

1     **Development of a tool to monitor static balance of construction workers for**  
2                                    **proactive fall safety management**

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24 **Abstract**

25 The construction industry around the globe is afflicted with an exorbitant rate of fatal and non-  
26 fatal falls. To lower the propensity of the falls, researchers and safety experts have recommended  
27 to supplement the traditional passive fall safety measures with some active measures (such as  
28 early identification of task/environmental hazards and personal risk factors). Unfortunately, at  
29 present, there is no readily available onsite tool which could identify workers with poor postural  
30 controls. This study aimed to develop a static balance monitoring tool for proactive tracking of  
31 construction workers on-site using a wearable inertial measurement unit (WIMU) and a  
32 smartphone. To this end, a three-phase project was conducted. Firstly, a validation study was  
33 conducted to examine the validity of using WIMUs to detect task/fatigue-induced changes in  
34 static balance during a 20-second static balance test. The results of the study revealed that  
35 WIMUs could detect the post-task subtle changes in static balance with reference to the findings  
36 of a force-plate (considered as industrial standard). Secondly, since there were no existing static  
37 balance classification methods, five experts were engaged to establish balance classification  
38 thresholds using the fuzzy set theory. Thirdly, a mobile phone application was developed for the  
39 managers/foremen for onsite balance monitoring of the construction workers using the 20-second  
40 test at different times of the day and establishing their corresponding balance performance  
41 profiles. This would assist early identification of fall prone workers, plan mitigation schemes  
42 before a fall accident happens and ultimately help reduce falls in the construction industry.

43

44 **Keywords**

45 Fall prevention; Proactive safety; Wearable Inertial Measurement Unit; Construction industry

## 46 **1. Introduction**

### 47 **1.1 Background**

48 Around the globe, fall accidents are a substantial burden and an impediment to accomplish  
49 occupational safety in the construction industry. During the year 2015, falls accounted for 40%  
50 of the total fatal accidents in the US private construction industry [1]. In the UK, almost one-half  
51 of the all industrial fatalities every year are associated with construction fall accidents [2].  
52 Likewise, the fatal fall accidents in the Australian construction industry accounted for more than  
53 one-third of all falls from height fatalities during 2003 to 2015 [3]. Similarly, falls constitute a  
54 major proportion of accidents in the construction industry in China, Hong Kong, South Korea,  
55 Japan and Singapore [4–6]. While statistics indicate that falls result in a considerable number of  
56 fatal injuries, non-fatal fall injuries are also severely afflicting the global construction industry by  
57 placing significant economic, emotional and medical burden on the affected workers, their  
58 families and societies [7]. In addition to the medical expenses, non-fatal falls cause losses to  
59 construction companies in forms of work absenteeism, productivity loss and compensation  
60 claims [7,8]. For example, a typical non-fatal fall accident caused an average of ten days of work  
61 absenteeism in the US construction industry from 1992 to 2000 [9]. Likewise, the highest  
62 number of compensation claims filed in the Hong Kong construction industry were related to  
63 non-fatal falls [10]. Taken together, reducing the risk of falls has become an important priority  
64 for researchers and practitioners alike in the construction industry.

### 65 **1.2 Fall risk assessment in the construction industry**

66 Various methods have been suggested in the literature for fall risk assessment in the construction  
67 industry. Traditionally, these include but are not limited to the review of fall archival data  
68 [11,12], interviews of fall affected workers [13], site inspections [14], schedule oriented  
69 site/work safety plans [15], combined use of virtual reality and 4D construction plans [16,17] and  
70 Building Information Modelling (BIM) integrated safety rules approach [18]. Although  
71 considerable fall prevention efforts have been made, falls still outweigh the other reported  
72 construction accidents [11,19,20]. One possible reason for this phenomenon may be ascribed to  
73 the shortcomings of traditional practices/techniques of fall risk identification, and passive fall  
74 protection measures [21]. For example, the use of archival data may not always reveal the actual  
75 cause of a fall incident because of probable bias, experiences and beliefs of the reporter and the  
76 subjective nature of interpretation [11,22]. Similarly, other methods (such as safety plans) cannot  
77 take into account of the dynamic interactions of workers, machinery and materials, which require  
78 real-time risk identification and mitigation methods [23,24]. More importantly, these risk  
79 methods do not consider personal fall risk factors (such as physiological traits, personal health,  
80 fatigue, age and body mass index) which are considered to be a major contributor to falls  
81 [11,12].

82 Despite the shortcomings of existing risk identification methods, various fall protection measures  
83 have been implemented on construction sites. These include the use of personal fall arrest  
84 systems, installation of guardrails, deployment of safety nets [21,25], hole (openings) coverings  
85 [25], warning-line systems [7] and fall risks scheduling for better risk management [26]. While  
86 these passive measures may prevent workers from falls, they cannot proactively identify risk  
87 factors for loss of balance, or distinguish workers with poor balance ability [23] such that proper

88 training or education can be given. Additionally, under certain situations, the deployment of  
89 aforementioned passive measures becomes nonpragmatic (such as working in a controlled  
90 decking zone) or these measures are not available to construction workers [21,27,28], which in  
91 turn increases the risk of falls.

92 To better strategize against falls, it is essential to develop proactive strategies to identify task and  
93 environment related fall risks and to discern construction workers with poor balance controls  
94 [7,11,23]. Given that many construction trades are labor intensive and physically demanding,  
95 these work tasks may leave the workers susceptible to fatigue, muscle pain and distraction which  
96 could afflict the balance of construction workers [23,29–31]. For instance, it is not uncommon  
97 for construction workers to be involved in heavy manual material handling and working on  
98 sloped surfaces that can disturb their postural stability [23,32–34]. If such fall risks can be  
99 identified proactively, remedial measures could be taken. For example, Umer et al. found that  
100 commonly adopted rebar tying postures in squatting or stooping may lead to the subsequent  
101 suboptimal control of standing balance [23]. Accordingly, they developed an ergonomic  
102 intervention using stool-sitting to significantly improve the standing balance after rebar tying  
103 tasks [23]. Furthermore, it is essential to identify fall risks in construction jobsites because  
104 multiple factors (personal, task-related and environmental risks) may present and interact  
105 concurrently. While each individual risk factor might have a minimal effect on balance control  
106 [35], these factors may interact with one another to compromise the balance of workers [36,37].  
107 In fact, since loss of balance is known to be a major cause of falls on construction sites [21,38–  
108 42], it is paramount to proactively monitor the balance of the construction workers at different  
109 times of the day and plan appropriate mitigation strategies.

### 110 **1.3 Recent related fall prevention studies in the construction industry**

111 Traditionally, the fall prevention research in the construction industry was focused on optimum  
112 utilization of personal safety equipment and other allied fall protections. Lately, with recent  
113 technological advancement, efforts are underway to detect and mitigate fall risk factors before  
114 any accident occurs. Fall risk assessments have been used in health research for a long time. For  
115 example, balance assessments in community-dwelling elderly can provide information about the  
116 necessity of using walking aids and help caretakers taking care of seniors [29]. Likewise, there is  
117 a pressing need to proactively identify fall risk factors in construction workers because fall  
118 incidents in the construction industry could cause serious injuries or fatality [21,41]. Dzens et al.  
119 [29] studied the feasibility of detecting falls and fall portents (unsteady stepping, swaying or loss  
120 of balance) using mobile phone gyroscope and accelerometer. They reported that the  
121 accelerometer data was suitable for future fall and fall portent detection on actual jobsites.  
122 Recently, Fang and Dzens extended their work by attaching multiple accelerometers to various  
123 body parts and utilized a hierarchical threshold-based algorithm to successfully curtail the false  
124 alarm rate for detecting fall portents for tile-fixing [43]. Jebelli et al. [41,44] demonstrated that  
125 wearable inertial measurement units (WIMUs) are sensitive to differentiate between different  
126 static work postures. They recommended the development of a tool to monitor fall risk in future.  
127 Besides exploring fall portents and static postures, studies have also explored the feasibility of  
128 WIMUs to detect fall risks during walking. Jebelli et al. [45,46] experimented with different  
129 walking tasks of varying difficulty levels to assess the capability of a WIMU in distinguishing

130 them. They found that it was able to significantly differentiate difficult walking tasks from the  
131 easier ones. Similarly, Yang et al. [47] successfully employed a semi-supervised learning  
132 algorithm to identify non-stable gait sections during simulated walking on iron beams using  
133 WIMUs. Likewise, Kim et al. [48] and Yang et al.[49] showed that collective acceleration  
134 responses (acquired using WIMUs) from workers could be advantageous in identifying unsafe  
135 locations on a construction site. Building on this concept, they successfully experimented  
136 augmentation of the gait data with spatial (location) information to identify fall hazards on a  
137 worksite [50]. Recently Kim et. al [51] illustrated the use of WIMUs to quantify and differentiate  
138 the risk of slipping caused by various coatings of steel beams. Collectively, these studies have  
139 advanced our understanding pertinent to pro-active monitoring of fall hazards and abnormal gait  
140 patterns.

#### 141 **1.4 Research gap**

142 Despite aforementioned advances, to date, there is no readily available tool that can be deployed  
143 by site managers or foremen to evaluate the static or dynamic balance of the construction  
144 workers on site [41]. Static balance ability is known to be a predictor of: falls in the elderly  
145 community [52], ankle sprains in teenagers [53,54] and prospective falls among construction  
146 workers [23]. Generally, the static balance test requires a person to stand as stable as possible to  
147 keep the movement of his center of gravity at a minimum, usually for a minimum duration of 20-  
148 second [55,56]. Traditionally, force-plates are considered as an industrial standard for static  
149 balance assessment. However, given their excessive weight and size, higher cost, and  
150 requirement of additional electronic and power components, it is not feasible to use them at  
151 construction sites [57].

152 Recent WIMU related fall prevention studies can be broadly classified into two categories: (1)  
153 static and (2) dynamic. Static studies primarily investigated the capability of using WIMU  
154 signals to differentiate different static work postures in a laboratory setting and to detect the risk  
155 of falls during stationary work tasks [29,41,43,44]. On the other hand, dynamic studies explored  
156 the feasibility of using WIMUs to characterize gait patterns under different situations (e.g.  
157 normal walking, obstacle passing, walking on slippery surfaces, walking with a load) based on  
158 data collected from an individual [46,47] or a group of participants [27,45,49–51]. Importantly,  
159 no previous studies have developed tools to evaluate static or dynamic balance of construction  
160 workers as to help identify individuals with poor balance skills and to plan appropriate  
161 preventive measures. Additionally, with respect to static balance, despite the ability of WIMUs  
162 to classify postures [41], it remains unclear whether WIMU can detect temporal changes in static  
163 standing balance induced by construction tasks [tested in the same posture](#). In many instances,  
164 these changes may be unobservable by vision technologies but the detection of such changes  
165 may help predict the risk of fall in future.

166 Accordingly, this study aimed to develop a WIMU based tool to monitor the static balance of the  
167 workers for proactive fall safety management. For the said purpose, a three-stage study was  
168 conducted. Firstly, a laboratory study was conducted to validate the accuracy of WIMUs in  
169 measuring task/fatigue induced changes in the static balance with reference to a force-plate  
170 during a 20-second static balance test. Secondly, five experts were invited to determine the  
171 thresholds of static balance parameters for onsite balance classification of construction workers  
172 using the fuzzy set theory. Finally, based on those suggested thresholds, a mobile application

173 was developed to link WIMU signals to a smartphone for onsite balance evaluation and further  
174 management perusal.

175 To accomplish the outlined objectives, the manuscript is organized as follows. Section 2  
176 delineates methods employed for WIMU based detection of task/fatigue induced changes in  
177 static balance. Next, section 3 reports the results of the study. It is followed by methods and  
178 results for thresholds determination in Section 4 and 5. Section 6 demonstrates the mobile  
179 application developed for the onsite balance assessment. Finally, the discussion is made in  
180 Section 7, followed by the limitations and future works (Section 8) and conclusions (Section 9).

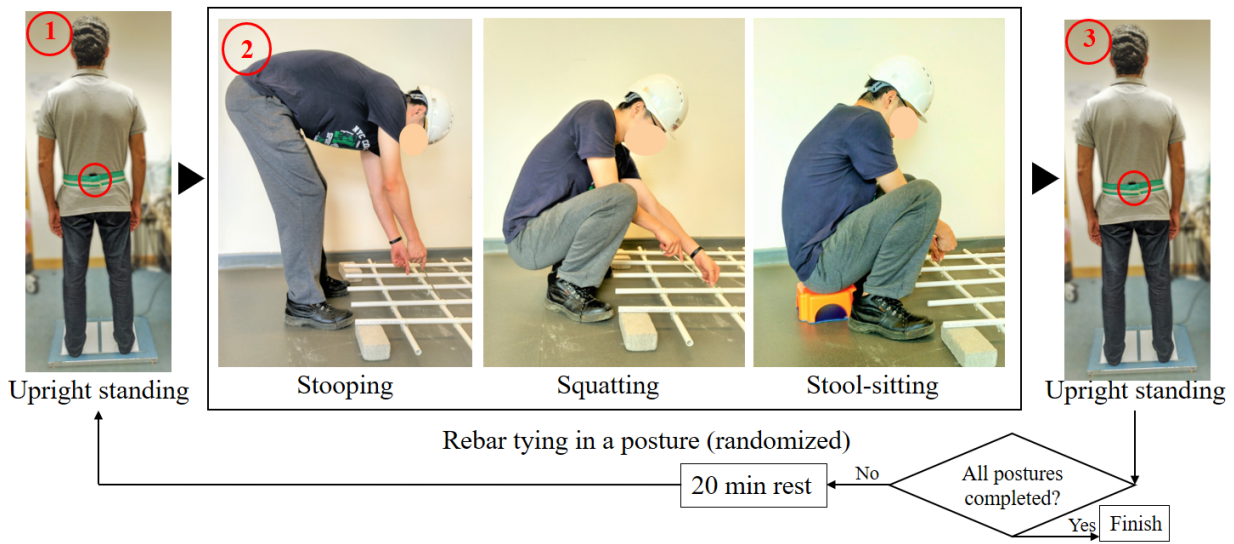
## 181 **2. Material and methods for validation of WIMUs to detect task/fatigue induced changes** 182 **in static balance**

### 183 **2.1 Participants**

184 To validate the usefulness of WIMUs in detecting task/fatigue induced changes in static balance,  
185 thirteen male volunteers (university student and staff, mean age:  $27.5 \pm 4.4$  years; mean body  
186 mass index:  $22.8 \pm 1.5$  kg/m<sup>2</sup>) were recruited for the experiment. The volunteers were eligible for  
187 the study if they had (1) normal or corrected vision, (2) no known history of balance problems,  
188 and (3) no musculoskeletal disorders/pain in the past 12 months [23]. The current study was  
189 approved by the Human Research Ethics Committee of The Hong Kong Polytechnic University  
190 (Ref: HSEARS20160712003).

### 191 **2.2 Experimental procedure**

192 The cross-sectional study involved a randomized crossover design in a single visit (Fig. 1). On  
193 arriving at the laboratory, the participant was briefed about the experimental procedures and a  
194 written consent was obtained. To start with, a WIMU was worn on the waist using a stretchable  
195 belt. Afterwards, the participant was instructed to standstill barefooted on a force-plate for a  
196 duration of 20 seconds with his feet shoulder's width apart, arms resting aside while looking at a  
197 target placed in front of him at the eye level [23,58]. Two familiarization trials were given prior  
198 to data collection. Further, the feet placement was traced on a piece of paper adhered to the force  
199 plate to guide subsequent static balance trials [59]. It was followed by a randomized simulation  
200 of rebar tying in one of the three postures of stooping, stool-sitting (15cm in height) and  
201 squatting. The three postures were chosen because rebar tying in these postures has shown to  
202 elicit divergent perceived discomfort levels (an indicator of whole-body fatigue) and post-task  
203 static postural stability [23,60]. Immediately after rebar tying, the participant was instructed to  
204 repeat the static balance trial in the same way as performed before the rebar tying task.  
205 Subsequently, a 20-minute relaxed sitting was provided which was followed by the repetition of  
206 aforementioned procedures for the rebar tying task in the remaining two postures.



208

209

**Fig. 1 Experimental Procedure**

### 2.3 Simulated rebar tying

211 Rebar tying was performed using a simulation setup made of five-by-five plastic pipes [31,60].  
 212 The pipes were 1.2m in length and were separated to each other with a center-to-center distance  
 213 of 0.2m. The participant was instructed to tie simulated rebar using tie-wires and a pigtail tool  
 214 repeatedly in the first three rows of the setup. During the experiment, the participant was not  
 215 allowed to stand or change posture in order to keep the procedure standardized for all of the  
 216 participants. The duration for rebar tying in each posture was initially planned to last for 20  
 217 minutes but the pilot testing revealed that the duration was too long to hold these postures  
 218 continuously because of the severe discomfort in the legs [23,60]. Noteworthy, the perceived  
 219 discomfort levels during stooping posture increased at a much faster rate than the other two  
 220 postures. *In contrast the duration of 12.5 minutes was well tolerated by the participants during*  
 221 *the pilot tests.* Accordingly, the rebar tying duration was limited to 12.5 minutes for squatting  
 222 and stool-sitting postures whereas for the stooping posture, it was reduced to 5 minutes. The  
 223 specific figures of 12.5 and 5 were chosen because they were multiples of 2.5, which were the  
 224 selected time interval to document perceived discomfort levels in our previous study [60].

### 2.4 Instrumentation for data acquisition and variables of interest

226 For the static balance trials, a multicomponent force-plate (0.4m by 0.6m) with four load cells  
 227 (Kistler 9286AA, Kistler Instrument Corp., Switzerland) was used to assess the postural stability  
 228 of the participants while the rate of data collection was 1,000Hz. The load cells registered ground  
 229 reaction forces once a participant stood on it. The postural stability parameters were then  
 230 calculated based on the variations in load cell readings arising from subtle body movements.  
 231 Smaller body movements indicated better static balance. The force-plate data acquisition was  
 232 synchronized with the acceleration data collection (1500Hz) from a WIMU (MyoMotion system,  
 233 Noraxon USA) worn at the level of S1 spinous process using a stretchable belt. The WIMU was

234 placed at the specified body landmark because this location closely represents an individual's  
235 center of mass [57,61].

236 The static balance of a participant using the force-plate (considered as an industry standard) was  
237 evaluated using *total path length* metric of the center of pressure (COP). COP is the vertical  
238 projection of the center of an individual's mass and usually measured using a force-plate [62]  
239 whereas total path length is one of the widely used COP metrics for static balance assessment  
240 [63]. The raw data from the force-plate was filtered through a second-order Butterworth filter  
241 with a cut-off frequency of 3Hz prior to the calculation of the COP metric [23,64]. Afterwards,  
242 total path length was calculated as follow:

$$243 \quad \text{Total path length} = \sum_{n=1}^{N-1} [(AP[n+1] - AP[n])^2 + (ML[n+1] - ML[n])^2]^{1/2} \quad (1)$$

244 In the above equation n and N refer to n<sup>th</sup> and last data set value of 20-second static trial,  
245 respectively while AP and ML refer to force-plate COP coordinates in anterior-posterior and  
246 mediolateral directions, respectively.

247 To compare with the total path length data on the force-plate, four WIMU metrics were  
248 computed to assess the 20-second static balance of the participants; namely resultant  
249 acceleration, horizontal plane velocity and displacement in the AP and ML directions. Multiple  
250 metrics were explored to ascertain which one of them would be more suitable for the balance  
251 monitoring tool. Resultant acceleration was calculated by computing root mean square of the  
252 acceleration values in the three planes of the accelerometer [57], whereas velocity and  
253 displacement related metrics were calculated by integrating the respective acceleration data in  
254 the corresponding planes [61,65]. A smoothing window of 1.3 seconds with a step size of 1.5  
255 milliseconds was applied to the raw data prior to calculation of WIMU based metrics. Regardless  
256 of the metric used (force-plate based or WIMU), a larger magnitude (sway) indicates poor static  
257 balance and vice versa [55]. The analyses revealed no significant difference among the various  
258 pre-task static tasks for any of the parameters. Accordingly, the three pre-task static balance  
259 values for each metric were averaged together for the subsequent analysis. Customized  
260 MATLAB programs (Version 2015a, MatchWorks, Inc., Natick, USA) were used for all static  
261 balance data processing.

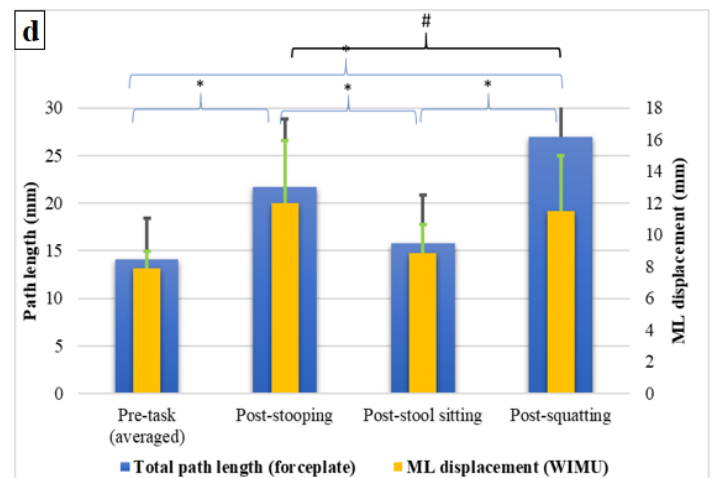
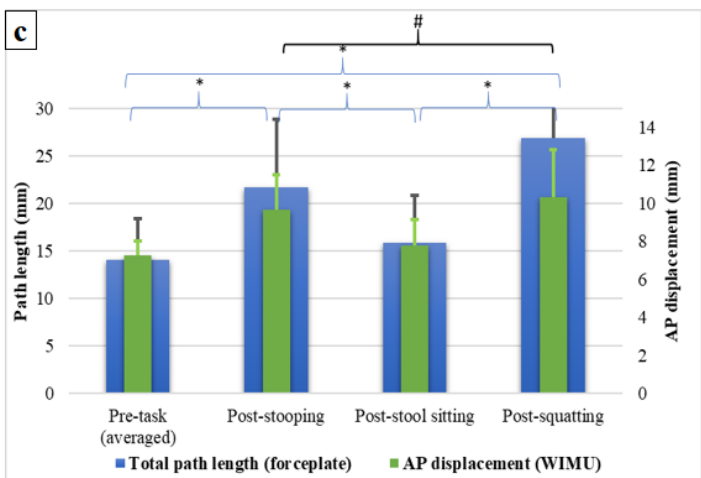
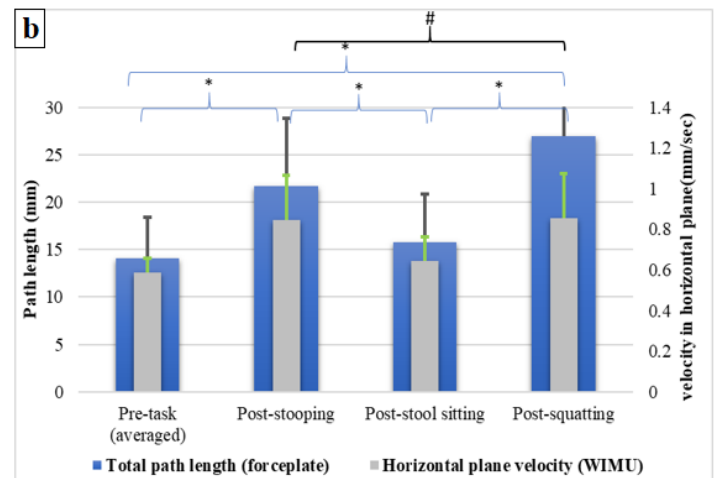
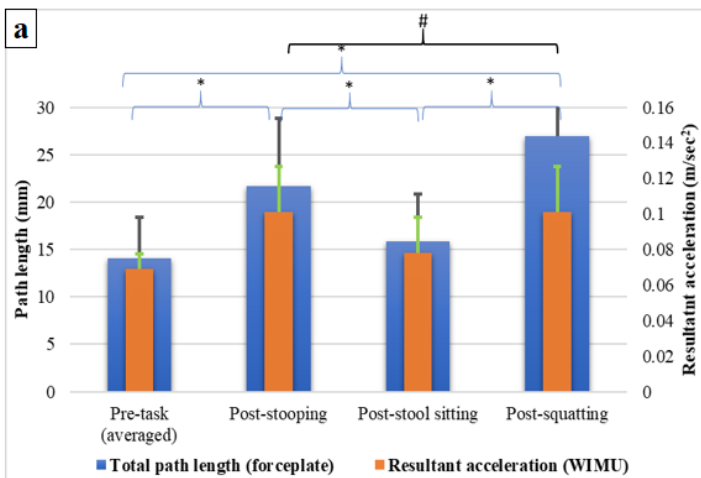
## 262 **2.5 Statistical analysis**

263 To compare the performance of WIMU against the force-plate in detecting task/fatigue induced  
264 changes in the static balance, separate one-way repeated measures ANOVA were used to  
265 compare averaged pre-task and post-task static stability values for each of the aforementioned  
266 metrics. Statistically significant results were explored using post-hoc paired t-test with false  
267 detection rate (FDR) correction [66]. To further explore the suitability of each WIMU metric for  
268 the balance tool, the ability of each metric to discriminate different balance conditions (effect  
269 sizes) was compared using partial eta-squared statistic. Additionally, Pearson's correlation  
270 coefficient was used to compare the correlation between each WIMU metric and force-plate  
271 based total path length data. The statistical significance level was set at 0.05 for all tests and  
272 SPSS (Version 19.0, IBM Corporation, USA) software was used for all statistical analyses.



273 **3. Results for using WIMUs to detect task/fatigue induced changes in static balance**

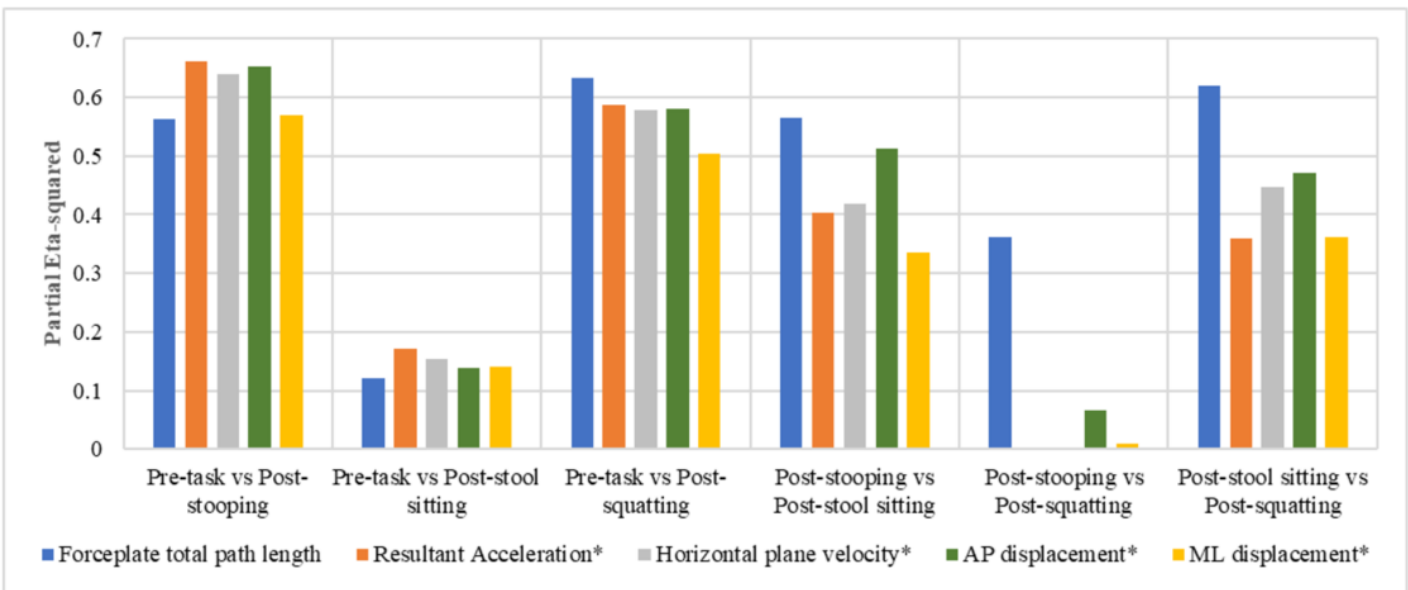
274 One-way repeated measures ANOVA revealed that all of the force-plate and WIMU based  
 275 metrics were able to detect significant differences among pre- and various post-task static  
 276 balance conditions. All of the force-plate and WIMU metrics indicated that pre-task test  
 277 demonstrated least postural instability (sway) whereas rebar tying in squatting posture resulted in  
 278 the worst stability except for WIMU based ML displacement, which indicated post-stooping  
 279 balance to be the most unstable (Fig. 2). Additionally, paired t-tests (with FDR correction) for all  
 280 of the metrics (force-plate and WIMU) indicated that using the stooping or squatting posture for  
 281 rebar tying caused a significant deficiency in postural stability as compared to the respective pre-  
 282 task static balance test results ( $p < 0.05$ ). Similarly, post-stooping and post-squatting sway was  
 283 significantly larger than post-stool sitting sway ( $p < 0.05$ ). In contrast, stool-sitting posture did not  
 284 have any significant detrimental effect on the static balance (the difference between pre-task and  
 285 post-stool sitting sway was not statistically significant,  $p > 0.05$  for all metrics). Interestingly,  
 286 while the force-plate based total path length found that the post-squatting sway was significantly  
 287 larger than the post-stooping sway, none of the WIMU based metrics could statistically  
 288 differentiate between these two conditions.



290 **Fig. 2 Pre- and post-task static balance as measured by force-plate and WIMU metrics for**  
 291 **various rebar-tying postures**

292 Note: \* indicates significant post-hoc paired t-test results for both force-plate and WIMU data (with FDR (false  
 293 detection rate) correction;  $p < 0.05$ ); # indicates significant difference in the force-plate data only ( $p < 0.05$ ); Bars  
 294 indicate standard deviation; AP= anterior-posterior direction; ML= mediolateral direction; WIMU= wearable inertial  
 295 measurement unit

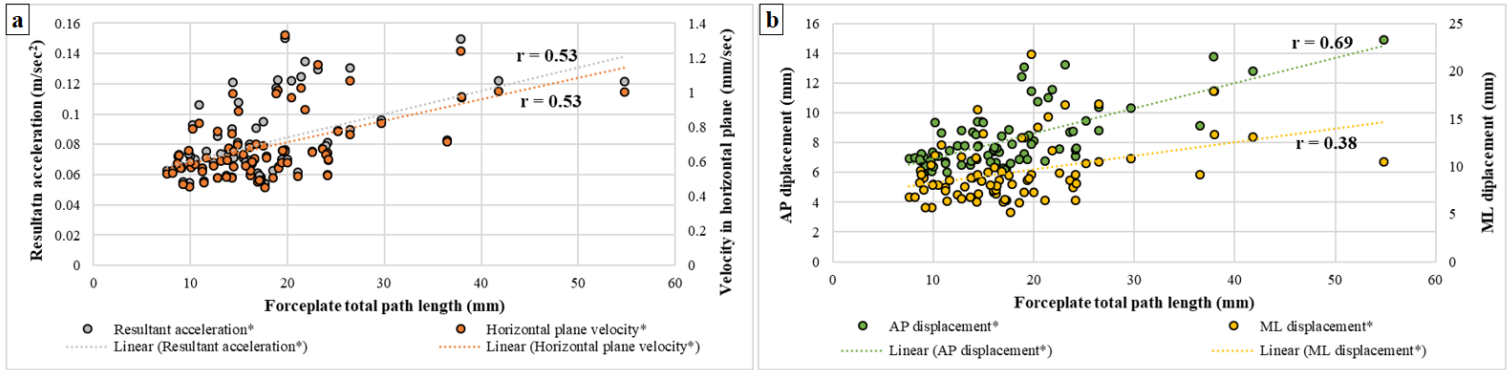
296 Fig. 3 depicts the effect size comparison among the various force-plate and WIMU metrics. The  
 297 results showed that the force-plate based total path length was the most sensitive metric to  
 298 discriminate among various stability conditions. Of all WIMU based metrics, the AP  
 299 displacement had the highest discriminating power comparable to the total path length measured  
 300 by the force-plate. Further, resultant acceleration and horizontal plane showed similar but  
 301 relatively smaller effect size, whereas ML displacement demonstrated the least capability to  
 302 discriminate various stability conditions.



304 **Fig. 3 Effect size comparisons among various force-plate and WIMU metrics in**  
 305 **discriminating various post-task static balance**

306 Note: AP= anterior-posterior direction; ML= mediolateral direction; \* indicates measured using a wearable inertial  
 307 measurement unit (WIMU)

308 Separate Pearson's correlation coefficient calculation for the force-plate based total path length  
 309 data and each of the WIMU metrics revealed significant correlation for all of the WIMU based  
 310 metrics ( $p < 0.05$ , Fig.4). Specifically, the correlation was the strongest between total path length  
 311 and AP displacement ( $r = 0.69$ ), moderate between total path length and each of resultant  
 312 acceleration and horizontal plane velocity ( $r = 0.53$  for each) and weak between total path length  
 313 and ML displacement ( $r = 0.38$ ). Taken together, our results (Fig. 2, 3 and 4) suggested that  
 314 WIMU based AP displacement was the best parameter to detect the task/fatigue induced  
 315 differences in static balance for future onsite balance assessment.



317 **Fig. 4 Pearson's correlation coefficient comparisons among various WIMU metrics against**  
 318 **force-plate data**

319 Note: AP= anterior-posterior direction; ML= mediolateral direction; r= Pearson's correlation coefficient; \* indicates  
 320 measured using a wearable inertial measurement unit (WIMU)

321 **4. Material and methods for determining the threshold for static balance conditions**

322 While an increased postural sway may indicate a higher risk of falls [32,33], there are no  
 323 established objective methods/standards/cutoff values that can categorize the balance  
 324 performance of a worker as “very good”, “good”, “poor” and “very poor”. Given the subjective  
 325 and vague boundaries in separating various balance categories, it was a big challenge to classify  
 326 people into different levels of balance performance. Unlike quantitative information with  
 327 randomness which could be explained by a probability distribution, the uncertainty in the current  
 328 scenario was more related to vagueness and ambiguity of information for which the probabilistic  
 329 approach and associated methods are not recommended [67,68]. To bridge this gap, this study  
 330 adopted the fuzzy set theory, which allows decision making (characterization in this study) by  
 331 applying mathematical operators and programming to the fuzzy information [69]. The theory has  
 332 been widely adopted in the domain of construction management for decision making in dealing  
 333 with the prevalent vagueness and fuzziness in human concept formation and reasoning [69–72].

334 For the said purpose, five experts (including three registered physiotherapists, an occupational  
 335 therapist and a biomedical engineer, each with at least five years of experience in conducting  
 336 static balance assessments in their daily job or for research projects) were contacted to provide  
 337 opinions on the cutoff thresholds for characterizing good and poor static balance. Five experts  
 338 were deemed to be sufficient because a study conducted to assess the effect of number of  
 339 assessors (5, 10, 15 and 22) found that five assessors could be sufficient to obtain a reasonable  
 340 response using fuzzy set theory [73]. Upon their consent, the study was explained and the data  
 341 collected during the abovementioned experiment was shared with them. The experts were asked  
 342 to assist in forming two sets of triangular fuzzy membership functions using the interval  
 343 estimation method [74], which could be used for classifying static balance of the workers.  
 344 Interval estimation method was chosen among other methods (e.g. point estimation, membership  
 345 function exemplification and pairwise comparison) because it better suited the requirements of  
 346 this study. Chameau and Santamarina [73] found that the interval estimation method was  
 347 simpler, easier and more capable to handle vagueness when compared to other methods.

348 The first set of fuzzy membership function characterized pre-work shift static balance of the  
 349 workers as; “very good”, ‘good”, “poor” and “very poor” based on the AP displacement data of  
 350 WIMU. Similarly, the second set of fuzzy membership function characterized the relative  
 351 increase in post-task/post-work-shift sway (percentage change in WIMU AP displacement) as  
 352 “small”, “medium”, “large” or “very large”. Specifically, triangular membership functions were  
 353 chosen for this work because they are easier to understand, use and process in a fuzzy  
 354 environment [75,76]. A triangular fuzzy membership function was represented using three real  
 355 numbers such that  $\tilde{A} = (L,M,U)$  where L,M, U are lower limit, modal (the strongest grade of  
 356 membership) and upper limit values, respectively for a particular membership function [72].  
 357 These limits are an expansion of the idea of confidence interval with varying degree of  
 358 membership for a given WIMU-based AP displacement value. For a given x (AP displacement),  
 359 there is a corresponding real number  $\mu_{\tilde{A}}(x) \in [0,1]$ , where  $\mu_{\tilde{A}}(x)$  is the degree of membership of  
 360 x for  $\tilde{A}$ , 1 refers to the full membership while 0 refers to the null membership. For the  
 361 intermediate values,  $\mu_{\tilde{A}}(x)$  is determined as follow:

$$362 \quad \mu_{\tilde{A}}(x) = \begin{cases} (x - L)/(M - L), & L \leq x \leq M \\ (U - x)/(U - M), & M \leq x \leq U \end{cases} \quad (2)$$

363 Accordingly, each of the contacted experts was asked to provide three defining values for each  
 364 stability condition of the two fuzzy membership functions. Additionally, no specific overlapping  
 365 limit was imposed on the experts for the membership functions in order to capture the most  
 366 suitable values for each stability condition as per their experience and knowledge.

### 367 5. Results for the determination of thresholds for static balance conditions

368 The fuzzy membership functions related response gathered from the experts was averaged for the  
 369 final membership functions which could readily be used for the balance monitoring tool. Table 1  
 370 and 2 depict the subjective opinion of each of the experts for the two fuzzy membership  
 371 functions. Based on their response, the final fuzzy membership functions are illustrated in Fig. 5.

372 **Table 1**

373 Suggested values by the experts for pre-task/unfatigued characterization of static balance

Expert	Pre-task/unfatigued static balance AP displacement values (mm)			
	Very good	good	poor	Very poor
1	(0,0,7)	(4,7,10.3)	(8,11,15.5)	(14,17,40)
2	(0,6.5,8)	(7,18,29)	(28,35,41)	(40,42,50)
3	(0,1,6)	(6.5,16,21.5)	(15,26,29.5)	(28,35,49)
4	(0,3,8)	(7,13,19.5)	(16,20.5,25.5)	(23,30,51)
5	(0,5,10)	(7,17,20)	(18,25,42.5)	(32.5,42,55)
<b>Final membership functions</b>	(0,3.1,7.8)	(6.3,14.2,20.1)	(17,23.5,30.8)	(27.5,33.2,49)

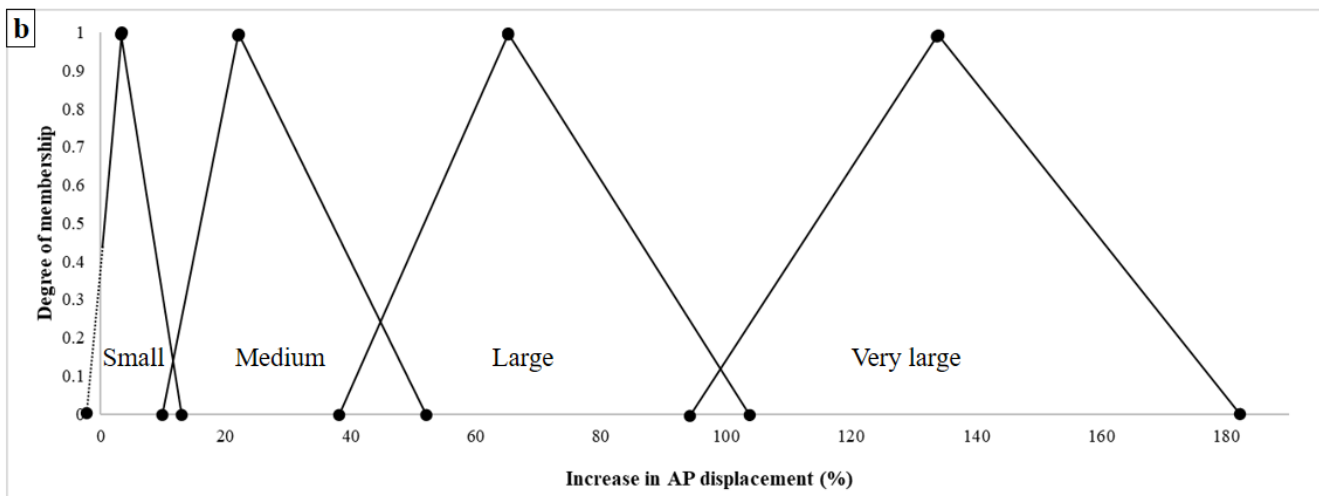
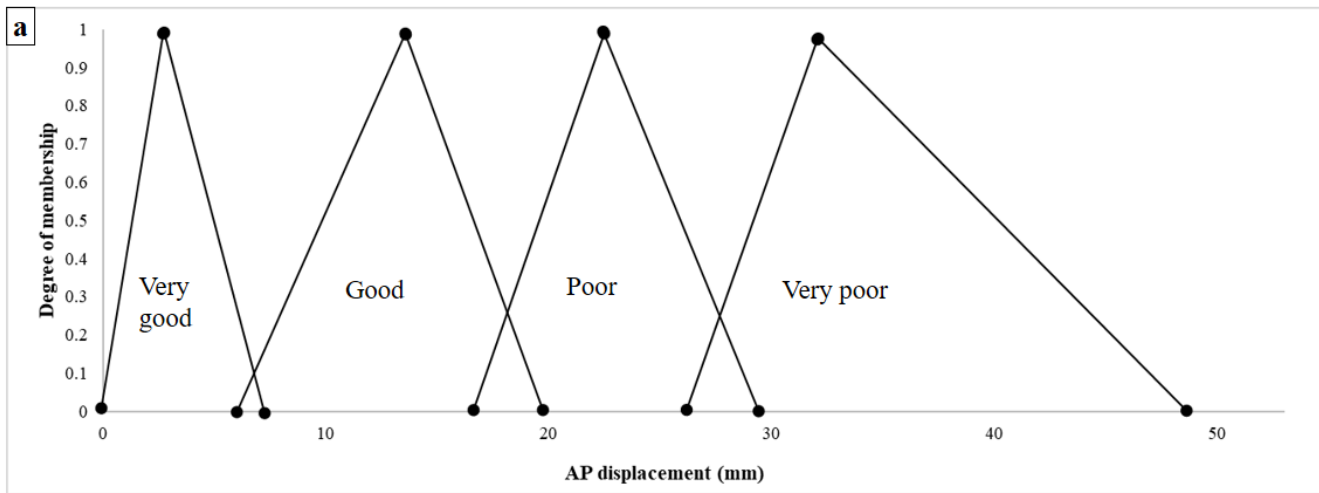
374 Note: AP refers to anterior-posterior direction; each triplet represents the lower bound, strongest  
 375 grade of membership and upper bound AP displacement values for each stability condition

376 **Table 2**  
 377 Suggested values by the experts for post-task/post-work-shift characterization of static balance

Expert	Post-task/post-work-shift increase in sway (%)			
	Small	Medium	Large	Very large
1	(0,5,10)	(7,14.5,20)	(18,45,70)	(60,100,150)
2	(0,5,10)	(9,20,55)	(50,70,110)	(100,120,200)
3	(-10,0,15)	(10,35,55)	(30,60,90)	(85,150,200)
4	(0,1,15)	(10,20,55)	(50,70,100)	(90,108,115)
5	(-5,5,20)	(10,25,60)	(45,80,150)	(100,190,250)
<b>Final membership functions</b>	(-3,3.2,14)	(9.2,22.9,49)	(38.6,65,104)	(87,133.6,183)

378 Note: AP refers to anterior-posterior direction; each triplet represents the lower bound, strongest  
 379 grade of membership and upper bound AP displacement values for each stability condition

380



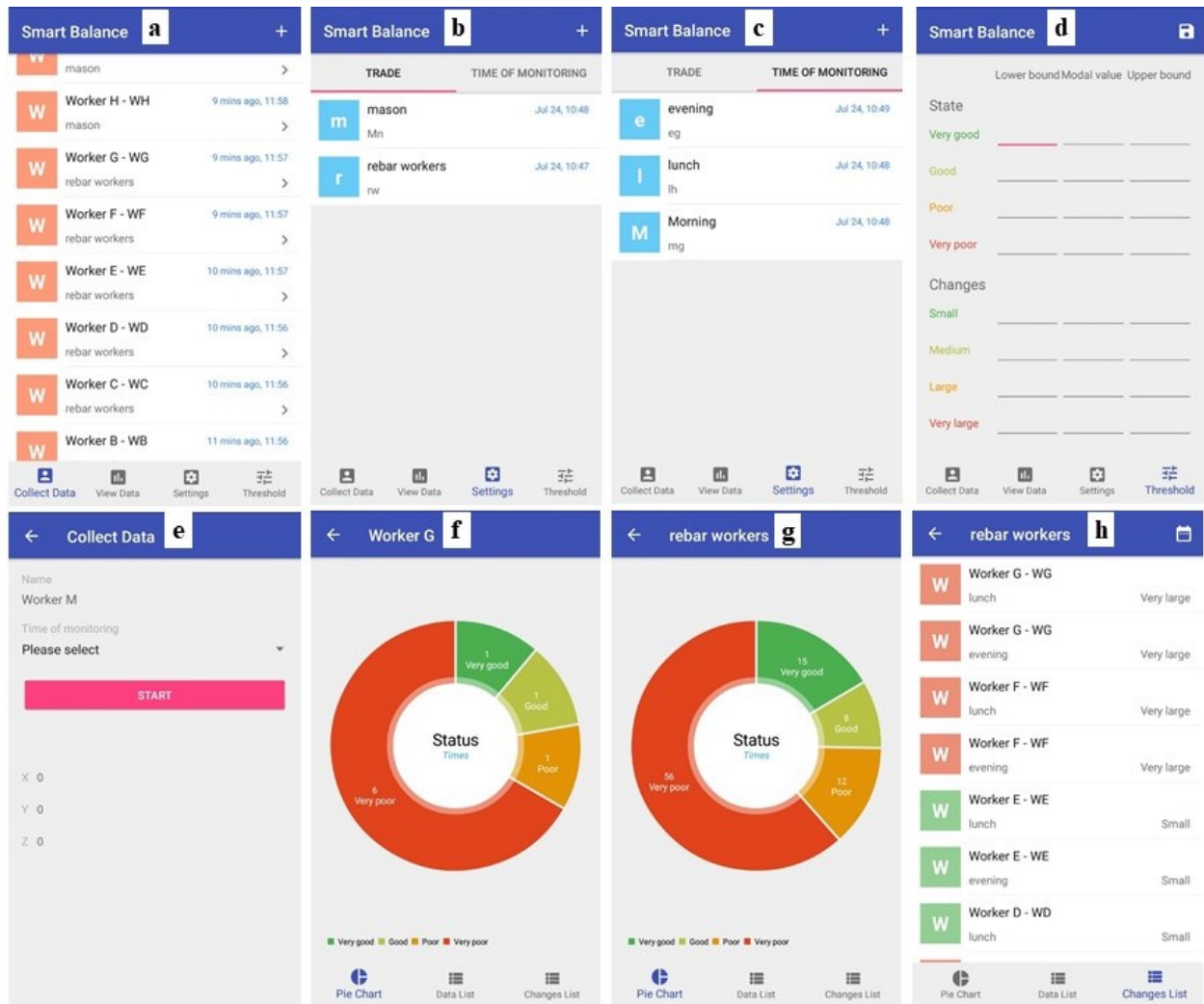
381

382 **Fig. 5 Fuzzy membership functions developed for the WIMU based balance monitoring**  
383 **tool**

384 Note: AP refers to anterior-posterior direction; WIMU= wearable inertial measurement unit

385 **6. Mobile application developed for the balance monitoring tool**

386 Based on the fuzzy membership functions, a mobile application (Android) was developed to link  
387 a WIMU to a smartphone using Bluetooth and onsite deployment of the WIMU based balance  
388 monitoring tool. The interface of the mobile application is shown in Fig. 6. Fig 6 (a) indicates a  
389 list of construction workers registered in the application (the data used in the illustrations is  
390 fictitious). The time mentioned in front of each worker refers to the point in time of his  
391 registration in the application. Fig. 6(b) illustrates the two construction trades (mason and rebar  
392 tying) as an example to which the registered workers belonged to whereas Fig. 6(c) refers to the  
393 suggested times of the day for balance monitoring. Both the trades and the time of monitoring  
394 could be edited or added as per onsite requirements using the application interface. The  
395 established thresholds for the stability conditions obtained using the fuzzy set theory could be  
396 plugged-in/edited using an interface as shown in Fig. 6(d). The interface for taking new static  
397 balance reading is shown in Fig. 6(e). Prior to data collection, it is necessary to specify the  
398 worker and the time of monitoring. Additionally, Fig. 6(f) and Fig. 6(g) show two pie charts  
399 depicting the stability records of an individual worker and workers from a specific trade,  
400 respectively. Fig. 6(h) shows the recorded changes in static stability of various workers of a  
401 specific trade after a particular work task/ post-work-shift. Once the stability related data is  
402 collected using the developed tool, it could be used in a number of ways for proactive fall  
403 prevention as explained in the next section (i.e. Discussion).



404  
405 **Fig. 6 Mobile application developed for the balance monitoring tool**

406 Note: All shown data is fictitious

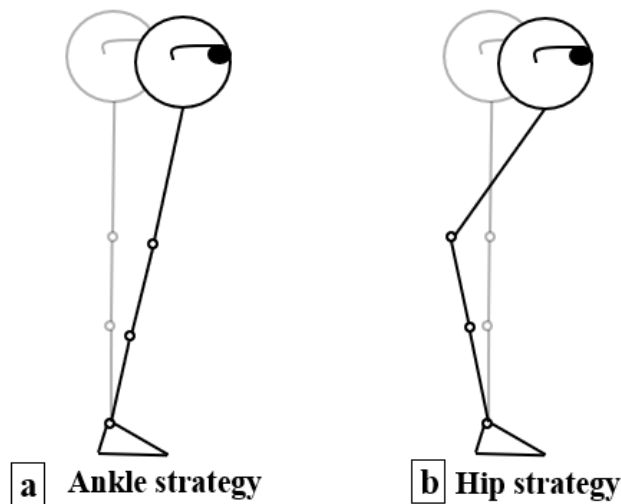
407 **7. Discussion**

408 This study, for the first time, developed a proactive WIMU based static balance assessment tool  
 409 tailored for construction site workers. The tool utilized a small and lightweight WIMU along  
 410 with a mobile application, which is expected to enhance its acceptance for onsite fall prevention  
 411 by the construction industry [57]. This will allow foremen/site managers to monitor the static  
 412 balance of the construction workers using the 20-second static balance tests at different times of  
 413 the day in order to keep a balance profile of the workers longitudinally. Ultimately, the tool  
 414 would enable them to identify the workers with consistent balance deficits that require relevant  
 415 balance trainings.

416 **7.1 Use of WIMUs to detect changes in static balance**

417 The results of this study indicate that the WIMU based metrics are sensitive to differentiate  
 418 distinct changes in balance conditions induced by rebar tying task in different work postures.  
 419 Specifically, WIMU-based AP displacement was highly correlated to the total path length as

420 measured by a force-plate in detecting task/fatigue induced changes in static balance (Fig. 2(c),  
421 Fig. 3 and Fig. 4). It is noteworthy that although WIMU-based AP displacement indicated a  
422 greater post-squatting static sway than post-stooping sway, the AP displacement metric could not  
423 differentiate between the two balance conditions, which could be distinguished by the force-  
424 plate-based total path length (Fig. 2(c) and 3). This finding might be attributed to the fact that  
425 tasks inducing severe static instability (such as rebar tying in squatting and stooping postures in  
426 this experiment) may also require hip strategy to regain the balance in addition to ankle strategy  
427 (Fig. 7) [61]. Under such circumstances, there could be movements at the hip (sacrum) level  
428 without corresponding changes in COP parameters [61], that results in a reduction of association  
429 between the force-plate and WIMU parameters which might explain the aforementioned  
430 disparity.



431  
432 **Fig. 7 Strategies for regaining balance**

## 433 7.2 Implications

434 Generally, most of the construction trades are physically demanding (e.g., prolonged and  
435 repetitive awkward postures, manual material handling, and operating heavy tools) [77–79]. As  
436 such, the daily tasks of different trades may predispose the workers to peripheral or whole-body  
437 fatigue. It is known that fatigue of individual body parts (such as ankle [80], lower back [33],  
438 shoulder [81], neck [82]) or whole-body [83,84] could lead to loss of balance. Therefore, the  
439 developed tool will provide an opportunity to quantify the postural instability induced by any of  
440 these construction tasks, such as bricklaying, floor laying, carpentry or concrete laying.

441 Given that loss of balance is one of the major causes of fall incidents on the construction sites  
442 [21,38,47], the use of our tool may enable proactive balance monitoring for high fall risk  
443 workers/activities. For instance, previous studies have indicated that fall accidents happen more  
444 often in the afternoon [5,12], which could be attributed to highly demanding construction tasks  
445 leading to fatigue and associated poor balance control [23,33,47]. As such, there is an increased  
446 need for monitoring of the workers in that time [5]. Similarly, ageing workforce has been a  
447 serious challenge for the construction industry in a number of countries. Since, ageing is linked



448 with a decline in work capacity, cognitive and proprioceptive skills and muscle strength [85,86],  
449 aged workers more commonly suffer from fall accidents than their younger counterparts [87].  
450 The developed tool in this study provides an innovative and pragmatic way to increase the fall  
451 risk surveillance in these situations.

452 Combined with the developed tool, Prevention through Design (PtD) [28,88] could be a more  
453 effective avenue to lower the risk of falls in the construction industry. For instance, by  
454 employing the tool, various task and environment related fall risks (e.g. height, equipment and  
455 gear, work-technique, visual stimuli) could be analyzed and their effect on the balance of the  
456 workers could be better understood. Subsequently, appropriate risk alleviation strategies could be  
457 adopted. Similarly, while three-quarters of all fall accidents involve specialty trades workers  
458 [27,89], PtD approach could be used to target the individual trade workers with a higher fall risk  
459 (such as roofers and structural steel erectors). In different trades, the balance monitoring tool  
460 could be effectively used to redesign work-rest cycles to minimize fatigue and associated fall risk  
461 [57].

462 While many workers may have poor balance, those with poor postural controls can undergo  
463 balance training programs to enhance their static and dynamic balance skills [90]. These training  
464 programs may include muscle strengthening, agility and plyometric exercises, single and double  
465 leg stance on unstable surfaces such as wobble boards and biofeedback based balance  
466 improvement schemes systems [90–92]. During or by the end of the balance training program,  
467 our tool can be used to quantify improvements attained by the workers. Moreover, the tool can  
468 be used to assess the efficacy of any newly designed balance training program.

469 Although the use of our developed balance monitoring tool could be beneficial, the importance  
470 of other fall safety measures cannot be overlooked. Other mitigation measures (such as the use of  
471 fall protections, enforcement of safety provisions and compliance to protection plans [28],  
472 educational trainings, workshops and seminars) are regarded as useful in preventing falls,  
473 enhancing fall hazard awareness and imparting safe behaviors among the construction workers  
474 [11,93]. Importantly, using a holistic systems approach is highly recommended to reduce the risk  
475 of fall and other accidents on construction sites [94].

## 476 **8. Limitations and future works**

477 Despite numerous advantages, the current study has a few limitations. First, it is important to  
478 evaluate both the static and dynamic balance of workers in order to assess the fall risk [23].  
479 Accordingly, future studies should develop pragmatic dynamic balance assessment tools for  
480 construction workers. Second, the current study validated the use of WIMUs to detect  
481 task/fatigue induced changes in static balance using inexperienced workers in a laboratory setting  
482 and entailing a single work task (i.e. rebar tying). Future studies should validate the usefulness of  
483 WIMUs using experienced construction workers, on actual worksites and incorporating various  
484 construction trade tasks. **Third, this study explored a single duration of work task for inducing**  
485 **changes in static balance. Future studies should evaluate the relation between fatigue**  
486 **development in the three postures and the corresponding induced static imbalance as a function**  
487 **of rebar tying duration. Additionally, it will be worthwhile to explore the effect of prolonged**  
488 **rebar tying in various postures against intermittent rebar tying in identical postures (with**

489 frequent work-breaks) on fatigue development and induced static imbalance. Finally, the current  
490 study established the thresholds for balance classification based on the laboratory data from a  
491 relatively small sample size and the opinions from a few experts using a questionnaire.  
492 Accordingly, future studies should gather the data from a large number of construction workers,  
493 and should involve a methodology (e.g., a Delphi method) that can obtain consensus from  
494 experts for establishing more reliable thresholds.

## 495 **9. Conclusions**

496 The current study adopted a three-step approach to develop a tool for onsite balance monitoring  
497 of the construction workers. First, a validation study was conducted to investigate the suitability  
498 of the WIMUs to detect task/fatigue induced faint changes in the static balance by validating  
499 various WIMU metrics against the metric from a force-plate. The study found that WIMU based  
500 AP displacement metric was an adequate alternative for the force-plate based static balance  
501 assessment. Second, five experts were contacted to help determine AP displacement based  
502 thresholds for categorizing static balance performance of individuals. Last, a mobile application  
503 was developed to link data collected by WIMU during 20-second balance trials to the mobile  
504 phone application. The developed tool will have a great potential to enhance proactive  
505 identification of the workers with a higher risk of falls so that proper balance training can be  
506 provided. It can also be used to assess the effect of various tasks and environmental risk factors  
507 on the ensuing balance. Collectively, the tool can contribute to informed decision making to  
508 alleviate the risk of falls in the construction industry.

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