [103] Karthikeyan A, Previsic M, Scruggs J, Chertok A. Non-linear Model Predictive Control of Wave Energy Converters with  
4 Realistic Power Take-off Configurations and Loss Model. CCTA 2019 - 3rd IEEE Conf. Control Technol. Appl., 2019, p. 270–  
5  
6 7. <https://doi.org/10.1109/CCTA.2019.8920640>.  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
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