

# Tunable absorption characteristics in multilayered structures with graphene for biosensing

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Graphene derivatives, possessing strong Raman scattering and near-infrared absorption intrinsically, have boosted many exciting biosensing applications. The tunability of the absorption characteristics, however, remains largely unexplored to date. Here, we proposed a multilayer configuration constructed by a graphene monolayer sandwiched between a buffer layer and onedimensional photonic crystal (1DPC) to achieve tunable graphene absorption under total internal reflection (TIR). It is interesting that the unique optical properties of the buffer-graphene-1DPC multilayer structure, the electromagnetically induced transparency (EIT)-like and Fanolike absorptions, can be achieved with pre-determined resonance wavelengths, and furtherly be tuned by adjusting either the structure parameters or the incident angle of light. Theoretical analyses demonstrate that such EIT- and Fano-like absorptions are due to the interference of light in the multilayer structure and the complete transmission produced by the evanescent wave resonance in the configuration. The enhanced absorptions and the huge electrical field enhancement effect exhibit potentials for broad applications, such as photoacoustic imaging and Raman imaging.

Keywords: Graphene; photonic crystal; electromagnetically induced transparency; absorption.

## 1. Introduction

Two-dimensional materials have been intensely investigated for their wide applications in biomedicine.<sup>1,2</sup> Specifically, the unique properties of graphene have enabled applications in numerous technological areas. As an example, the fast and broadband

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optical absorption features of graphene have benefited many novel optoelectronic and biosensing applications.<sup>3,4</sup> The desired properties of graphene in these applications mainly include three aspects. First, strong optical absorption from the graphene layers is sought for as it is directly related to the performance of imaging camera,<sup>5</sup> coherent absorption,<sup>6</sup> photoacoustic imaging,<sup>7</sup> and photothermal therapy applications.<sup>8,9</sup> To overcome the low absorption challenge of single-layer graphene, many approaches have recently been proposed, such as one-dimensional photonic crystal (1DPC),<sup>10</sup> microcavity with mirrors,<sup>11</sup> the gratings<sup>12</sup> and the graphene ribbon array.<sup>13</sup> Second, different absorption line shapes are desired. In the above-mentioned structures, light recycle of photon interference at a resonant wavelength is the basic principle to increase the absorption, causing all absorbing responses to have Lorentzian line shapes. In fact, the phenomenon of electromagnetically induced transparency (EIT) found in quantum optical systems has been realized in classical optical structures such as microtoroid,<sup>14</sup> metamaterials,<sup>15</sup> and terahertz waveguide<sup>16</sup> for applications of sensor, filter, slow light, and logic processing. Also, all optical analog EIT has been experimentally achieved by 1D coupled photonic crystal microcavities.<sup>17</sup> On the other hand, Fano resonance with asymmetric line shape is widely investigated in plasmonic systems for its high sensitivity and figure of merit.<sup>18</sup> Third, tunable optical absorption in the near-infrared regime and multi-wavelength operation is desired in graphene-based devices<sup>19,20</sup>; the tunability and multi-wavelength operation allow good match with the laser sources of different wavelengths, while the resultant electrical field enhancement at desired position can be applied for surface-enhanced Raman scattering (SERS)-based biosensing.<sup>21</sup> In configurations reported earlier,<sup>22</sup> however, it is challenging to tune the absorption properties after the structure is fabricated.

In this work, we propose a configuration of a graphene monolayer sandwiched between a buffer layer and 1DPC multilayer. The resultant tunable multichannel absorption property is investigated under the total internal reflection (TIR) condition. Meanwhile, by utilizing the evanescent wave resonance in the 1DPC, the EIT-like and Fano-like absorption is implemented at desired resonance wavelengths due to the interference of light in the proposed configuration. It is shown that the absorption characteristics of the configuration, including the absorption peak positions, widths, intensities, number of the peaks, and the interval between adjacent peaks, are all adjustable without engineering the graphene monolayer. Such a property may find wide use to improve the performances of graphene-based devices and furtherly extend their applications in biosensing.

## 2. Structure Model and Principle

Similar to the EIT phenomenon in an atomic system, in our configuration two "atoms" should be constructed, including one broadband "Atom 1" (bright state) being absorbed and one narrowband "Atom 2" (dark state) being transmitted. The EITlike and Fano-like absorption then can be obtained by detuning the central wavelength of the narrowband transmission peak from that of the broadband absorption. The characteristics of such two-atom configuration, i.e., the buffer-graphene-1DPC multilayer structure, are discussed herein with a schematic shown in Fig. 1. In this system, "Atom 1" realizing the broadband absorption is constructed by designing a multilayer structure producing light interference. The complete absorption is achieved in such a multilayer structure that contains a layer of graphene as the absorption material. On the other hand, the transmission and the reflection of the whole structure are separately engineered to be zero based on the TIR and destructive interference experienced by the reflected light at all layer interfaces,<sup>23</sup> and the position of the broadband absorption peak can be optimized with the help of the transfer matrix method.<sup>24</sup> As for "Atom 2", the



Fig. 1. Schematic of the structure of buffer-graphene-1DPC multilayer. The evanescent wave is coupled into the structure through the prism or the surface of an oblique cross-section of a fiber under TIR.

narrowband transmission is enabled by a periodic structure like the 1DPC that produces the evanescent wave resonance. A perfect narrowband transmission is obtained when the evanescent wave resonance is formed in the low-index dielectric layers under the TIR. In an infinite periodic dielectric multilayers  $(BC)^N$  alternately composed by a layer of high refractive index (B) and a layer of low refractive index (C), the propagation of light satisfies the following equation based on the Bloch theory<sup>25</sup>:

$$\cos[\beta_{z}(d_{b}+d_{c})] = \cos[k_{zb}d_{b}]\cos[k_{zc}d_{c}] - 1/2(q_{b}/q_{c}+q_{c}/q_{b})\sin[k_{zb}d_{b}]\sin[k_{zc}d_{c}],$$
(1)

where  $\beta_z$  is the Bloch vector normal to the layer interfaces of periodic dielectric multilayers  $(BC)^N$ ,  $k_{zb} = k_0 n_b \cos(\theta_b)$  and  $k_{zc} = k_0 n_c \cos(\theta_c)$  are the zcomponents of the wave vector in layers B and C,  $k_0$  is the wave vector in air,  $n_b$  and  $n_c$  are the refractive indexes,  $\theta_b$  and  $\theta_c$  are the incident angles,  $d_b$  and  $d_c$ are the thickness of layer B and C, respectively. If the period of 1DPC is finite, the transmission peak number and  $\beta_z$  have the following relation<sup>25</sup>: for period number N, the values of  $\beta_z$  corresponding to the transmission peaks (light propagating from left to right) are just  $(N-1)(\pi/d)/N, \ldots, (\pi/d)/N$ , where  $d = d_b + d_c$ . Thus, when the material and structure parameters are determined, the position of perfect transmission peak can be solved through Eq. (1).

The absorption characteristics of the onedimensional dielectric multilayers can be investigated based on the above-mentioned transfer matrix method.<sup>24,25</sup> The propagation of light in the one-dimensional multilayer structure with homogeneous materials can be expressed with the production of the matrices for each layer. The transmission matrix for *j*th layer can be written as

$$T_j(d_j,\omega) = \begin{bmatrix} \cos(k_{zj}d_j) & \frac{i}{q_j}\sin(k_{zj}d_j) \\ iq_j\sin(k_{zj}d_j) & \cos(k_{zj}d_j) \end{bmatrix}, \quad (2)$$

where  $d_j$  is the thickness,  $k_{zj} = k_0 n_j \cos(\theta_j)$  is the z component of the wave vector,  $n_j$  is the refractive index,  $\theta_j$  is the incident angle,  $q_j = \sqrt{\varepsilon_j/\mu_j} \cos \theta_j$  for TE wave and  $q_j = \sqrt{\mu_j/\varepsilon_j} \cos \theta_j$  for TM wave,  $\varepsilon_j$  is the permittivity, and  $\mu_j = 1$  is the permeability of the *j*th layer. Matrix  $M_0$  for the whole structure equals to the successive production of the matrices of each layer. The transmission and reflection coefficients of the whole structure can be respectively calculated from  $M_0$  as:

$$r_{0} = \frac{(m_{11} + m_{12}q_{\text{out}})q_{\text{in}} - (m_{21} + m_{22}q_{\text{out}})}{(m_{11} + m_{12}q_{\text{out}})q_{\text{in}} + (m_{21} + m_{22}q_{\text{out}})}, \quad (3)$$

$$t_0 = \frac{2q_{\rm in}}{(m_{11} + m_{12}q_{\rm out})q_{\rm in} + (m_{21} + m_{22}q_{\rm out})}, \quad (4)$$

where  $m_{11}$ ,  $m_{12}$ ,  $m_{21}$ , and  $m_{22}$  are the elements of  $M_0$ ,  $q_{\rm in}$  and  $q_{\rm out}$  are the admittance coefficients of the input and output materials, respectively. The transmission and reflection then can be calculated as  $T = q_{\rm out}/q_{\rm in}|t_0|^2$ ,  $R = |r_0|^2$ . The absorption is A = 1 - T - R.

#### 3. Results and Discussion

To illustrate the validity of the above principle, a typical buffer-graphene-1DPC multilayer structure  $EG(BC)^2$  is presented for achieving the EIT-like and Fano-like absorption performance. The two half-sphere prisms are used to couple light based on a model proposed by Kretschmann.<sup>26</sup> The advantage of using such a scheme is that the polarization response of the configuration can also be investigated if needed. It should be pointed out that prisms of other shapes, such as triangular<sup>27</sup> and half-cylinder,<sup>28</sup> can also be used. The structure parameters are set as follows: the thickness of the G layer  $d_q = 0.34 \,\mathrm{nm}$  and its optical refractive index  $n_q = 3 + i\lambda C_1/3$ , where  $C_1 = 5.446 \,\mu \text{m}^{-1}$ , the refractive indexes of B and C layers are respectively  $n_b = 3.48$  and  $n_c = 1$ , and the buffer layer E is a low-index layer with a refractive index  $n_e = 1$ . Specifically, the optimal thicknesses of B, C and E layers in the structure  $EG(BC)^2$  are separately  $d_b = 269 \text{ nm}, d_c = 500 \text{ nm}, \text{ and } d_e = 220 \text{ nm}, \text{ which}$ are selected to get the perfect absorption of the structure by making the transmission and reflection to be zero under TIR in mid-infrared electromagnetic region. The size of the configuration in the transverse directions theoretically can be infinite.<sup>29</sup> For practical fabrication, according to the reported works, one-dimensional multilayered configuration of centimeter long in the transverse directions can work for investigations within an area  $\sim 100 \times 100 \,\mu \mathrm{m}^2$ .<sup>30,31</sup> In addition, the graphene monolayer with a practical area of  $\sim 0.5 \times 0.5 \,\mathrm{mm}^2$ has been experimentally reported.<sup>32</sup>



Fig. 2. The absorption (A), reflection (R) and transmission (T) spectra of the structure (a) EGBC, (b) BCBC, and (c) EG(BC)<sup>2</sup> under TIR, respectively. The absorption (A), reflection (R), and transmission (T) of graphene monolayer are also plotted in (a) for comparison (dash line).

Figure 2 shows the absorption (A), reflection (R), and transmission (T) of the two composited "atoms" (EGBC and BCBC) as well as the whole structure EG(BC)<sup>2</sup> with incident angle  $\theta = 60^{\circ}$ under TE polarization. From Fig. 2(a), a highly enhanced broadband absorption is observed in the structure EGBC comparing with the 2.3% absorption of graphene monolayer. In Fig. 2(b), the perfect transmission is achieved when the evanescent resonance is formed in the BCBC structure; both absorption and reflection are zero at the resonant wavelength  $\lambda = 1439$  nm. And, as shown in Fig. 2(c), the EIT-like absorption is achieved by  $EG(BC)^2$ structure at the dark state wavelength  $\lambda = 1439 \,\mathrm{nm}$ . This confirms that the formation mechanism of the EIT-like absorption is the combination of the highly enhanced absorption caused by the light interference in the EGBC multilayer and the narrowband perfect transmission caused by the evanescent wave resonance in the 1DPC. This principle to get the EIT-like absorption is different from those reported in the references.<sup>14–17</sup> Moreover, the position and the width of the absorption tip (dark state) can be adjusted by altering the thickness of layer B and C, respectively.

As displayed in Fig. 3, the positions of the absorption tips occur redshift as increasing  $d_b$  (Fig. 3) (a)), and the widths of the absorption tips decrease as increasing the thickness  $d_c$  (Fig. 3(b)). In addition, the number of the absorption tips and the interval between adjacent tips can also be changed by varying the periodic number N and the thickness of the C layer in the middle unit of the 1DPC (denoted as defect layer F), respectively, as shown in Fig. 4. From Fig. 4(a), there are N-1 absorption tips for 1DPC with N periods. From Fig. 4(b), the interval between the adjacent absorption tips increases with reduced thickness of the defect layer  $d_f$ . And the Fano-like absorption is gradually obtained (for  $d_f$ smaller than about  $400 \,\mathrm{nm}$ ) during the increase of the wavelength detuning between the two "atoms".



Fig. 3. The layer thickness-dependent absorption in the structure with N = 2: (a) layer B and (b) layer C. The maximum absorptivity is 1 for all curves.



Fig. 4. The absorption as a function of wavelength  $\lambda$ , with relating to (a) the period N of 1DPC and (b) the thickness of defect layer F of structure EGBCBFBC, respectively.

Moreover, the influence of different thicknesses  $d_f$  of the defect layer F on the spectrum response has also been checked in the structure  $EG(BC)^mBF(BC)^m$ (the total period N = 2m + 1, m = 2, 3). It is noted that the case for m = 1 is given in Fig. 4(b). It is found that that the number of the tips is 2m when the thickness of F is 500 nm. With increased  $d_f$ , the number of tips gradually changes to m main sessions. The interval between the main sessions is defined as the "external interval", and the interval between the two tips within each main session is referred to as the "internal interval". Therefore, the external intervals decrease and the internal intervals increase with reduced  $d_f$ .

As shown in Fig. 5, the absorption of the structure  $\text{EG(BC)}^2$  can be changed by adjusting either the thickness of the buff layer E or the incident angle of light. From Fig. 5(a), an optimized thickness  $d_e = 220 \text{ nm}$  is found to obtain the complete absorption of "atom 1". The perfect transmission caused by the evanescent wave resonance always exists in the structure and is almost independent of the thickness  $d_e$ . From Fig. 5(b), a tradeoff is found between the maximum value of the absorption and the width of the absorption tip. That is, with increased incident angle, the absorption decreases linearly but the tip becomes narrower. The angular-sensitive response of the proposed structure is a significant advantage for designing a good performance directional filter and sensor. For example, the angular-sensitive response is calculated to be  $\sim 70 \text{ nm/degree}$ , i.e.,  $\sim 4010 \text{ nm/radian}$ , for wavelength from 1100 nm to 1800 nm, with an incident angle from  $55^{\circ}$  to  $65^{\circ}$ .

Moreover, the configuration can work in both near-infrared and visible regimes. By properly changing the materials and the geometry parameters of the configuration, the operation wavelength can be transited. At the same time, as demonstrated above, the structure parameters can be selected to make the central wavelength of "atom 2" a little far from that of "atom 1", which will



Fig. 5. The absorption map of the structure  $EG(BC)^2$  for (a)  $A(d_e, \lambda)$  and (b)  $A(\theta, \lambda)$ . The color bar indicates the absorption value.

result in a Fano-like absorption. Figure 6(a) shows single Fano-like absorption at visible region, and the number of the absorption peaks can be changed by varying the period number N of structure BC. Same as the case of EIT, there are N-1 peaks for period number N. Figure 6(b) shows the absorption responses of structure  $EG(BC)^6$  are linear and have five ultra-narrow Fano-like absorption peaks. The full width at half maximum  $\Delta \lambda$  is about 9 pm for the middle peak at  $\lambda = 670.54 \,\mathrm{nm}$ , which corresponds to the quality factor of  $7.45 \times 10^4$  calculated from  $\lambda/\Delta\lambda$ . It is very useful for designing of highsensitive sensor and ultra-narrowband filter. Moreover, for the Fano-like absorption, the electrical field distribution in the structure is also calculated to investigate the influence of the wavelength detuning of "atom 2" from that of "atom 1". Figures 6(c) and 6(d) show the electrical field distributions for the absorption peaks in Fig. 6(a) with Lorentzian and Fano-like shapes, respectively. It is observed that the confinement area of electrical field has obviously been changed from the cavity close to the graphene layer to a more distant one. This confirms that the EIT-like or the Fano-like absorption peak is formed through the interference between the two cavities of "atom 1" and "atom 2". The huge electrical field enhancement with a magnitude of over  $1.4 \times 10^4$  means the SERS enhancement factor beyond of  $3.8 \times 10^{16}$ , which can be potentially applied for single-molecule detection.<sup>33</sup>

Furthermore, when the nonlinear property of the material is considered, the bistable absorption can

be obtained.<sup>34</sup> Figures 7(a) and 7(b) show the nonlinear performances in the cases of EIT-like and Fano-like absorption, respectively. Obviously, the bistable behaviors are observed for both the absorption and reflection curves. As shown in Fig. 7 (a), with a set of suitable structure parameters, the absorption dip of the EIT-like absorption occurs at  $\lambda = 1118$  nm. With increased input light intensity, a nearly zero (~ 10<sup>-4</sup>) absorption arrives at threshold about 10 kW/cm<sup>2</sup>. Whereas, in Fig. 7(b), the complete absorption arrives at  $\lambda = 670.53$  nm with a threshold of 0.8 MW/cm<sup>2</sup>. The much low bistable thresholds show their great potential advantages for the design of all optical switching and logical circuits.

In principle, the EIT and the Fano-like absorption also can be theoretically explained by the coupled mode model. For the structure of EG- $(BC)^{N+1}$ , the N individual "atoms" are characterized by the energy amplitudes of the cavities which are denoted by the energy amplitude array  $\mathbf{a} = [a_1, a_2, \ldots, a_N - 1, a_N]^T$ , where  $a_q$   $(q = 1, \ldots, N)$  represents the energy amplitude in the  $q_{\text{th}}$  cavity. We assume that the input power is  $P_{\text{in}}$ , then the input array  $\mathbf{s} = [-j\mu_i P_i^{1/2}, 0, \ldots, 0, 0]^T$ . The time evolution of the energy amplitude  $\mathbf{a}(t)$  has the following form<sup>35</sup>:

$$\frac{d\mathbf{a}}{dt} = \mathbf{M}\mathbf{a} + \mathbf{s},\tag{5}$$

where  $\mu_i$  represents the normalized coupling coefficient between the incident layer and the "bright"



Fig. 6. The A, R, and T spectra and the electrical field distributions: (a) spectra for structure  $EG(BC)^2$  with single Fano-like absorption peak; (b) spectra for structure  $EG(BC)^6$  with five Fano-like absorption peaks; (c) and (d) the electrical field distributions corresponding to the absorption peaks in (a) with Lorentzian and Fano-like shapes. Each layer of  $EG(BC)^2$  is marked with different colors from the left to the right. Structure parameters include  $n_{prism} = n_b = 3.48$ ,  $d_b = 120 \text{ nm}$ ,  $n_c = 1.55$ ,  $d_c = 269 \text{ nm}$ ,  $n_e = 1.23$ , and  $d_e = 100 \text{ nm}$ .

cavity;  $\mu_z$  (z = 1, ..., N - 1) are those between the adjacent cavities, respectively;  $\Delta \omega_q = 2\pi \Delta f_q$  is the angular frequency detuning from the resonance angular frequency  $\omega_q$  of the *q*th cavity. The coupling matrix **M** is expressed as:

$$\mathbf{M} = -\begin{bmatrix} j\Delta\omega_1 + \frac{\mu_i^2}{2} + \frac{\mu_{L,1}^2}{2} & j\mu_1 & 0 \\ j\mu_1 & j\Delta\omega_2 + \frac{\mu_{L,2}^2}{2} j\mu_2 & & \\ & \ddots & \\ & & j\mu_{N-2} \ j\Delta\omega_{N-1} + \frac{\mu_{L,N-1}^2}{2} & j\mu_{N-1} \\ & & 0 \ j\mu_{N-1} & j\Delta\omega_N + \frac{\mu_{L,N}^2}{2} \end{bmatrix},$$
(6)

where  $\mu_{L,q}^2/2 = 1/\tau_{L,q}$  is the decay rate came from the intrinsic loss, and  $\mu_i^2/2 = 1/\tau_i$  is the decay rate coupled to the incident layer. The absorption amplitude of the system is given by:

$$A_{N} = \frac{\frac{1}{Q_{i}}}{\left(j2\delta_{1} + \frac{1}{Q_{L,1}} + \frac{1}{Q_{i}}\right) + \frac{\overline{q}_{i,1}^{\frac{1}{2}}}{\left(j2\delta_{2} + \frac{1}{Q_{L,2}}\right) + \frac{\overline{q}_{i,1}^{\frac{1}{2}}}{\left(j2\delta_{3} + \frac{1}{Q_{L,3}}\right) + \dots + \frac{\overline{q}_{i,N-1}^{\frac{1}{2}}}{j2\delta_{N} + \frac{1}{Q_{L,N}}}}},$$

$$(7)$$

where the normalized detuning of angular frequency  $\delta_q = \Delta \omega_q / \omega_q, Q_{L,q} = \omega_q \tau_{L,q}/2$ , and  $Q_i = \omega_q \tau_i/2$  are the quality factors related to the intrinsic loss and the incident coupling loss,  $Q_{c,q} = \omega_q \tau_{c,q}/2$  represents the quality factors of the cavity related to the coupling loss for the *q*th cavity, respectively.



Fig. 7. The nonlinear performance of structure EGBCBC: (a) at  $\lambda = 1120 \text{ nm}$  with structure parameters  $n_{\text{prism}} = n_b = 3.48$ ,  $d_b = 200 \text{ nm}$ ,  $n_c = 1.55$ ,  $d_c = 400 \text{ nm}$ ,  $n_e = 1.55$ , and  $d_e = 185 \text{ nm}$ ; (b) at  $\lambda = 670.53 \text{ nm}$  with structure parameters shown in Fig. 6(a). The nonlinear refractive index of layer C is  $n_{c2} = 2.5 \times 10^{-15} \text{ m}^2/\text{W}$  in both calculations.



Fig. 8. Absorption of a system with three cavities. The simulation parameters are set as  $Q_{L,1} = 5 \times 10^4$ ,  $Q_{L,2} = 1 \times 10^8$ ,  $Q_{L,3} = 1 \times 10^8$ ,  $Q_i = 2 \times 10^3$ , and  $Q_{c,1} = Q_{c,2} = Q_{c,3} = 2 \times 10^4$ .

By using Eq. (7), for a typical system with three coupled cavities, Fig. 8 exhibits an EIT-like absorption with two tips, agreeing well with the result in Fig. 4(a). It demonstrates that this model can also be used for inverse design. That is, for a given line shape calculated by the transfer matrix method, the coupling coefficients and the detuning wavelength of the individual cavity in a coupled resonator structure can be fitted and extracted by the coupled mode model. This builds a link between the desired spectral property and the geometric parameters for the design of the device with the characteristic of EIT-like absorption. This can be potentially applied for absorption-based imaging as targets with varied refractive index response can be located in the buffer or B sensing layer.

It should be clarified at this point that the captioned manuscript focuses on numerical simulation as the first step of the project to make sure of the feasibility and optimum design. That said, experiments have been planned and under preparation. In the following, the fabrication of the structure is briefly discussed herein. For multiple graphene layers, researches have reported the realization of enhanced absorption between two dielectric materials.<sup>23</sup> For monolayers, there are studies positioning the graphene monolayer in a microcavity to form a photodetector,<sup>3,36</sup> which may be used as reference in fabrication. Specifically, when silicon and air materials are used (e.g., Figs. 1–5), the silicon-air filter can be fabricated using the method in Ref. 37. The graphene monolayer can also be fabricated through a suspended structure.<sup>38</sup> When other dielectric materials are used (e.g., Fig. 6), the multiple dielectric layers can be fabricated through plasma-enhanced chemical vapor deposition (PECVD)<sup>3,39</sup> or spin-coating.<sup>32</sup>

Note that imperfections, such as twisted or folded regions, are inevitable during fabrication, which will reduce the performance of the spectrum response obtained in numerical simulation. That said, recent developments in the field have allowed for fabrication of large-area continuous and uniform graphene monolayers.<sup>40,41</sup> For example, graphene monolayers of  $\sim 3.5 \times 1.5$  cm<sup>2</sup> have been achieved.<sup>40</sup> Lastly, but not the least, the following dielectric material parameters will be considered in fabrication: for the silicon-air configuration in near-infrared as shown in Figs. 1–5, silicon with n = 3.48 will be used for prism and B layer (E, F, and C layers are air);<sup>42</sup> for the multiple dielectric layers in Fig. 6, SiO<sub>2</sub> (quartz) with n = 1.55 will be used for B layer, but nanoporous SiO<sub>2</sub> with a low-refractive-index material n= 1.23 [44] will be used for C layer;<sup>43</sup> for nonlinear application in Fig. 7, silicon with n = 3.48 will be used for prism and B layer, and polydiacetylene 9-BCMU organic material with n = 1.55 and high nonlinear coefficient  $n_{c2}$  will be used for C layer.<sup>45</sup>

### 4. Conclusions

In summary, to achieve tunable absorptions characteristics for biosensing, a buffer-graphene-1DPC multilayer structure is proposed to obtain the EITlike and the Fano-like absorptions in the nearinfrared regime. The absorption property of the structure can be tuned by changing the geometric or physical parameters of the designed configuration and the incident angle of light. The tunable multichannel EIT-like and Fano-like absorptions may be applied for designing of various biosensing devices, such as sensor, filter, modulator, optical tagging, thermal detecting, optical switching and all-optical diode.<sup>46–48</sup> Moreover, the structure with EIT-like and Fano-like absorption in visible and near-infrared regimes can potentially be extended to infrared and even terahertz spectrum for more applications in biosensing.

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#### **Conflicts of Interest**

The authors have no conflicts of interest relevant to this article.

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