

Research Article

Influence of Shape Anisotropy on Magnetization Dynamics Driven by Spin Hall Effect

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As the lateral dimension of spin Hall effect based magnetic random-access memory (SHE-RAM) devices is scaled down, shape anisotropy has varied influence on both the magnetic field and the current-driven switching characteristics. In this paper, we study such influences on elliptic film nanomagnets and theoretically investigate the switching characteristics for SHE-RAM element with in-plane magnetization. The analytical expressions for critical current density are presented and the results are compared with those obtained from macrospin and micromagnetic simulation. It is found that the key performance indicators for in-plane SHE-RAM, including thermal stability and spin torque efficiency, are highly geometry dependent and can be effectively improved by geometric design.

1. Introduction

The effect of spin-transfer torque [1–3] has been investigated extensively in the last decade due to its potential applications in spin-transfer torque magnetic random-access memory (STT-RAM) [4–7], nanoscale microwave generators [7–10], and spin based logic devices [11]. The functional element utilizing spin-transfer torque is commonly a magnetic tunnel junction (MTJ) with a magnetic free layer and reference layer separated by a tunneling barrier. For STT-RAM, the bit is stored by the relative orientation of magnetization of free layer and reference layer, and the polarized current is used to change its state between parallel (P) and antiparallel (AP). In order to balance the demands for low threshold current, high thermal stability, and small element size, MTJ stacks with different materials and structures have been proposed. In the last few years, MTJ with perpendicular magnetization has attracted much attention since the strong interfacial magnetic anisotropy in CoFeB/MgO bilayer reduces the switching current density by canceling out the demagnetization field [12–14]. However, as the element dimension keeps scaling down, time dependent dielectric breakdown (TDDB) becomes a critical issue restraining the performance of perpendicular

MTJ [15]. More recently, a three-terminal MTJ utilizing spin Hall effect (SHE) [16] has been demonstrated to be an effective solution [4, 17, 18]. Pure spin current, due to spin orbit interaction, can be generated by applying a current to a heavy metal (β -W [19, 20], β -Ta [21], and Pt [22]) adjacent to the free layer of MTJ.

Apparently, the SHE-RAM allows for further scaling down of the nonvolatile memory element. However, there is a critical issue from the scaling perspective, that is, the influence of shape anisotropy on switching characteristics, which needs to be carefully examined. In previous macrospin based researches, simplified expressions of the shape anisotropy were often used with the assumption that the area of free layer is large compared with its thickness. However, as the element dimension is scaled down, this simplification frequently becomes a nontrivial source of error when studying the switching current and thermal stability of STT-RAM elements [23–26]. The problem can be addressed by either micromagnetic modeling or accurate demagnetizing factors for macrospin model.

In this paper, we introduce the analytic demagnetizing factors for elliptic film nanomagnets and theoretically investigate the geometric dependent critical current density

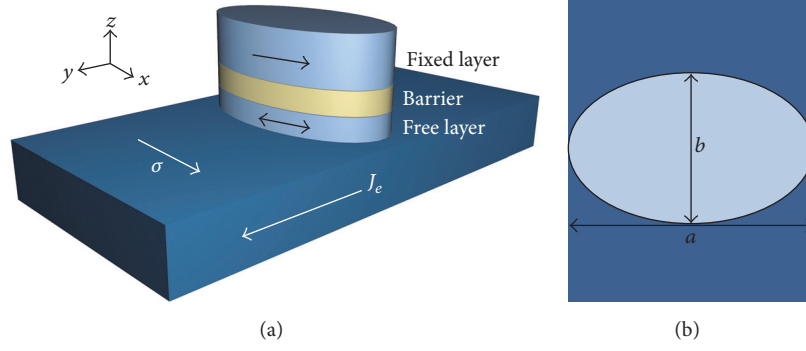


FIGURE 1: The sketch of in-plane SHE-RAM element.

for SHE-RAM with in-plane magnetization. We present the analytic expressions for both current densities leading to magnetization instability and switching. The analytic results are compared with macrospin and micromagnetic numerical simulation, and good consistency is found below a critical size. We further analyze the geometric dependent thermal stability and spin torque efficiency in room temperature, and it is found that these key performance indicators can be effectively improved by geometric design.

The remainder of this paper is organized as follows. Section 2 gives the theoretical model and analytic equations for demagnetizing factors and critical current density. Section 3 presents the dependence of zero temperature critical current density on free layer geometry and the comparisons between analytic expression, macrospin, and micromagnetic simulation. Section 4 introduces thermal fluctuation by stochastic LLG equation, and the element characteristics concerning thermal fluctuation are investigated. Section 5 summarizes the paper and draws the conclusion. SI units are used for equations and results in this paper.

2. Model Detail

2.1. LLGS Equation. Figure 1 is a sketch of the in-plane SHE-RAM element. The short axis lies in y direction with length b . The long axis of the free layer lies in x direction with length a , which is also the width of the heavy metal layer, as shown in Figure 1(b).

The magnetization dynamics of the in-plane MTJ driven by SHE polarized current are similar to that of a conventional STT-RAM and can be described by the Landau-Lifshitz-Gilbert equation with an SHE spin torque term [27] as follows:

$$\frac{d\mathbf{m}}{dt} = -\gamma \mathbf{m} \times (\mathbf{H}_{\text{eff}} + \mathbf{H}_{\text{the}}) + \alpha \mathbf{m} \times \frac{d\mathbf{m}}{dt} + a_J \mathbf{m} \times (\mathbf{m} \times \boldsymbol{\sigma}), \quad (1)$$

where \mathbf{m} and $\boldsymbol{\sigma}$ are the normalized magnetization of the free layer and spin polarization vector, respectively, $\gamma = 1.76 \times 10^{11} \text{ T}^{-1} \text{ s}^{-1}$ is the gyromagnetic ratio, α is the Gilbert

damping constant, and a_J is the spin torque strength which can be expressed as [28]

$$a_J = \frac{\gamma \hbar J_e \theta_{\text{SH}}^{\text{eff}}}{2\mu_0 e t_f M_s}, \quad (2)$$

where \hbar is the reduced Planck constant, J_e is the charge current density applied to the heavy metal layer in the y direction, e is the electron charge, μ_0 is the permeability of vacuum, $\theta_{\text{SH}}^{\text{eff}}$ is the material dependent effective spin Hall angle, and t_f is the thickness of the free layer. In our latter discussion, we assume $\alpha = 0.01$, $M_s = 1 \times 10^6 \text{ A/m}$, and $\theta_{\text{SH}}^{\text{eff}} = 0.32$ to simulate the CoFeB-based MTJ adjacent to an 8 nm β -W thin film [20]. \mathbf{H}_{the} is the stochastic field related to thermal fluctuation. Based on the framework of Brown [29], it can be expressed as follows:

$$\langle \mathbf{H}_{\text{the}} \rangle = 0, \quad \langle \mathbf{H}_{\text{the},i}(t_1) \mathbf{H}_{\text{the},j}(t_2) \rangle = \frac{2k_b T \alpha}{\mu_0 \gamma M_s V} \delta_{ij} \delta(t_1 - t_2), \quad (3)$$

where $i, j = 1, 2$, and 3 and $\mathbf{H}_{\text{the},i}$ refers to the Cartesian component of the stochastic field. k_b is the Boltzmann constant, T is the temperature in kelvin, and V is the volume of the free layer. \mathbf{H}_{eff} represents the effective field. Since bulk anisotropy is ruled out, the energy density of the free layer with a zero applied field is

$$E_{\text{total}} = E_{\text{demag}} = \frac{1}{2} \mu_0 M_s^2 (N_x m_x^2 + N_y m_y^2 + N_z m_z^2), \quad (4)$$

where m_x , m_y , and m_z are the three components of the normalized magnetization \mathbf{m} and N_x , N_y , and N_z are the demagnetizing factors along the corresponding directions. Since $m_x^2 + m_y^2 + m_z^2 = 1$, we have

$$E_{\text{total}} = \frac{1}{2} \mu_0 M_s^2 (N_x - N_y) m_x^2 + \frac{1}{2} \mu_0 M_s^2 (N_z - N_y) m_z^2 + \frac{1}{2} \mu_0 M_s^2 N_y, \quad (5)$$

and \mathbf{H}_{eff} can be derived from the magnetic energy density of the free layer as

$$\mathbf{H}_{\text{eff}} = (N_y - N_x) M_s \mathbf{m}_x - (N_z - N_y) M_s \mathbf{m}_z, \quad (6)$$

with the easy axis anisotropy field \mathbf{H}_k in the long axis direction with strength $(N_y - N_x)M_s$ and the demagnetizing field \mathbf{H}_d normal to the film plane with strength $(N_z - N_y)M_s$.

2.2. Demagnetizing Factors. The analytic demagnetizing factors for elliptical disk can be expressed as a power series expansion of the ratio between the disk thickness and long axis length, $\tau = t_f/a$ [30, 31], with a “squat elliptic cylinder” limit ($b > 2t_f$):

$$\begin{aligned} N_x &= \frac{1}{8\pi^2\lambda} (J_1 - J_2), \\ N_y &= \frac{\lambda}{8\pi^2} (J_1 + J_2), \\ N_z &= 1 - N_x - N_y, \end{aligned} \quad (7)$$

where

$$\begin{aligned} J_1 &= 16\tau \left\{ L_0 - \left(\frac{1}{2} + \ln \frac{\tau}{4} \right) I_0 + \frac{\tau^2}{8} \left[L_1 \right. \right. \\ &\quad \left. \left. + \left(\frac{1}{4} - \ln \frac{\tau}{4} \right) I_1 \right] + O(\tau^4) \right\}, \\ J_2 &= \frac{16\tau}{\gamma} \left\{ (1 + \varepsilon) L_{-1} - L_0 + \left(\frac{3}{2} - \ln \frac{\tau}{4} \right) [(1 + \varepsilon) I_{-1} \right. \right. \\ &\quad \left. \left. - I_0] - \frac{\tau^2}{24} \left[(1 + \varepsilon) L_0 - L_1 \right. \right. \right. \\ &\quad \left. \left. - \left(\frac{5}{12} + \ln \frac{\tau}{4} \right) [(1 + \varepsilon) I_0 - I_1] \right] + O(\tau^4) \right\}, \\ I_{-1} &= E \left(1 - \frac{1}{\lambda^2} \right), \\ I_0 &= K \left(1 - \frac{1}{\lambda^2} \right), \\ I_1 &= \beta^2 K \left(1 - \frac{1}{\lambda^2} \right), \\ L_{-1} &= \frac{1 + \lambda^2}{2\lambda^2} K \left(1 - \frac{1}{\lambda^2} \right) - \left(\frac{\ln \lambda}{2} + 1 \right) E \left(1 - \frac{1}{\lambda^2} \right), \\ L_0 &= -\frac{\ln \lambda}{2} K \left(1 - \frac{1}{\lambda^2} \right), \\ L_1 &= \lambda^2 \left[\left(1 - \frac{\ln \lambda}{2} \right) E \left(1 - \frac{1}{\lambda^2} \right) - \frac{1 + \lambda^2}{2\lambda^2} K \left(1 - \frac{1}{\lambda^2} \right) \right], \end{aligned} \quad (8)$$

with aspect ratio $\lambda = a/b$, $\varepsilon = (\lambda^2 - 1)/(\lambda^2 + 1)$, and K, E refer to the complete elliptic integral of the first and second kind, respectively. In previous research works, simplified shape anisotropy was commonly used as $H_{ks} = 2(1/b - 1/a)t_f M_s$ [32–35]. It however leads to overestimation as Figure 2 depicts. For an MTJ sample with a size of $45 \text{ nm} \times 15 \text{ nm} \times 3 \text{ nm}$,

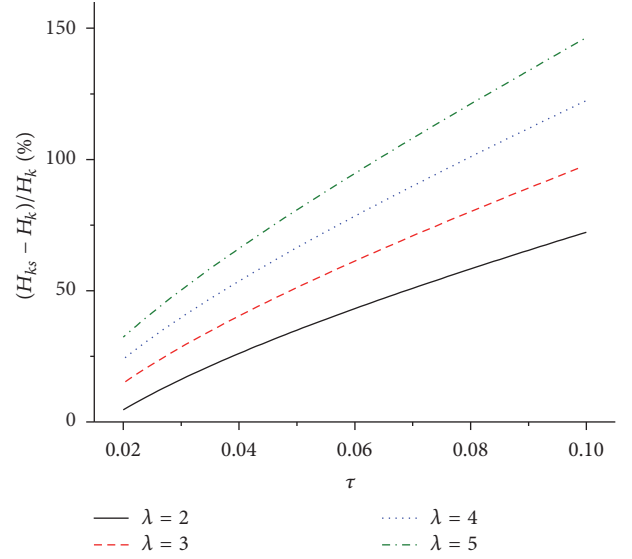


FIGURE 2: The deviation percentage caused by simplified shape anisotropy with varied τ and λ .

the shape anisotropy field is overestimated by 70%, leading to poor predictions of device characteristics.

2.3. Current Density for Instability and Switching. The analytical expression of the critical current density necessary for the in-plane MTJ free layer magnetization to become unstable has been introduced by Sun [36] as follows:

$$J_{\text{ins}} = \frac{2e\alpha t_f \mu_0 M_s}{\hbar \eta} \left(H_k + \frac{H_d}{2} \right). \quad (9)$$

And the critical current density for magnetization switching is given by [37, 38] as

$$J_{\text{sw}} = \frac{4e\alpha t_f \mu_0 M_s}{\pi \hbar \eta} \sqrt{H_d (H_d + H_k)}, \quad (10)$$

where η is the spin polarization, and for SHE device it should be the effective spin Hall angle. An intermediate current density will drive the magnetization towards oscillation state, which is not sensitive to the initial angle θ_0 . With results from (6), the analytical critical current densities for an in-plane SHE-RAM can be written as

$$\begin{aligned} J_{\text{ins}} &= \frac{e\alpha t_f \mu_0 M_s^2}{\hbar \theta_{\text{SH}}^{\text{eff}}} (1 - 3N_x), \\ J_{\text{sw}} &= \frac{4e\alpha t_f \mu_0 M_s^2}{\pi \hbar \theta_{\text{SH}}^{\text{eff}}} \sqrt{(N_z - N_y)(N_z - N_x)}. \end{aligned} \quad (11)$$

3. Zero Temperature Simulation Results

3.1. Analytic Results. In this section, we exclude the influence from temperature and use a free layer with $t_f = 1.5 \text{ nm}$ and $\lambda = 2$. Figure 3 shows J_{ins} and J_{sw} dependence on the long axis length of the free layer. It can be seen that J_{sw} drops more

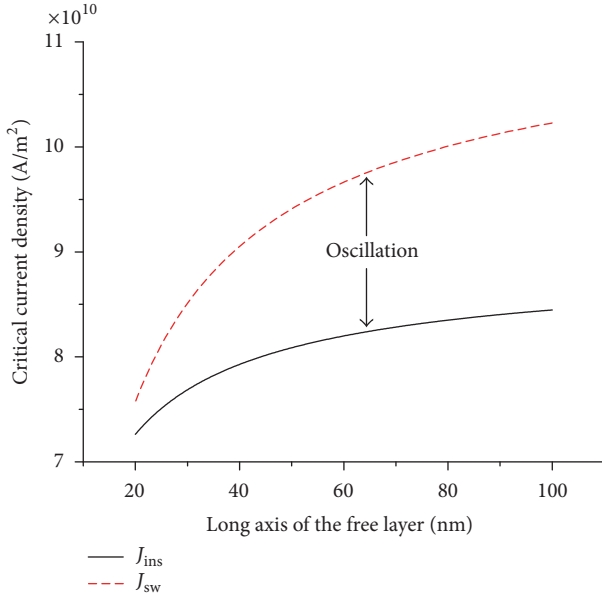


FIGURE 3: J_{ins} and J_{sw} dependence on long axis length of the free layer with $t_f = 1.5$ nm and $\lambda = 2$. Intermediate current density leads to stable oscillation of \mathbf{m} .

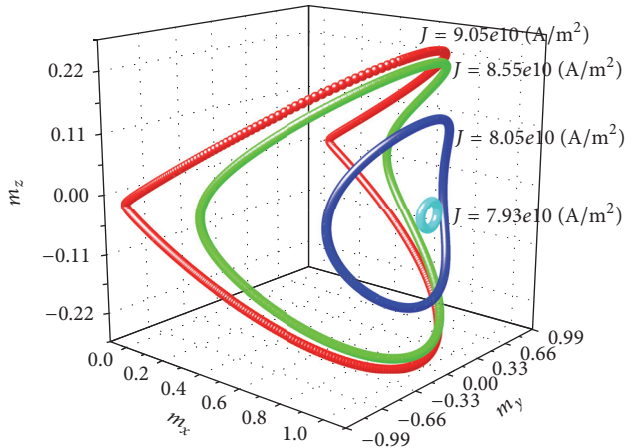


FIGURE 4: Magnetization oscillating trajectory with different current densities for in-plane free layer with initial state $m_x \approx 1$. Higher current density leads to oscillation with larger cone angle and finally switching. The free layer size is $40 \text{ nm} \times 20 \text{ nm} \times 1.5 \text{ nm}$, with $J_{\text{ins}} = 7.93 \times 10^{10} \text{ A/m}^2$ and $J_{\text{sw}} = 9.05 \times 10^{10} \text{ A/m}^2$.

rapidly and approaches J_{ins} as the lateral dimension scales down, which also indicates that a smaller current density span allows for oscillation to occur. The magnetization oscillating trajectories with different current densities are shown in Figure 4. J_{ins} leads to small cone angle precession illustrated by the cyan circle, while J_{sw} leads to a clamshell-shaped trajectory illustrated in red. Current density higher than J_{sw} leads to magnetization switching. The results from the analytical expressions agree with that obtained from macrospin modeling.

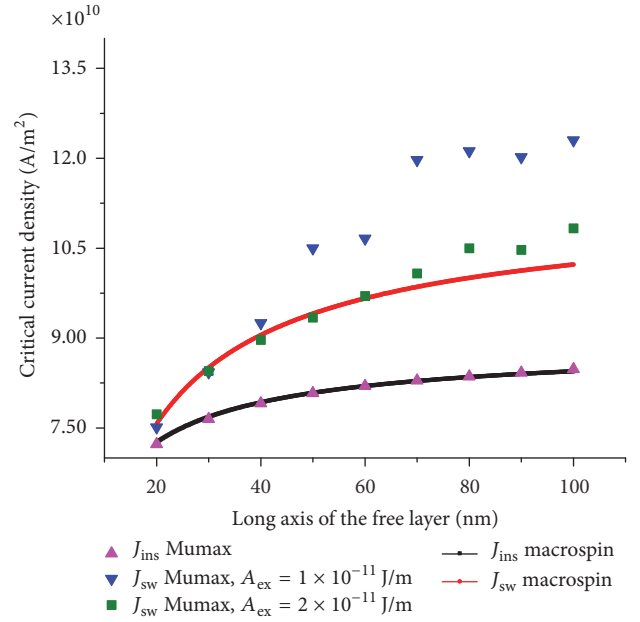


FIGURE 5: The critical current densities obtained from macrospin model and micromagnetic simulation.

3.2. Macrospin and Micromagnetic Results. The critical current densities based on macrospin and micromagnetic simulations are compared in Figure 5. An open-source code, Mumax [39], was used for micromagnetic simulation with a mesh of $64 \times 32 \times 1$ set for all geometries for better GPU performance. The initial magnetization tilt angle is 5 degrees. Good consistency can be observed in J_{ins} , indicating uniform magnetization for small cone angle precession. The discrepancy in J_{sw} indicates that noncoherent oscillating or switching behavior takes place for larger nanomagnet size. For samples with exchange stiffness constant $A_{\text{ex}} = 1 \times 10^{-11} \text{ J/m}$, J_{sw} rises due to increased exchange energy when $a > 40$ nm and keeps around $1.2 \times 10^{11} \text{ A/m}^2$ when $a > 70$ nm, as shown by the blue triangle. For samples with $A_{\text{ex}} = 2 \times 10^{-11} \text{ J/m}$, the discrepancy is alleviated and can be observed when $a > 60$ nm, as shown by the green square.

Figure 6 shows the magnetization components during the switching process of an $80 \text{ nm} \times 40 \text{ nm} \times 1.5 \text{ nm}$ free layer. The applied current density is $1.2 \times 10^{11} \text{ A/m}^2$. It can be seen that the magnetization experiences a period of oscillation before switching occurs. Figure 7 shows the corresponding magnetization spatial distribution. The noncoherent magnetization behavior can be observed at the two ends of the free layer, which is more obvious in Figure 7(d). Magnetization switching occurs when the magnetization in the central part of the free layer oscillates across the short axis.

4. Thermal Effect and Stability Analysis

As the free layer size is scaled down below 100 nm, the thermal fluctuation becomes significant and will have an impact on the SHE-RAM characteristics. In this section, we use (3) to account for the influence of thermal fluctuation, and

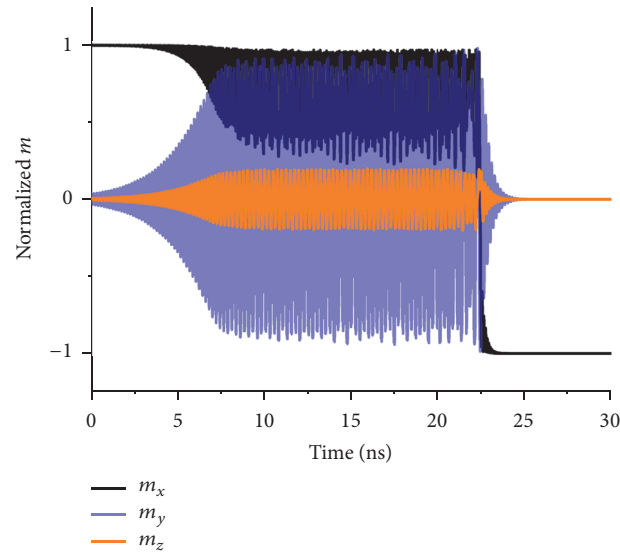


FIGURE 6: Free layer magnetization components during a switching process. The applied current density is 1.2×10^{11} A/m. The magnetization oscillating time before switching is 22 ns.

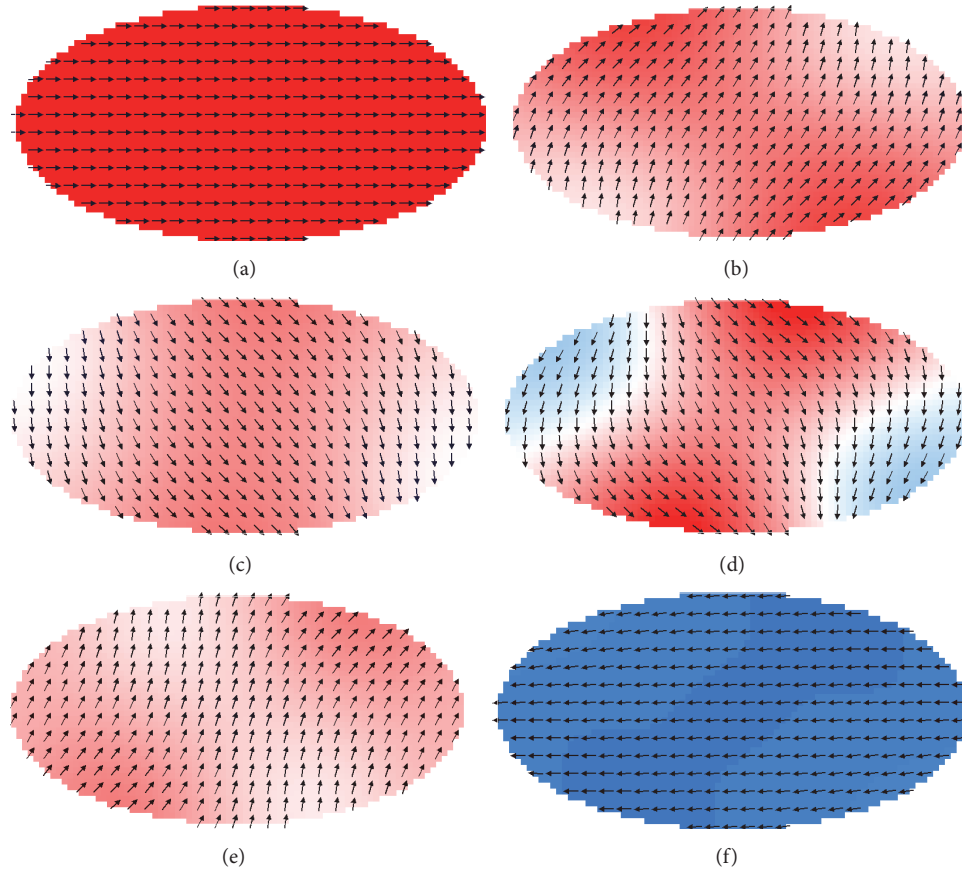


FIGURE 7: Magnetization spatial distribution corresponding to Figure 6. The snapshots (a)~(f) are picked at 3 ns, 7 ns, 11 ns, 15 ns, 19 ns, and 23 ns during the switching process.

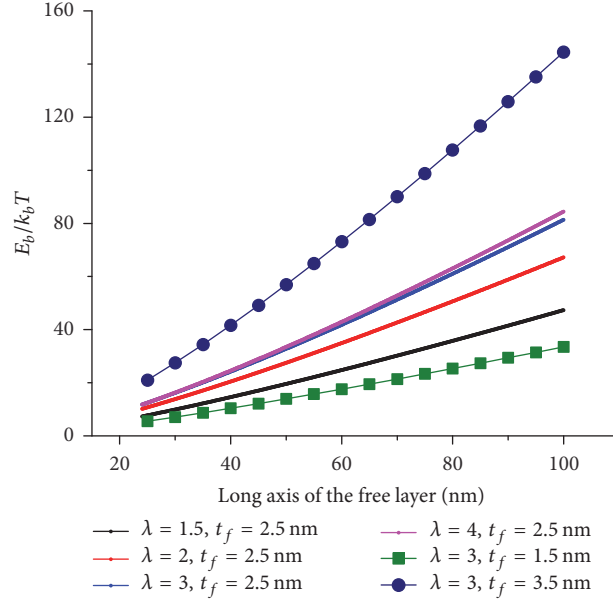
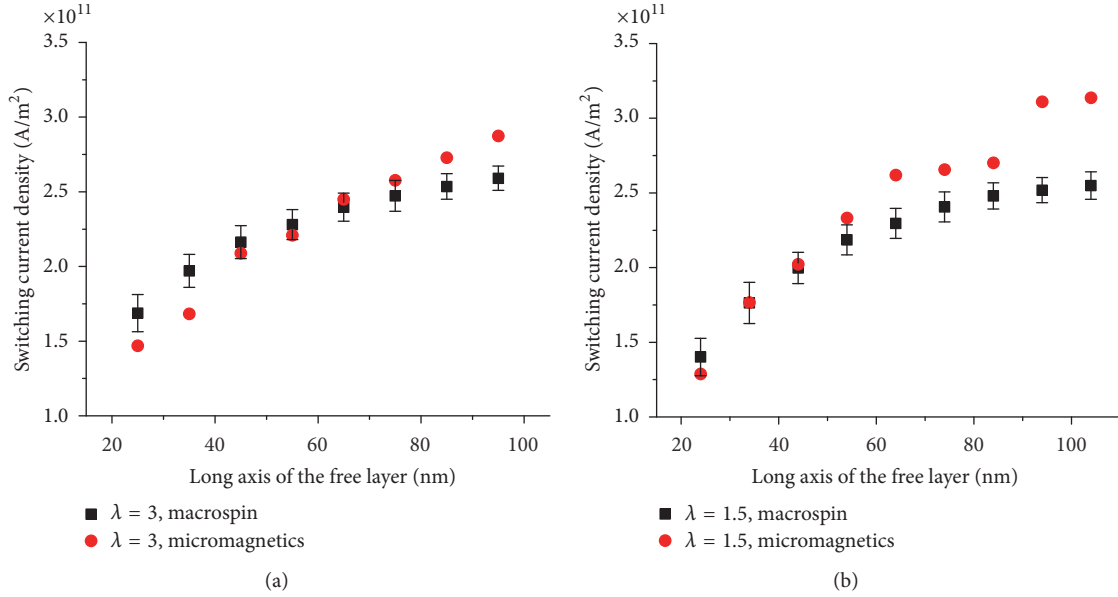


FIGURE 8: Geometric dependence of thermal stability.

FIGURE 9: Current densities lead to magnetization switch in 5 ns in room temperature for free layers with (a) $\lambda = 3$ and (b) $\lambda = 1.5$.

the geometry dependent thermal stability and the spin torque efficiency in room temperature (300 K) are investigated.

The energy barrier of the free layer can be described by $E_b = \mu_0 M_s^2 V (N_y - N_x)/2$. It is found that thermal stability $\Delta = E_b/k_b T$ scales almost linearly with the long axis length rather than the area of free layer, as shown in Figure 8. The reason is that the shape anisotropy which determines the energy barrier decreases with the dimension of the free layer. This tendency is similar to that of perpendicular MTJs used for conventional STT-RAM [23]. We further investigate the influences from aspect ratio λ and free layer thickness t_f .

It is found that Δ can be effectively improved by tapering the free layer; this gain however saturates when $\lambda > 3$, as illustrated by the solid lines without symbol in Figure 8. The improvement of Δ with free layer thickness can be attributed to the enhanced easy axis anisotropy and a larger volume, as shown by lines with solid symbol.

Figure 9 shows the critical current density necessary for a free layer with $t_f = 3.5$ nm to switch in 5 ns in room temperature. The results from both macrospin and micromagnetic modeling are shown. It can be noted that, despite the improvement in thermal stability, higher λ does not lead to an

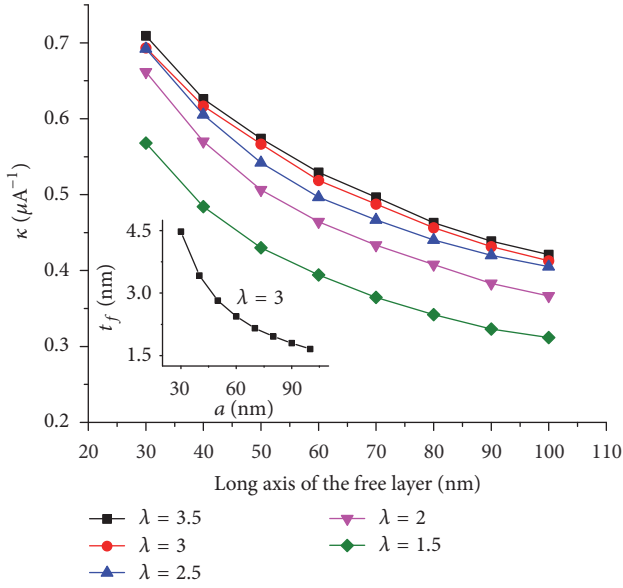


FIGURE 10: Geometric dependence of spin torque switching efficiency with fixed thermal stability $\Delta = 40$. The inset shows the corresponding adjustment of thickness of free layer with $\lambda = 3$.

obvious increase in switching current density, which is due to a smaller demagnetizing field. We used $A_{\text{ex}} = 1 \times 10^{-11}$ J/m for micromagnetic modeling. The discrepancy between results from macrospin and micromagnetic modeling for larger geometries indicates the nonuniform magnetization during switching process that, for smaller geometries, as shown in Figure 9(a), might be caused by coarse mesh. It can be noted that the free layer with $\lambda = 1.5$ is more susceptible to nonuniform behavior, and this is due to a larger area compared with free layers with $\lambda = 3$.

The spin torque efficiency is defined as $\kappa = \Delta/I_c$. For SHE-RAM, $I_c = J_c a t_w$, where t_w is the thickness of the tungsten layer. In order to analyze the geometric dependence of κ for devices satisfying the retention requirement, the thermal stability Δ is fixed at 40 by adjusting the thickness of the free layer, while the length of long axis, a , and the aspect ratio, λ , are varied. It is found that the spin torque efficiency decreases with a , as shown in Figure 10. Moreover, improvement of κ can be observed in the free layer with higher aspect ratio. This improvement also saturates when $\lambda > 3$, similar to that of thermal stability. The inset of Figure 10 shows the thickness adjustment of free layer with $\lambda = 3$.

5. Conclusion

In this paper, we have studied the influence of shape anisotropy on switching dynamics of elliptic nanomagnets by introducing accurate demagnetizing factors and theoretically investigated the characteristics of SHE-RAM with in-plane magnetization. Analytic expressions of the key performance indicators for in-plane SHE-RAM are obtained including the critical switching current density, thermal stability, and spin torque efficiency, which are found to be highly geometry

dependent. In particular, the thermal stability and spin torque efficiency can be effectively improved by selecting the appropriate aspect ratio of the free layer. Moreover, the spin torque efficiency tends to increase as the SHE-RAM element is scaled down. The demagnetizing factors can also be applied to the macrospin approach to give more reliable characteristic predictions for sub-100 nm spin torque based device.

Competing Interests

The authors declare that they have no competing interests.

Acknowledgments

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