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# Investigation on fiber-optic curvature sensor based on SMF-FMF-SMF structure with up-taper fusion

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## ABSTRACT

A compact fiber-optic curvature sensor based on modal interferometer (MI) in few mode fiber (FMF) is presented and investigated both in theory and experiment. The proposed MI is simply constructed by splicing a 2-centimeter-long FMF between single mode fibers (SMFs) with built-in up-taper fusion mode, i.e., SMF-FMF-SMF structure is fabricated. Both the curvature sensing performance and temperature dependency are addressed, and the result shows that curvature within a range from 0 m<sup>-1</sup> to 1.87 m<sup>-1</sup> can be monitored without ambiguity and the temperature sensitivity can reach up to 111 pm/°C.

**Keywords:** Fiber-optic, curvature, few mode fiber

## 1. INTRODUCTION

With the development of the modern industry, like super high buildings, railways, tunnels, bridges, etc., real-time and long-term curvature monitoring is extremely important, to avoid severe accidents and disasters. Traditional electrical curvature sensors suffer problems including vulnerable to electromagnetic interference, hard to work in harsh environments, etc. [1] As for fiber-based curvature sensor, it intrinsically overcome these drawbacks together with merits of long distance and distributed sensing, compact in size, high sensitivity and low maintenance cost [1]. Therefore, it is a promising technique in curvature sensing, which has been investigated a lot, including multi-core fiber (MCF) based, single/multi-mode fiber (SMF/MMF) based, photonic crystal fiber (PCF), etc. with or without grating inscription.

Y. Wu et al [2] proposed an asymmetrical twin-core fiber based MI utilizing MMF to realize mode excitation and recoupling, achieving a high curvature sensitivity of 103.35 nm/m<sup>-1</sup> and 0.431 nm/°C within 0.24 ~ 0.6 m<sup>-1</sup>. S. Wang et al [3] presented a curvature sensor based on three-core fiber with asymmetric core distribution and different core diameters inscribed by two non-orthogonal long period gratings, realizing curvature and temperature sensitivity of 3.234 nm/m<sup>-1</sup> in a range of 0 m<sup>-1</sup> ~ 0.588 m<sup>-1</sup> and 56 pm/°C. In a similar structure, X. Wang et al [4] utilized a seven core fiber to form the MI obtaining a curvature and temperature sensitivity of 31.54 nm/m<sup>-1</sup> in 0.45 m<sup>-1</sup> ~ 1.01 m<sup>-1</sup> and 55.81 pm/°C respectively. One can see that as for MCF-based, the structure is kind of complexity and high fabrication difficulty, especially for grating inscription.

As for SMF/MMF-based, S. Dong et al [5] proposed a cascade MI constructed with dual-up-taper in SMF to monitor the curvature, achieving a curvature sensitivity of 4.362 nm/m<sup>-1</sup> from 0 to 1.134 m<sup>-1</sup> and a temperature sensitivity of 108 pm/°C. R. Wang et al [6] presented a SMF-MMF-SMF-MMF-SMF structure to form the MI between core mode and cladding mode with a sensitivity of -14.4 nm/m<sup>-1</sup> in the range of 0 m<sup>-1</sup> ~ 1.134 m<sup>-1</sup> and a temperature sensitivity of 63 pm/°C. PCF is known for its ultra-low temperature response and H. Gong et al [7] presented a SMF-PCF-SMF based curvature sensing obtaining curvature sensitivity 4.451 nm/m<sup>-1</sup> in a range of 0 m<sup>-1</sup> ~ 2.14 m<sup>-1</sup> and temperature sensitivity of 7.78 pm/°C.

In this paper, a compact SMF-FMF-SMF with up-taper fusion is proposed and the curvature monitoring performance and temperature dependency are addressed. The length of the FMF is about 2 centimeters supporting LP<sub>01</sub> and LP<sub>11</sub> mode and the whole fabrication process is very simple with built-in fusion mode. Besides, compared with PCF or MCF, FMF is more cost-effective and easy to operate.

## 2. PRINCIPLE

The schematic of the proposed SMF-FMF-SMF structure is sketched in Fig. 1. It mainly consists of a section of FMF sandwiched in SMFs with up-taper connection. When the incident light leaded by the core of the SMF meets the first up-taper junction, high order core modes of FMF mainly including LP<sub>01</sub> and LP<sub>11</sub> will be effectively stimulated owing



Figure 1. Schematic of the SMF-FMF-SMF structure.

to mismatched mode field distributions. After propagating the FMF, the light meets the second junction and recouples back into the core of the lead out SMF. The output light amplitude  $E_{out}$  can be simply described as follows:

$$E_{out} = E_{01}e^{j\varphi_{01}} + E_{11}e^{j\varphi_{11}}. \quad (1)$$

The output intensity  $I_{out}$  is calculate by

$$\begin{aligned} I_{out} &= E_{out} \times E_{out} \\ &= E_{01}^2 + E_{11}^2 + 2E_{01}E_{11} \cos(\varphi_{01} - \varphi_{11}) \\ &= E_{01}^2 + E_{11}^2 + 2E_{01}E_{11} \cos(\Delta\varphi) \\ &= E_{01}^2 + E_{11}^2 + 2E_{01}E_{11} \cos(2\pi\Delta nL / \lambda) \end{aligned} \quad (2)$$

where  $E_{01}$ ,  $E_{11}$  are the amplitude of the exited mode,  $L$  is the length of the FMF,  $\lambda$  is the wavelength in vacuum,  $\Delta n$  is the effective index difference. The external curvature will influence the  $\Delta n$  between excited LP<sub>01</sub> and LP<sub>11</sub> mode. Assuming the  $\Delta n$  equals to  $(2k+1)\pi$ , one can obtain that

$$\lambda_{dip} = \frac{2\Delta nL}{2k+1}. \quad (3)$$

Therefore, we can collect the wavelength shift to track the curvature.

## 3. EXPERIMENT AND DISCUSSION

To investigate its curvature monitoring performance, experimental setup is established as shown in Fig. 2, including a broad band source (BBS), a sensing element, and an optical spectrum analyzer (OSA). The sensing element is arranged as most of the curvature sensing scheme [1]. As shown in Fig. 3, it shows the spectrum of the sensing structure without curvature applied. One can see that there exist two dips denoted with Dip1 and Dip2 respectively. We can track the wavelength shift to study the curvature dependency.

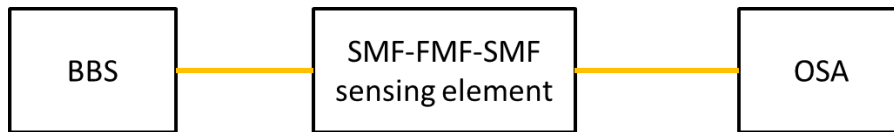


Figure 2. Experimental setup.

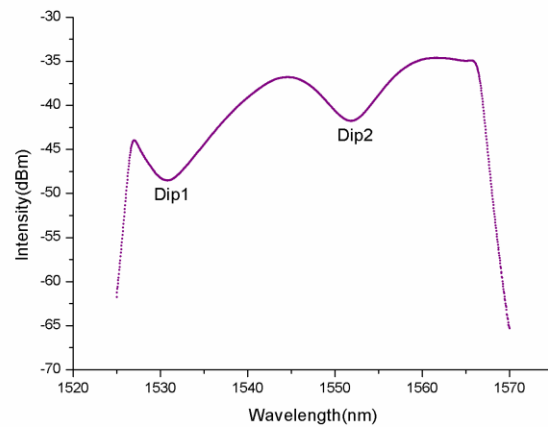


Figure 3. Spectrum of the sensing element without curvature applied.

As shown in Fig. 4, Dip2 is used to track the curvature change within a range of  $0 \text{ m}^{-1} \sim 1.87 \text{ m}^{-1}$ . Here, we use polynomial fitting line to fit the data, which has a high  $R^2$  more than 0.99. The nonlinearity mainly results from the different mode excitations, i.e., with the increasing curvature, the excited mode could be changed. Therefore, it shows piecewise linear characteristics. Besides, the estimated linear sensitivity is about  $-6.7 \text{ nm/m}^{-1}$  with  $R^2$  of 0.96.

Fig. 5 shows the temperature dependency within a range of  $25.9 \text{ }^{\circ}\text{C} \sim 67.9 \text{ }^{\circ}\text{C}$  for Dip1 and Dip2 respectively. The linearity of the fitting lines for both two Dips are 0.999 and 0.997 with similar sensitivity of  $127.2 \text{ pm/ }^{\circ}\text{C}$  and  $116.9 \text{ pm/ }^{\circ}\text{C}$ , respectively.

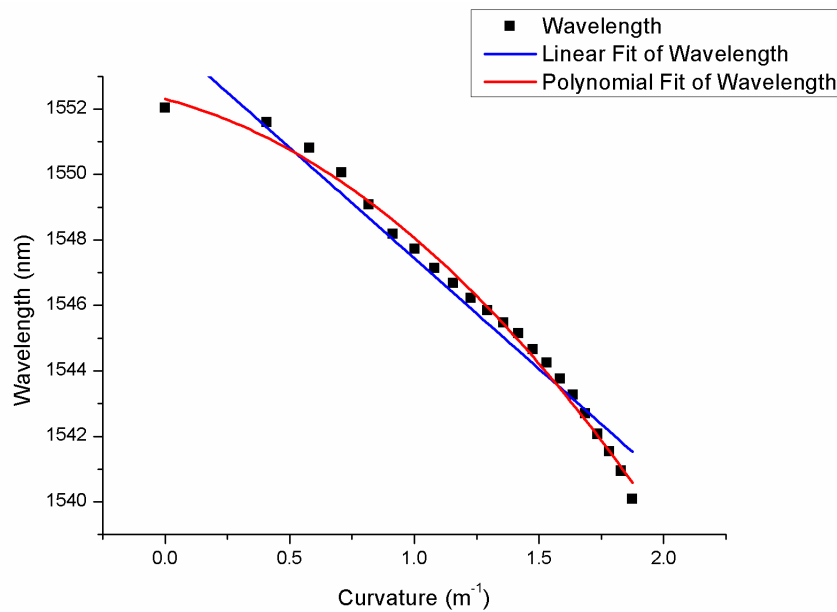


Figure 4. Wavelength shift versus curvature of Dip2.

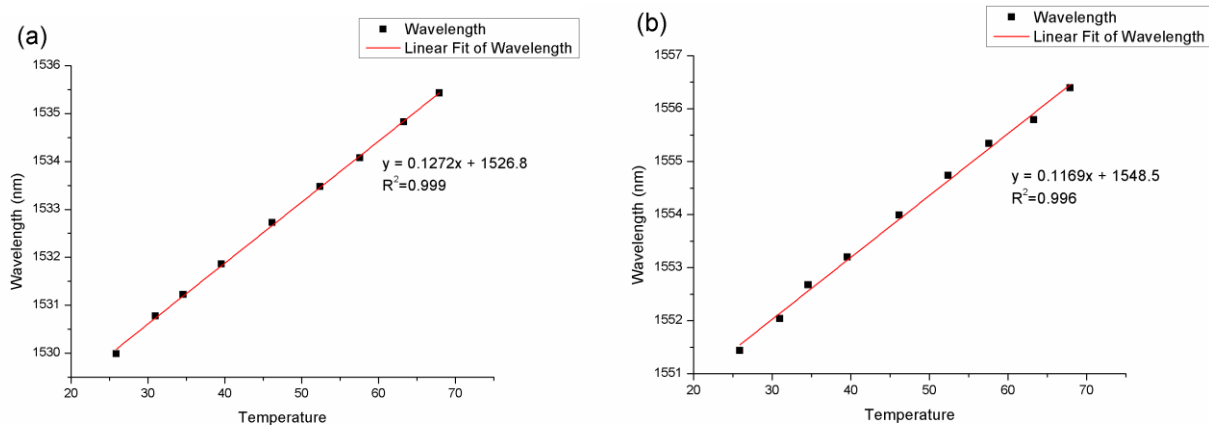


Figure 5. Temperature dependency of the SMF-FMF-SMF structure for Dip1(a) and Dip2(b).

#### 4. CONCLUSION

In conclusion, a simple SMF-FMF-SMF with up-taper fusion is investigated and the curvature can be monitored from  $0 \text{ m}^{-1} \sim 1.87 \text{ m}^{-1}$  with high  $R^2$  exceeding 0.99. The proposed sensor's temperature sensitivity can reach up to  $127.2 \text{ pm}/^\circ\text{C}$ .

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