

A New Fast Door-opening Method for Quick Release of a Rock Boulder or Debris in a Large-scale Physical Model

by

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1 **Abstract**

2 Study on mitigation of debris flows and rockfalls is a very challenging topic due to the complex
3 moving and impacting mechanisms. Large-scale physical model is preferred by researchers in
4 the study of debris flow and rockfall because large-scale tests can duplicate major phenomena
5 of natural geo-hazard events. In the design of a large-scale physical model, how to initiate or
6 release a certain volume of debris material or a giant rock boulder is the key technical issue. In
7 current large-scale models for debris flow research, debris material is normally released from
8 a reservoir with a trap door located at the upper end of the flowing path. It is found that the
9 door-opening methods utilized in the models can interfere with the motions of the generated
10 debris flows. In this note, a new fast door-opening method is introduced in detail. This method
11 has been implemented in a large-scale physical model built in Hong Kong to study the impacts
12 of rockfalls and debris flows on a flexible barrier. With the utilization of this novel door-
13 opening method, the impact tests of rock boulders, dry granular flows, and debris flows were
14 successfully performed. From the observations of the impact tests, the unbalanced resisting
15 forces and the disturbance from the door were avoided. The successes of the large-scale tests
16 using different testing materials demonstrated that the new fast door-opening method can be
17 further utilized in physical modelling study of geohazards.

18 **Keywords:** Debris flow; Rockfall; Large-scale physical modelling; Door-opening method

19

20 **Introduction**

21 Many countries and regions (e.g. Japan, China, and Canada) are constantly threatened by
22 natural hazards in the hilly terrain (Su *et al.* 2017; Takahashi 2014; Fan *et al.* 2017; Xu et al.
23 2019; Zhu and Randolph 2009). High degree of urbanization and a shortage of land resources
24 in regions such as Hong Kong have necessitated the construction of infrastructures and
25 residential buildings in the vicinity of natural hillsides with great risks of natural hazards (Kang
26 and Chan 2017). European Organization for Technical Approvals (EOTA) introduced a
27 comprehensive guideline for the design of rockfall net fences (Peila and Ronco 2009).
28 Geotechnical Engineering Office (GEO) of Hong Kong Government published the first guide
29 reference for the design of debris flow-resisting flexible barrier (Kwan and Cheung 2012).
30 Volkwein et al. (2015) discussed the design standard of flexible barriers in preventing debris
31 flows. However, the impact mechanisms of rockfalls, debris flows on a flexible barrier are still
32 poorly understood. To fulfill this research gap, physical model tests have been advocated by
33 researchers in the study of geotechnical engineering due to the good controllability in testing
34 conditions and repeatability of tests (Volkwein *et al.* 2015; Iverson 2015; Xu et al. 2018).

35 In physical model tests to study the behavior of debris flows, scaling is a key factor because
36 the influences of viscous shear resistance and excess pore-fluid pressure on the interaction of
37 water with debris sediment have a close relationship with the scale of tests. Iverson (2015)
38 concluded that miniaturized landslides exaggerate the effects of viscous shear resistance and
39 weaken the effects of excess pore-fluid pressure. On the other hand, for the research of flexible
40 barriers, which is a complicated structure with several major components, miniaturized
41 prototypes cannot realistically reflect the dynamic performance under the impacts of different
42 geohazards, especially the influence of earth gravity or the stress level (Wendeler et al. 2018).
43 Therefore, large-scale physical modelling is preferred by researchers to study the behavior of
44 debris flows and their interaction with protection structures. The U.S. Geological Survey

45 (USGS) in cooperation with the U.S. Forest Service built a large-scale flume in 1991 to study
46 landslide initiation and debris flow deposition behaviors (Iverson *et al.* 1992). Paik *et al.* (2012)
47 built a real-scale field experiment facility in a natural gully in Korea with the main objectives
48 of investigating the erosional and depositional patterns of debris flows. The Swiss Federal
49 Institute for Forest Snow and Landscape Research (WSL) constructed a large-scale facility in
50 Veltheim, Switzerland to study the impact of debris flows (Bugnion *et al.* 2012).

51 **Brief Description of the Large-scale Physical Model in Hong Kong**

52 Based on the previous works and conditions in Hong Kong, a large-scale physical modeling
53 facility has been designed and built in the Road Research Lab of The Hong Kong Polytechnic
54 University for studying the interaction of rockfalls or debris flows with a flexible barrier. This
55 large-scale facility is built in a reinforced steel frame, as shown in Fig.1(a). This facility can be
56 divided into 4 main components: (i) a reservoir with the capacity of 5 m³ locating 5 m above
57 the bottom cable of the flexible barrier; (ii) a flip-up door and corresponding fast door-opening
58 system; (iii) a flexible barrier with supporting posts and cables; and (iv) a flume connecting the
59 reservoir to the flexible barrier. This flume has a channel width of 1.5 m, a length of 7 m, and
60 an inclination of 35 °. Side walls of the flume are made up of tempered glass to provide a clear
61 observation of the generated rockfalls and debris flows.

62 ***Instrumentation***

63 To monitor the dynamic response of a flexible barrier under the impact of natural hazards, this
64 facility is instrumented by a high-frequency monitoring system (see Fig.1(a)). The monitoring
65 system consists of tension link transducers, a dynamic datalogger, and two high-speed cameras.
66 Two types of transducers are installed on the flexible protection system: mini-tension link
67 transducers and high capacity tension link transducers. The mini-tension link transducers are
68 utilized to link two adjacent rings in the central area of the flexible barrier to measure the impact
69 force on the flexible barrier directly, as shown in Fig.1(a). Besides, four commercial high

70 capacity tension link transducers (Type: CFBLBH) with a certified capacity of 50 kN are
71 installed on the supporting cables of the posts. A dynamic data-logger with the capability of
72 sampling 48 transducers at 1000 Hz simultaneously is used to collect the data of all transducers.
73 Two high-speed cameras capable of capturing a resolution of 1024 ×768 pixels at a sampling
74 rate of 1000 frames per second are used to capture the motions of the impacting mass and the
75 dynamic response of the flexible barrier. One high-speed camera is installed at the right side
76 of the barrier, and the other camera is set in front of the barrier.

77 **A New Fast Door-opening Method for Quick Release of a Rock Boulder or Debris Flow**

78 *Limitations of door-opening methods in current large-scale physical models*

79 In the design of a large-scale physical model for debris flow study, the release method of
80 debris material is of concern, because a poorly designed release method could seriously
81 interfere with the motion and the impact characteristics of the debris flow. Table 1 lists the
82 basic parameters and the door-opening methods of representative large-scale physical models
83 in the literature. To better understand the possible influences of the existing door-opening
84 methods on the generated debris flows, the large-scale physical facility built by USGS in 1991
85 is reviewed in this note. From the description of testing procedures and the videos of the
86 experiments (Iverson 2015), it is observed that a pair of steel head-gates were side opened by
87 the self-weight of the debris deposit when the lock was released. The steel head-gates used in
88 that testing facility could affect the generated debris flow in three aspects: firstly, the kinetic
89 energy of the debris flow can be obviously dissipated when pushing the heavy steel head-gates
90 open; secondly, the unbalanced frictions of the side-open doors may cause deviation of the
91 flow direction or asymmetrical flow velocities and depths of the generated debris front; thirdly,
92 the side-open doors are left in the flume as obstacles after being opened, which impedes the
93 motion of the debris flow continuously.

94 To solve those problems, the following aspects should be considered for development of the
95 door-opening method: (i) the lock of the door should be easy to operate and sturdy enough to
96 sustain the earth pressure from the stored debris material; (ii) the door should be opened faster
97 than the moving of the testing material to prevent disturbance of the generated rockfall or debris
98 flow; (iii) the door should be out of the flowing path of the generated debris flow after being
99 opened to avoid continuous obstruction to the debris flow.

100 ***Development of a new fast door-opening method and the release system***

101 Based on the above review, a developed fast door-opening method is proposed in this study
102 to fulfill the requirements:

103 (a) A flip-up door is utilized, which can be out of the moving path after being pulled up to
104 avoid the continuous obstruction to the released boulder or debris flow.

105 (b) A spring set is connected to the flip-up door to lift the door up in a short period and keep
106 the door open.

107 (c) Rotatable levers are utilized to lock the door and impose excessive compressive force on
108 the door to provide water tightness by rotating toward the door.

109 Following the above door-opening method, a new release system has been designed and
110 implemented in the large-scale facility. Beside a steel reinforced flip-up door, the new release
111 system contains 3 main components: a set of springs, a pair of rotatable steel levers, and a pair
112 of quick release hooks (see Fig. 1(b)). Detailed descriptions of the functions and characteristics
113 of those components are presented as follows:

114 *The springs:* in our design, 4 springs are attached to the back surface of the flip-up door. The
115 functions of the springs are lifting the door up in a short time period and keeping the door open
116 during the test. The springs are pre-stretched by the wire twisters before each test to store the
117 potential energy and bounce the door up. Energy dissipation blocks are installed on the frame to

118 dissipate the potential energy of the springs to prevent the swing of the door after being bounced
119 up in a short period and keep the door open in a designed opening angle. In our facility, the
120 designed door-opening angle is 55° to keep the door parallel to the flume. Based on the video
121 recordings, the flip-up door can be opened in less than 0.5 s with the assistance of the spring
122 set.

123 *The steel levers:* the levers are curved steel bars with the fulcrums installed on an I-beam
124 underneath the flip-up door and the flume basal plate (see Fig. 1(b)). The levers are used to
125 lock the door before the test and release the door to start the test. The levers can transform from
126 the lock status by rotating up to the unlock status by rotating beneath the flume in a short period
127 (less than 0.5 s) to be out of the flowing path after releasing the door with the help of dead
128 weight. Rectangular openings (300 mm * 100 mm) on the flume base plate provide rotation
129 paths to the levers. To prevent leakage of debris material during the test, fiber-reinforced
130 flexible rubber mats with the dimension of 5-mm-thick, 300-mm-width, and 500-mm-length
131 are used to cover those openings. The flexible rubber mat can flip with the rotation of the lever
132 and cover the opening when the lever rotates beneath the basal plate. The upper end of the
133 rubber mat is fixed on the flume basal plate by compression of a steel bar (300 mm * 10 mm)
134 with screws. Due to the small thickness of the rubber mat to reduce obstruction of the moving
135 particles, the rubber mats should be replaced after every three tests to prevent being ripped.
136 The levers should have a high strength to resist the earth pressure from debris material in the
137 reservoir and a high stiffness to reduce the deformation under the earth pressure. The large
138 deformation can form a gap between the flip-up door and the reservoir, which can lead to a
139 leakage of the debris material. In our study, the dimensions and the parameters of the lever
140 have been calibrated by numerical simulation using the software ABAQUS. The designed
141 loading for the numerical simulation is the maximum earth pressure from the debris material
142 with a Factor of Safety (FoS) of 2.0. By performing numerical simulations with the designed

143 loading, the stiffness and the strength of the lever are determined following the principle that
144 no plastic deformation occurs in any part of the lever, and the deformation is small (less than
145 5 mm) to prevent leakage of slurry. Referring to the simulation result, the hardening technique
146 has been utilized on the steel levers to improve the mechanical performance.

147 *The quick release hooks:* two quick release hooks are used to lock the flip-up door, which
148 are provided by the RELEASE company with the model name TGQ-5T-LS. The specially
149 designed hook can be released by a small pulling force (around 50 N) under the maximum
150 working load of 50 kN. To make sure that the hooks can be released at the same time, the
151 triggers of both hooks are connected to one rope, and the test is started by arranging an
152 authorized person to pull the rope and release the hooks simultaneously. With the application
153 of the hooks, the door can be locked easily in the preparation stage and opened fast in the test.
154 As shown in Fig. 1(b), the lock of the door is realized by utilizing the hooks to stretch the steel
155 chains connecting the levers with the frame foundation and restrict the rotation of the levers.
156 Once the hooks are released at the beginning of the test, the levers can rotate beneath the flume
157 basal plate and open the door to start a test.

158 ***Operating procedures of the release system using the fast door-opening method***

159 The operation procedures of the release mechanism are presented in Fig. 1(b). The
160 procedures can be specified into 4 steps:

161 (a) Lock the door by using the quick release hooks to stretch the chains and restrict the rotation
162 of the levers.

163 (b) Lift the testing boulder or debris material into the reservoir, and pre-stretch the springs by
164 the wire twisters connected to the upper ends of the springs.

165 (c) The test is started by releasing the quick release hooks. Afterwards, the levers rotate beneath
166 the flume with the assistance of dead weight connected to their tails. Meanwhile, the door
167 is lifted in less than 0.5 second and kept open by the pre-stretched springs.

168 (d) After the test, the door can be closed again by releasing the springs.

169 With these simple procedures, a series of large-scale physical modelling tests with different
170 testing materials have been successfully conducted using the large-scale testing facility with
171 implementation of this new fast door-opening method.

172 **Performance and Evaluation of the New Fast Door-opening System**

173 A comparison of the door-opening systems in representative large-scale debris flow physical
174 models in the literature (Bugnion *et al.* 2012; Iverson *et al.* 2010; Paik *et al.* 2012) and the new
175 door-opening system in the present model in PolyU, Hong Kong is made in Table 1. Based on
176 the comparison, the door-opening method in PolyU model has the best performance among all
177 listed large-scale physical models. Moreover, the impact tests of rockfalls, dry granular flows,
178 and debris flows have been successfully performed in this large-scale physical model to assess
179 this new door-opening system and study the interaction between different impacting masses
180 and a flexible barrier.

181 Fig. 2 plots the performance of the door-opening system in a rockfall impact test. In the test,
182 the flip-up door was firstly locked by the levers, and the boulder was located behind the center
183 of the door to make sure the boulder can hit the central area of the flexible barrier. At the
184 beginning of the test, the flip-up door was pulled up in a short time and kept open by the pre-
185 stretched spring set. After that, the boulder rolled down along the central axis of the flume and
186 hit the central area of the flexible barrier. From the photographs plotted in Fig. 2, it can be
187 observed that the motion of the boulder was not impeded by the release door due to the
188 utilization of the fast door-opening system. The results and findings of the rockfall impact tests
189 were analyzed and presented in Tan *et al.* (2018b).

190 The performance of the door-opening system in a granular flow impact test is shown in Fig.
191 3. In this test, around 4 m³ aggregate was filled in the reservoir in the preparation stage, which
192 imposed a large earth pressure on the flip-up door and the lever locks. At the beginning of the
193 test, the door flipped up fast with the assistance of the spring set, the levers rotated beneath the
194 flume base, and the rubber mats covered the openings at the flume basal plate to prevent
195 leakage of the granular material. It can be observed from Fig. 3 that the door was opened much
196 faster than the initiation of the granular flow. Neither the levers nor the flip-up door interfered
197 with the granular flow during the test. The results and findings of the granular flow impact tests
198 were analyzed and presented in Tan et al. (2018a).

199 The debris flow material consists of a mixture of aggregate and completely deposited granite
200 (CDG) slurry with a high water content (higher than 45% in mass). Therefore, leakage of slurry
201 should be taken into serious consideration. The leakage of slurry and water can obviously
202 reduce the fluidity and weaken the homogeneity of the generated debris flow. To prevent the
203 leakage problem, highly compressible rubber cushions and silicone glue were sandwiched in
204 the gap between the door and the reservoir to provide water-tightness. Besides, basket screws
205 were attached to the ends of the chains to provide excessive compressive stress on the door to
206 enhance the sealing ability. It can be observed from Fig. 4(a) that no leakage of slurry occurred
207 before the test, and the generated debris front was uniform and undisturbed. The peak loads
208 measured by the mini-tension link transducers in the debris flow impact test is shown in
209 Fig.4(b), which indicates that the debris flow imposes a horizontally symmetrical impact
210 pressure on the flexible barrier.

211 Therefore, it can be concluded from the tests that this new fast door-opening system
212 implemented in the large-scale physical model has a reliable performance and can avoid
213 interference from the door.

214 **Conclusions**

215 A new fast door-opening method is proposed and introduced in detail in this note. This new
216 method has been implemented in a large-scale physical modelling facility to study the impact
217 mechanisms of different natural hazards. A series of tests including single boulder, dry granular
218 flow and debris flow impact tests were performed using this facility. From the observations of
219 those tests, it was found that the interference of the release door with the testing material has
220 been avoided by utilizing this new system. The reliable performance of the new door-opening
221 method proves that it can be utilized in the experimental study of natural hazards.

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