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Research article

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Edge detection with meta-lens: from one dimension to three dimensions

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Abstract: Meta-lens has successfully been developed for a variety of optical functions. We demonstrate a light-field edge detection imaging system with a gallium nitride achromatic meta-lens array. It enables edge detection from one dimension to three dimensions. The designed metalens array consists of 60 by 60 achromatic meta-lenses, which operate in the visible range from 400 to 660 nm. All of the light field information of objects in the scene can be captured and computed. The focused edge images from one dimension to three dimensions are extracted with depth estimation by image rendering. Three dimensions edge detection is two dimensions edge imaging with depth information. The focused edge images can be obtained by the sub-image reconstruction of the light field image. Our multidimensional edge detection system by achromatic meta-lens array brings novel advantages, such as broadband detection, data volume reduction, and device miniaturization capacity. Results of our experiments show new insight into applications of biological diagnose and robotic

Keywords: edge detection; light field imaging; meta-lens; metasurface.

Mu Ku Chen and Yue Yan contributed equally to this work.

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1 Introduction

Edge detection in imaging processing has been widely used for biomedical and advanced manufacturing characterization and analysis [1, 2]. For vision, edge information and detection are the critical step of imaging and provide further assistance of object recognition. The boundaries of regions and the features of objectives can be obtained by edge detection image processing. For the manufacturing industry, edge detection plays an essential role in defect measurement to control product quality [3, 4]. In biology, edge detection enables the reveal of many interesting biological processes [5, 6]. Typically, one-dimensional (1D) or two-dimensional (2D) edge detection could satisfy the applications mentioned above, requiring a conventional camera to capture a focused image first before applying edge processing or analog optical differentiation [7-14]. While some applications, such as three-dimensional (3D) edge detection with volume imaging microscopy, require multiple focusing at different depths. Thus, a new type of edge detection method that can fully obtain multidimensional light ray information in the scene at one time is much demanded.

Light field imaging is integral photography to capture both the intensity and directions of the incoming light of the objects [15]. Conventional light field cameras used a microlens array to collect light field data of the scene. However, microlens had their inherent disadvantages. It is hard to realize high-quality full-color imaging due to its severe chromatic and sphere abbreviation [16]. Metasurfaces, advanced optical devices in flat optics, consists of subwavelength nanostructures, which is the best candidate to solve these problems for its compact size and strong capability to manipulate the wavefront of light [17–23]. Metasurfaces have been successfully applied in fields, including imaging [24–26], holography [27], beam shaping [28, 29], nonlinear optical enhancement [30], etc. Metasurfaces based on geometry phase for wavefront shaping have attracted much attention because of its high working efficiency and straightforward design concept. The geometry phase-based metasurfaces have also been

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utilized for many applications, such as asymmetric transmission [31], arbitrary polarization control [32], spin angular momentum, and orbital angular momentum sorting [33]. Specifically, the flexible phase modulation of metasurfaces brings new opportunities in imaging [34–36]. Many works related to meta-lens were reported in recent years [37, 38]. However, the chromatic abbreviation in nature still exists. One of the effective design methods of achromatic meta-lens is reported and demonstrated. For solving chromatic aberration, the phase arrangement and phase compensation are realized by combining the geometry phase with the integrated-resonant units (IRUs) [39–42]. The achromatic meta-lens can be used in practical imaging systems according to their flat, ultra-thin, compact size, aberration-free, and optical specification design flexibility. By using this design method, an achromatic meta-lens is fabricated and demonstrated fullcolor imaging [39]. Inspired by nature, an achromatic meta-lens array is used to develop a light field imaging system [41]. This imaging system realized the full-color imaging with depth information.

For edge detection, metasurface can offer this function by several methods [9, 13]. In this paper, we demonstrate using an achromatic meta-lens array for 1D to 3D edge detection. It takes full advantage of the achromatic metalens array and integrates the differential image process method for multiple dimension edge detection. The achromatic meta-lens array consists of 60 by 60 achromatic meta-lenses working in the visible range from 400 to 660 nm. Each meta-lens consists of gallium nitride (GaN) nano-blocks on a sapphire substrate. Multiple edge detection experiments with the specifically designed achromatic meta-lens array are conducted. The focused edge images are obtained at different depths with the rendering algorithm, and the depth of various objects in the scene is resolved.

2 Methods

2.1 Achromatic meta-lens array design and fabrication

The achromatic meta-lens design follows the phase requirement of the focusing lens formula as Eq. (1):

$$\varphi(r,\lambda) = -\left[\frac{2\pi}{\lambda}\left(\sqrt{r^2 + f^2} - f\right)\right] \tag{1}$$

Where φ is the phase requirement, r is the distance away from the meta-lens center, λ is the working wavelength, and f is the focal

length. It reveals that different phases are needed to focus light at the same focal spot with different wavelengths, which is hard to achieve due to the material's natural dispersive property.

Additional phase compensation is introduced to satisfy the required phases for the same focal length within the broadband spectrum, written as Eq. (2):

$$\varphi'(r,\lambda) = -\left[\frac{2\pi}{\lambda_{\text{max}}} \left(\sqrt{r^2 + f^2} - f\right)\right] + \Delta' \varphi_{\text{shift}}(r,\lambda)$$
 (2)

where

$$\Delta' \varphi_{\text{shift}}(r, \lambda) = -\left[2\pi \left(\sqrt{r^2 + f^2} - f\right)\right] \left(\frac{1}{\lambda} - \frac{1}{\lambda_{\text{max}}}\right) + \frac{\alpha}{\lambda} + \beta$$

and $\alpha=\delta \frac{\lambda_{\max},\lambda_{\min}}{\lambda_{\max}-\lambda_{\min}}, \beta=-\delta \frac{\lambda_{\min}}{\lambda_{\max}-\lambda_{\min}}$, and λ_{\max} and λ_{\min} are the maximum and minimum working wavelength, respectively. δ is the largest additional phase shift between λ_{min} and λ_{max} . The first term of Eq. (2) is wavelength-independent, realized through the P-B phase modulation. While the second term of Eq. (2) is both position and wavelengthdependent, realized through the IRU element that has been reported as an efficient method to compensate for the additional required phase [39-41].

According to the above theory, we design and fabricate a 60 by 60 achromatic meta-lens array consists of GaN meta-lenses with individual diameters of 21.65 μm, a focal length of 49 μm within working wavelength 400-660 nm. The GaN building blocks of each achromatic meta-lens are positive and negative nano-antennas with different feature sizes and orientations on the sapphire substrate. The corresponding phase compensations of all designed nano-antennas are listed in Figure S1. The phase compensations of achromatic focusing are arranged from 400 to 660 nm of wavelength. The fabrication step flow of the achromatic meta-lens array is shown in Figure S2. The standard electron beam lithography and dry etching processes with the hard mask are employed to produce nanometer size and high aspect ratio nano-antennas array. More details are shown in the Details of Methods section of the Supplementary material and also could be referred to our previously reported works [39, 41].

2.2 Light field imaging for edge detection from 1D to 3D

The light field imaging with the achromatic meta-lens array for 1D to 3D edge detection is presented in Figure 1. Objects located at different depths are firstly imaged at the front of the meta-lens array with the main lens. The light field raw image through the meta-lens array is captured by the complementary metal oxide semiconductor (CMOS) sensor. The designed focal length of all the achromatic meta-lens is 49 μm . The object distance a is set as 300 μm , the image distance b is about 58.56 µm according to the Gaussian lens law $\frac{1}{a} + \frac{1}{b} = \frac{1}{f_{max}}$. After capturing the light field raw image, one-pixel misplaced selfsubtraction along x-direction enables 1D edge information extraction. Similarly, the 2D edge image could be realized with misplaced self-subtraction along both x and y-direction. Each meta-lens captured the object image with various angles at different spatial positions. The disparities of neighboring images are utilized to extract the object's depth. Multiple edge detection can be realized with a rendering algorithm of light field imaging.

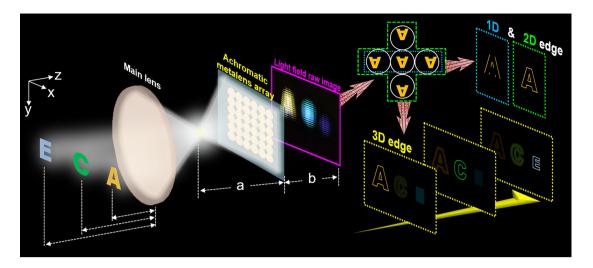


Figure 1: Schematic diagram of multidimensional edge detection with light-field imaging system by the achromatic meta-lens array.

3 Results and discussion

Figure 2a-d are the scanning electron microscope (SEM) images of the achromatic meta-lens array with different magnifications. The positive and negative nanostructures are specifically designed and precisely fabricated. The shape of the fabricated nanostructure slightly unmatches the ideal design due to the slight process parameter deviation. It does not deteriorate the performance of meta-lens from the experimental results. The measured focal length of the achromatic meta-lenses is $49.01 \pm 0.92 \,\mu m$ in the working bandwidth, as shown in Figure S3. The average operation efficiency is of 38.9% which is defined as the ratio of the optical power of the focused circularly polarized beam to the power of the incident light with the opposite circular polarization.

For edge detection imaging, an achromatic meta-lens array-based light-field imaging system is shown in Figure S4. Objects are illuminated by a noncoherent white light. Since the achromatic lens array is polarization sensitive, a linear polarizer (LP) and quarter wavelength plate (QWP) are used to transfer the unpolarized white light to circular polarization. The achromatic meta-lens array collects both the intensity and light field information of the objects. The light-field image is obtained by the CMOS sensor of the commercial camera. Another LP and QWP are used to remove the background noise. This light-field imaging setup with an achromatic meta-lens array enables full-color imaging as well as light-field edge detection from 1D to 3D of the objects. The experimental results of the edge detection are shown in Figure 3. Three patterns of the letter, 'A,' 'C,' and 'E', with the corresponding colors of yellow, green, and blue, respectively, are used as the objects placed at different locations. The light-field raw image collected through the achromatic meta-lens array by CMOS sensor displays 56 by 38 sub-images, as shown in Figure 3a. The disparity of each sub-image of the objects is derived through the surrounding sub-images with a brightness comparison. The depths are calculated using the Euclidean geometry and the disparity. The depth calculation is shown in Figure S5. In our experiments, the number of the subimages is less than the number of the achromatic meta-lens array due to the CMOS sensor's size. Each sub-image consists of 96 by 96 pixels. The zoomed-in image in Figure 3b shows the sub-images of various directions of the 'E' pattern. All directions of the object's light ray information are comprehensively acquired. The clear sub-images show the high imaging quality by our achromatic meta-lens array. The light-field raw image is further processed for the edge detection method. Figure 3c shows the 1D edge imaging results along the x-direction focused at the 'A' pattern. Circle-moving the light-field raw sub-images with one pixel along x or y-direction, then subtract it with the original light-field raw image. The 1D edge information extraction is enabled by displacement of the selfsubtraction. When both x- and y-directions of edge imaging processing are performed, the 2D edge information extraction can be obtained. The rendering algorithm is applied to acquire the multiple dimensions edge images. By selecting the disparity size of the sub-images, rotating 180 degrees of the selected sub-images, then join together all the selected sub-images as the reconstructed edge images at the specific depth. The light field rendering process is shown in Figure S5. According to the rendering algorithm of the light-field imaging, the disparity appears since each sub-image captures the objects from different

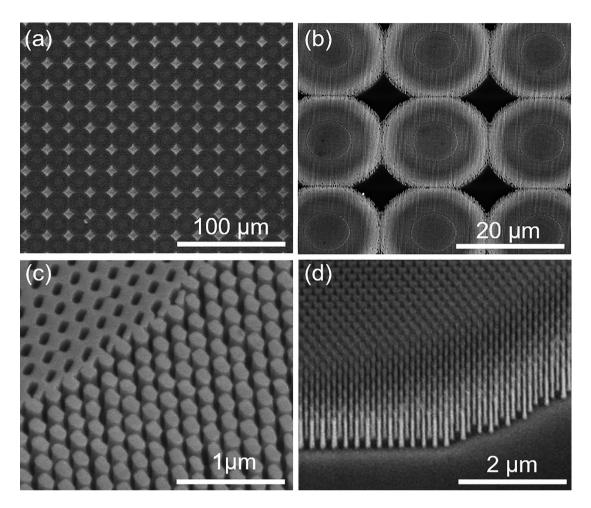


Figure 2: SEM images of the achromatic meta-lens array. (a) and (b) Zoomed-in SEM image of the achromatic meta-lens array. (c) and (d) Tilted-view zoomed-in SEM image of the achromatic meta-lens array. The tilted angle is 30° and 45°, respectively.

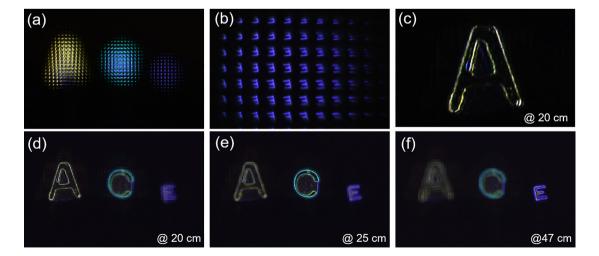


Figure 3: Experimental results of the edge detection light-field imaging. (a) Light field raw image formed by the achromatic meta-lens (b) the partial sub-images of the pattern 'E'. (c) The 1D edge image along the x-direction focused on the pattern 'A'. (d-f) The 3D edge images at different focused depths for patterns, 'A', 'C', and 'E'.

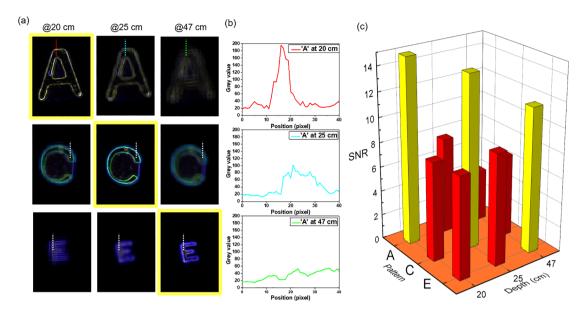


Figure 4: Edge sharpness measurement results of the 3D edge imaging at various depths. (a) The cut-line of the edge sharpness measurement for the SNR calculation. All the dotted lines (red, cyan, green, and white) are the selected regions for the SNR calculation. Rendered images in the same column are focused with depths of 20 cm, 25 cm, and 47 cm, respectively. (b) The edge profiles of pattern 'A' whose rendered images are focused with depths of 20 cm, 25 cm, and 47 cm. The color of the curve corresponds to the color of the dotted cut-line in (a). The edge profiles of the pattern 'C' and 'E' are shown in Figure S9 of Supplementary material. (c) The diagram of the measured SNR of the three patterns with three rendering depths.

directions. A smaller disparity value corresponds to the further distance, which can be used for depth calculation and reconstructing the focused images at different depths. The detail of the edge information extraction process is displayed in Figure S6.

The disparity values of the three patterns 'A', 'C,' and 'E' are calculated as 24, 18, and 13 pixels, respectively, as shown in Figure S7. The corresponding depths are 20 cm, 25 cm, and 47 cm for the pattern 'A,' 'C,' and 'E,' respectively. Figure 3d and e show the 3D edge information of the rendered images at different depths. The 3D edge imaging means the edge detection includes 2D edges at different depths. When the edge imaging is focused at 20 cm, the pattern 'A' has the sharpest edge. While in the other focusing depths, the edges of the pattern 'A' are blurred. Each pattern has the sharpest edge information while the other two letters are blurred at their corresponding depth. The results show the high-quality performance of 3D edge detection with our designed meta-lens array. (More details of the light-field imaging system, rendering algorithm, depth estimation method, 1D to 3D edge detection are discussed in Supplementary material)

We further characterized the 3D edge detection performance of the light-field system with the achromatic metalens array. Figure 4a shows the cut-line of the selected edges of three patterns at different depths. The edge profiles of the pattern 'A' at different imaging depths are shown in Figure 4b. The pattern 'A' is placed at 20 cm of depth, so the edge is clear at this depth than others. 'C' and 'E' have similar scenarios. The measured edge profiles in the embedded images at three corresponding depths for each pattern are shown in Figure S9. The signal-to-noise (SNR) ratios are calculated, and the SNR is defined as the ratio of the maximum signal value to the noise background value. Figure 4c shows the diagram of the measured SNR of the three patterns with three rendering depths. The SNR values of the pattern 'A' are 15, 7.8, and 4.2 at the depth-focused rendering of 20 cm, 25 cm, and 47 cm, respectively. At 20 cm of depth, the pattern 'A' has the sharpest edge with the highest SNR = 15. While in the other depths, edges of the pattern 'A' are blurred with lower SNR. The other two patterns, 'C' and 'E' show a similar situation. Based on the depth of patterns, the edges of the different objects can be clearly identified. It proves that focused, sharp edge images could be obtained within the broadband visible light with high quality. Our experimental results demonstrate multiple dimensional edge detection with an achromatic meta-lens array. It is quite important in imaging and sensing applications, such as 3D cell profile imaging microscopy, autonomous vehicle, advanced manufacture, etc.

4 Conclusions

We demonstrate edge detection from 1D to 3D by a light-field imaging system with an achromatic meta-lens array. The designed 60 by 60 GaN achromatic meta-lens array enables to capture of both intensity and light field information from the objects. The edge and depth of the light field information can be obtained without acquiring sectional data repeatedly. The differentiated and rendering algorithm effectively provides the boundary and the depth information of objects from 1D to 3D. This edge detection light field system has valuable advantages, such as chromatic aberration-free in the visible region, polarization selectivity, multidimensional edge detection, and the semiconductor process capability for mass production. The working band of this edge detection light field system is quite flexible. It can be tuned by changing the meta-lens array with a suitable design and fabrication. The presented 3D edge detection can improve optical characterization capabilities for applications ranging from biomedical diagnose to machine vision.

Author contribution: MKC, YY, and DPT conceived and designed the experiments. MKC designed the samples and fabricated the samples. MKC, YY, XL, YW, and DPT developed the algorithm. MKC, YY, JZ, ZZ, and JY performed optical measurement and imaging experiments. MKC, YY, and DPT prepared the manuscript. All authors analyzed the results and contributed to the preparation of the manuscript and discussions.

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