Magnesium-Based Hydrogen Storage Compounds: A Review

Liuzhang Ouyang, a, b \* Fen Liu, Hui Wang, Jiangwen Liu, Xu-Sheng Yang, c, d \*

Lixian Sun, e \* and Min Zhua

<sup>a</sup> School of Materials Science and Engineering and Key Laboratory of Advanced Energy

Storage Materials of Guangdong Province, South China University of Technology, Guangzhou,

510641, China

<sup>b</sup> China-Australia Joint Laboratory for Energy & Environmental Materials, Key Laboratory of

Fuel Cell Technology of Guangdong Province, Guangzhou, Guangzhou, 510641, China

<sup>c</sup> Advanced Manufacturing Technology Research Centre, Department of Industrial and Systems

Engineering, The Hong Kong Polytechnic University, Hung Hom, Kowloon, Hong Kong

<sup>d</sup> Hong Kong Polytechnic University Shenzhen Research Institute, Shenzhen 518057, China

<sup>e</sup> Guangxi Key Laboratory of Information Materials, Guangxi Collaborative Innovation Center

of Structure and Property for New Energy, Materials and School of Materials Science and

Engineering, Guilin University of Electronic Technology, Guilin, 541004, China

\* Corresponding Author:

Liuzhang Ouyang: E-mail: meouyang@scut.edu.cn; Tel: +86 20 87111317

Xu-Sheng Yang: E-mail: xsyang@polyu.edu.hk; Tel: +852-27666604

Lixian Sun: E-mail: sunlx@guet.edu.cn)

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Abstract: One of the key points to boost the application of fuel cells is the progress in the development of hydrogen storage alloys with appealing high capacity. Of the numerous candidate alloys for storing hydrogen, magnesium (Mg)-based alloys have been progressively attracting great attention owing to their abundance, low densities, and considerable capacities of hydrogen storage. Nevertheless, the practical applications of Mg-based hydrogen storage alloys are still seriously hampered by their sluggish kinetics and relative stable thermodynamic characteristics. At present, some strategies have been utilizing to tune the hydrogen storage properties of Mg-based alloys, but they are still insufficient to fulfill the requirements for practical industrial applications. In this review, advanced synthetic approaches and some effective strategies including alloying, nanostructuring, doping by catalytic additives and forming nanocomposites with other hydrides, etc., to enhance the requirements properties of Mg-based hydrogen storage alloys are summarized, and then the prospects for further promoting the properties of Mg-based hydrogen storage materials are also briefly discussed.

**Keywords:** Metal hydride; Mg-based hydrogen storage alloys; thermodynamics; alloying; nanostructuring; forming nanocomposites

#### 1. Introduction

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Future energy requests urgently desire substitutes for the present energy technologies that are relied chiefly on fossil fuels.[1] Hydrogen is a promising and broadly expected selection as an alternative energy feedstock.[2-4] The primary technical components of the hydrogen energy system cover the production, supply, storage, conversion, and employment of hydrogen, among which the storage and conversion of hydrogen are consistently the keys to the effective utilization of hydrogen energy. The conventional hydrogen storage approach mostly uses cylinders to store hydrogen, which has the drawbacks of inferior efficiency, excessive pressure hindrance, and leakage prevention. Owing to their high storage densities by human concern, hydrogen storage materials have been developed into one of the crucial functional materials in materials science exploration. Hydrogen storage material, as an extraordinarily significant applied material, plays a unique part in the field of secondary energy, exceptionally in the area of fuel cells and secondary batteries. Additionally, researches regarding the hydrogen storage material can be not only directly united with the application of electric vehicles, but also with the submarine, spacecraft and other fields with considerable impacts.[5] In recent several decades, enormous endeavors have been carried out to push the hydrogen storage alloys to achieve the desire for fairly competent solid-state hydrogen storage, which will be indispensable for the prospective hydrogen economy. The current metallic hydrogen storage materials<sup>3,19</sup> can be generally divided into several categories, such as rare earth systems (e.g., LaNi<sub>5</sub>), titanium- (e.g., FeTi), zirconium- (e.g., ZrMn), and magnesium (Mg) -based alloys (e.g., Mg2Ni), etc. The hydrogen density of some representative hydrogen storage alloys is summarized in Figure 1.[6] Of the primary hydrogen storage alloys progressed formerly, Mg and Mgbased hydrogen storage materials are believed to provide the remarkable possibility of the practical application, on account of the advantages as following: 1) the resource of Mg is plentiful and economical. Mg element exists abundantly and accounts for ~2.35 % of the earth's crust with the rank of the eighth; 2) low density of merely 1.74 g·cm<sup>-3</sup>; 3) superior hydrogen storage capacity. The theoretical hydrogen storage amounts of the pure Mg is 7.6 wt. % (weight percent),[7-9] and the Mg<sub>2</sub>Ni is 3.6 wt.%, respectively.

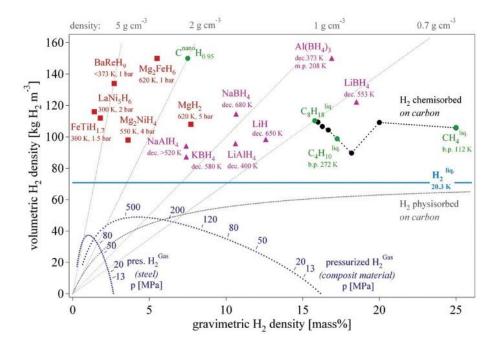


Fig. 1. Gravimetric and volumetric hydrogen density of some representative metallic hydrogen storage materials. Reproduced by permission from Züttel *et al.*, Mater. Today 6, 24 (2003). Mater. Today 6, 24 (2003). Copyright 2003 by Elsevier.

Mg-based hydrogen storage materials can be generally fell into three categories, i.e., pure Mg, Mg-based alloys, and Mg-based composites. Particularly, more than 300 sorts of Mg-based hydrogen storage alloys have been receiving extensive attention,[10] because of the relatively better overall performance. Nonetheless, the inferior hydrogen absorption/desorption kinetics rooting in the overly undue thermodynamic stability of

metal hydride make the Mg-based hydrogen storage alloys currently not appropriate for the real applications, and therefore, massive attempts have been dedicated to overcoming these shortages. Some sample preparation methods, such as smelting, powder sintering, diffusion, mechanical alloying, hydriding combustion synthesis method, surface treatment, and heat treatment, etc., have been broadly employed for altering the dynamic performance and cycle life of Mg-based hydrogen storage alloys. intrinsic modification Besides, some strategies, including alloying,[11-14] nanostructuring,[15-20] doping by catalytic additives,[21] and acquiring nanocomposites with other hydrides,[22-29] etc., have been mainly explored for intrinsically boosting the performance of Mg-based hydrogen storage alloys. Albeit considerable breakthrough has been attained, further endeavors are desired to enhance the properties of these materials. In this review paper, after briefly introducing the basic information of Mg-based

In this review paper, after briefly introducing the basic information of Mg-based hydrogen storage alloys in this Section 1. Then, the classification of Mg-based hydrogen storage alloys will be summarized in Section 2; the main approaches to modifying the properties of Mg-based alloys will be discussed in Section 3 and finally the conclusive statements, observations, and the research prospects of the Mg-based hydrogen storage materials will be provided in Section 4.

## 2. Mg-based alloys classification

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Though the hydrogen storage capacity of pure Mg is comparatively outstanding, the discontentedly high desorption hydrogen temperature and sluggish kinetics gravely block its practical applications.[2, 7, 21, 30-33] Diverse metals, counting rare earth (RE) (e.g. Ce, La), non-transition (e.g. Al, Li, In) and transition metals (e.g. Ni, Co, Fe, Cu, Ag, Sc, Y), etc., have been adopted to form Mg-based alloys for years, in which the relatively less stable hydride MgH<sub>2</sub> can be alloyed with Mg, so as to undermine the

thermodynamic stability of its hydride. The strategy, comparable to that applied to AB<sub>5</sub> (such as LaNi<sub>5</sub>), AB<sub>2</sub> (such as ZrMn<sub>2</sub>), and AB (such as FeTi) hydrides, where the A element has a larger affinity for hydrogen than the B element, has been found to be the appropriate alloying mix of Mg and a non-stable hydride to adequately reduce the strength of Mg-H bond. Three categorizations of Mg-based alloys, i.e., intermetallic compounds, solid-solution compounds and other compounds, are discussed in the following three sub-sections.

#### 2.1 Intermetallic compounds

The hydrogen storage material for realizing hydrogen as a fuel in mobile appliances has to meet stringent requirements, such as the hydrogen capacity, the stability of hydride, the hydrogen exchange rates, economy, and safety. In particular, the reversibility of the reactions between hydrogen and metals, alloys or intermetallic compounds would also highly affect their practical applications. As for the Mg-based hydrogen storage intermetallic compounds, some of them can reversibly absorb hydrogen and the original starting material can be regenerated. However, the reaction pathway of some other Mg-based hydrogen storage intermetallic compounds with hydrogen is usually irreversible and often complex. Therefore, the Mg-based hydrogen storage intermetallic compounds are summarized into three categories in this section, according to their hydrogenation/dehydrogenation routes.

## 2.1.1 Reversible Mg-based hydrogen storage alloys

Two representative reversible Mg-based hydrogen storage intermetallic compounds, which can absorb hydrogen and release hydrogen reversibly, are Mg-Ni alloys and Mg-Fe alloys. In this section, we will mainly introduce these two types of alloys and focus on the effects of the addition of the other elements on the enhancement of their

hydrogen storage properties, including thermodynamic and kinetic properties.

# (1) Mg-Ni alloys

An acclaimed of representative Mg-based compounds is Mg<sub>2</sub>Ni, which generates Mg<sub>2</sub>NiH<sub>4</sub> hydride during hydrogenation. It owns a low enthalpy of hydrogen desorption (ΔH = 64.5 kJ (mol<sup>-1</sup> H<sub>2</sub>)). The Mg-based hydrogen storage materials were first investigated at Brookhaven National Laboratory, where Reilly and Wiswall prepared Mg<sub>2</sub>Ni in an induction furnace under argon and introduced the reaction of hydrogen with Mg-Ni alloys at elevated temperatures and pressures.[34] It turned out that Mg<sub>2</sub>Ni alloy can react readily with hydrogen, forming Mg<sub>2</sub>NiH<sub>4</sub> at 300 °C under 2 MPa, with a storage capacity of 3.6 wt.%. Besides, the specific study of the hydrogen storage properties and mechanisms of Mg<sub>2</sub>Ni found that: 1) The pressure-compositional temperature (PCT) curve of Mg<sub>2</sub>Ni alloy was flat with a small lag, as shown in Figure 2; 2) Ni played a key catalytic role in making Mg easier to absorb and release hydrogen. Nonetheless, the hydrogen release temperature and powder resistance stability of Mg<sub>2</sub>Ni alloy is still needed to be further improved.

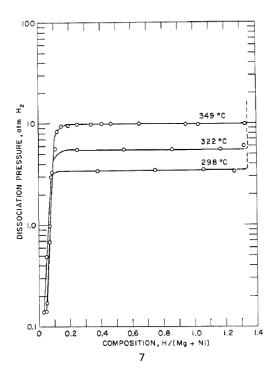


Fig. 2. Desorption isotherms for the Mg<sub>2</sub>Ni-H system. The initial alloy composition is 45.9 wt.% Mg and 54.6 wt.% Ni. Reproduced by permission from Reilly *et al.*, Inorg. Chem. 7, 2254 (1968). Copyright 1968 by ACS publications.

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The addition of the third element, namely M, to Mg<sub>2</sub>Ni has been extensively employed to enhance the hydrogen storage properties of Mg<sub>2</sub>Ni, either further reduce the temperature or boost the kinetic properties of hydrogen absorption and release processes. The added M elements include copper (Cu), zinc (Zn), palladium (Pd), chromium (Cr), manganese (Mn), cobalt (Co), Ni, Mg, zirconium (Zr), vanadium (V) and RE elements, etc.[35] In general, the M component in the Mg<sub>2</sub>Ni-M alloy takes up a relatively small proportion, normally less than 15 wt.%, and it can partially replace Ni or Mg. For example, amorphous and nanocrystalline Mg-Ni-RE alloys (RE = Y, Ce, La, Mm) formed by prompt solidification have seized the attention of researchers considering the improved hydrogenation characteristics.[36-39] However, it was reported that the maximum hydrogen storage capacity of the amorphous or nanocrystalline Mg-Ni-RE alloys was less than 5 wt.%, derived from the great number of Ni and RE and the comparatively large grain size of 100-150 nm. Accordingly, it is raring to redesign the composition together with the production approach of alloys. Yao and his colleagues [40, 41] raised Mg-based nanocomposites, possessing 4.7 nm grain size on average, and fine-grained Mg<sub>2</sub>Ni nanoparticles holding the size of ~2.7 nm via mechanical milling the amorphous Mg-10Ni-5Y along with the advanced nanocarbon supported metallic catalyst. As a result, this nanocomposite system exhibits ultrafast hydrogenation kinetics and acquires a summit hydrogen storage capacity of 6 wt.%. To dual tune the thermodynamic and kinetic properties of Mg<sub>2</sub>Ni, Ouyang et al. [42] prepared Mg<sub>2</sub>NiIn<sub>0.1</sub> solid solution via two steps, particularly sintering of the elemental improve its dehydrogenation kinetics as well as markedly diminish its thermodynamic stability, by which the dehydrogenation activation energy ( $E_a$ ) and enthalpy change ( $\Delta H$ ) decreases from 80 kJ mol<sup>-1</sup> and 64.5 kJ (mol<sup>-1</sup> H<sub>2</sub>) to 28.9 kJ mol<sup>-1</sup> and 38.4 kJ (mol<sup>-1</sup> H<sub>2</sub>), respectively. The attained consequences indicate a way to tune thermodynamic along with kinetic properties of hydrogen storage materials.

In addition to Mg<sub>2</sub>Ni alloy, Mg can form another type of intermetallic compound with Ni, viz. MgNi<sub>2</sub>, which barely reacts with hydrogen despite heating to 623 K in its regular polycrystalline phase status.[34, 43] However, nanostructured MgNi<sub>2</sub> formed via ball milling has been proved to be able to interact easily with hydrogen, even at ambient temperature, reaching 0.5 wt.% hydrogen (corresponding to MgNi<sub>2</sub>H<sub>0.7</sub>). This result demonstrated a feasibility method of optimizing the hydriding property of a MgNi<sub>2</sub>-based system by nanostructuring.

### (2) Mg-Fe alloys

The hydride Mg<sub>2</sub>FeH<sub>6</sub> can be produced upon reacting with hydrogen (according to the reaction Eq. (1)) despite the lacking miscibility of Mg and Fe.[44]

$$2Mg + Fe + 3H_2 \rightleftharpoons Mg_2FeH_6 \tag{1}$$

In particular, Mg<sub>2</sub>FeH<sub>6</sub> is promising as a hydride on account of its outstanding volumetric and gravimetric hydrogen storage capacities, reaching 150 kg/m<sup>3</sup> and 5.5 wt.%, respectively. In particular, Mg<sub>2</sub>FeH<sub>6</sub> possesses an extremely high hydrogen concentration per unit volume (9.1×10<sup>19</sup> atoms<sup>-1</sup>), which exceeds the figure of MgH<sub>2</sub> (6.5×10<sup>19</sup> atoms<sup>-1</sup>) by around 40%.[45] Whereas in terms of the theoretical stability, M<sub>2</sub>FeH<sub>6</sub> holds the relatively high enthalpy of dissociation (98 kJ (mol<sup>-1</sup> H<sub>2</sub>)), which is a drawback for the real energy storage applications. Besides, the disproportionation occurs during the desorption process, where Mg<sub>2</sub>FeH<sub>6</sub> decomposes into Mg and Fe

accompanied by the release of hydrogen. The release of hydrogen was reported to be declined apparently after four successive cycles. Notably, Batalovic [46] demonstrated that the addition of transition metal (Ni, Co, and Mn) attained a modification of the hydrogen sorption properties of Mg<sub>2</sub>FeH<sub>6</sub>. The maximum reduction in desorption enthalpy of 27.7 kJ (mol<sup>-1</sup> H) was achieved in the case of Ni doping. Similar to the Mg-Fe system, Mg<sub>2</sub>CoH<sub>5</sub> (hydrogen storage capacity, 4.5 wt.%) formed as long as mechanical mixing elemental Mg and Co under a hydrogen atmosphere, of which the hydride synthesis enthalpy is -82 kJ (mol<sup>-1</sup> H<sub>2</sub>), dehydrogenation temperature is ~513 K under 1 bar hydrogen pressure.[47] Specifically, the production of Mg<sub>2</sub>FeH<sub>6</sub> comprises two stages where MgH<sub>2</sub> regularly adopted as a precursor. More specifically, MgH<sub>2</sub> is first formed after a certain period of the ball-milling process, and then it further reacts with Fe to produce Mg<sub>2</sub>FeH<sub>6</sub> as prolonging the milling time. Mg<sub>2</sub>FeH<sub>6</sub>, however inversely produces metal and hydrogen in one-step way, supported by the in-situ hydrogen desorption curve (Figure 3) observed throughout the formation of Mg<sub>2</sub>TM (TM = Fe and Co) hydrides based on the reaction equation (Eq. (2));[48]Meanwhile, a novel absorption stage was noticed with regard to Ni.[49]

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$$2Mg+TM+\frac{x}{2}H_2 \rightarrow 2MgH_2+TM+\frac{x-4}{2}H_2 \rightarrow Mg_2TMH_x$$
172 (For Fe, Co,  $x = 6, 5$ ) (2)

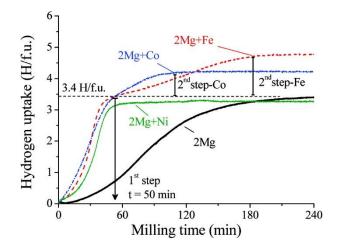


Fig. 3. Absorbed hydrogen atoms by formula unit of the formed hydride during RBM of Mg and  $Mg^{+2}TM$  mixtures (TM = Ni, Fe, and Co) (The number of absorbed H atoms per unit metal or alloy formula (H/ f.u.)). Reproduced by permission from Zhang *et al.*, J. Phys. Chem. C 115, 4971 (2011). Copyright 2011 by ACS publications.

## 2.1.2 Mg-based hydrogen alloys with one-step disproportionation reaction

The hydrogen involving the reaction process is complex in some Mg-based hydrogen storage alloys. For example, it has been found that a disproportionation reaction, i.e., MgB+H→MgH<sub>2</sub>+B, might be caused during the hydriding of these alloys. Notably, MgH<sub>2</sub> hydride is so stable that the onset of this reaction is undesirable, because it makes the hydrogen desorption reaction very difficult. According to the reaction pathway, we will mainly introduce two representative Mg-based hydrogen alloys with one-step disproportionation reaction in this section (i.e., Mg-RE alloys and Mg-transition metal systems). Then, three another typical Mg-based hydrogen alloys with multi-step disproportionation reaction (i.e., Mg-Ba, Mg-Ca, and Mg-Ga alloys) will be reviewed in section 2.1.3.

### (1) Mg-RE alloys

Since the 1970s, Mg-based hydrogen storage alloys without adding Ni but covering

almost all other metallic elements and a few nonmetallic elements, have been widely studied. In this case, Mg-based alloys can be formed from Mg and more than two non-Ni elements. Besides, since the 1980s, Mg and lanthanide RE alloys (e.g., REMg<sub>12</sub>, REMg<sub>17</sub> and RE<sub>3</sub>Mg<sub>41</sub>) have also been studied extensively because Mg and lanthanide RE metals can form the relatively stable alloy. However, Mg-RE alloys are proved impractically to apply due to the high hydrogen absorption/desorption temperature albeit the noticeable hydrogen storage capacity of those compounds. Taking La<sub>2</sub>Mg<sub>17</sub> as an example, which holds a storage capacity of around 6 wt.%, it can only absorb hydrogen at nearly 350 °C.[50] Moreover, La<sub>2</sub>Mg<sub>17</sub> transforms into LaH<sub>3</sub> and MgH<sub>2</sub> upon the hydriding process, where the LaH<sub>3</sub> is irreversibly bound.

Notably, a Mg<sub>3</sub>RE type compound (Mg<sub>3</sub>La) with a D03 type structure (BiF<sub>3</sub> type, space group Fm3m) was thereafter reported. Mg<sub>3</sub>LaH<sub>9</sub> hydride, owning an unrecognized crystal structure so far and a hydrogen storage capacity of 4.1 wt.% in theory, was formed under extremely high pressure (5 GPa).[51] Accordingly, Ouyang et al.[52] initially reported the hydrogen storage properties of D03 structured Mg<sub>3</sub>La alloy that was prepared by induction melting. It was found that the Mg<sub>3</sub>La alloy can react easily with hydrogen for the formation of metallic hydride at ambient temperature and under 1 atm pressure, possessing a reversible hydrogen storage capacity of about 2.89 wt.%. However, the release of hydrogen from the Mg<sub>3</sub>La hydride arises at a rather high temperature, denoting the lowest temperature as high as 274 °C. In addition, many types of Mg<sub>3</sub>RE compounds with the D03 structures can be synthesized by induction melting. The maximum reversible hydrogen absorption capacities of various Mg<sub>3</sub>RE, e.g., Mg<sub>3</sub>La,[52] Mg<sub>3</sub>Pr,[53] Mg<sub>3</sub>Nd,[54, 55] and Mg<sub>3</sub>Mm[56, 57] alloys are 2.89 wt.%, 2.58 wt.%, 1.95 wt.% and 2.91 wt.%, respectively, according to their PCI curves. The D03 structured Mg<sub>3</sub>RE compounds transform into FCC structured phases after the

hydrogenation processes. All the hydriding of these alloys are occurred at ambient temperature together with speedy hydrogenation/dehydrogenation kinetic properties. The nanometer-sized REH*x* phase has been found to be *in situ* formed upon activation, showing a beneficial catalytic effect on accelerating the kinetics. Further increased kinetics were obtained via mixing transition metals, especially Ni and Co, with Mg<sub>3</sub>RE.[34, 56-58] For example, it has been proved that Mg-RE-Ni alloy performs well during the hydriding process, which is attributed to the thermodynamic modification of the addition Ni.[34, 59, 60] Besides, the synthesis of fine REH<sub>x</sub> precipitates by adding the RE elements can catalyze the hydrogen desorption of MgH<sub>2</sub>.[52, 53, 55, 61]

# (2) Mg-transition metal systems

*Mg-Cu alloys*: Mg acquires two types of intermetallic compounds upon alloying with Cu, viz. Mg<sub>2</sub>Cu and MgCu<sub>2</sub>,[62] of which Mg<sub>2</sub>Cu alloy can easily react with hydrogen at 300°C under 2.15 MPa hydrogen pressure. While MgCu<sub>2</sub> barely absorbs hydrogen although heating to 350°C under 2.35 MPa hydrogen pressure.[63] Meanwhile, Mg<sub>2</sub>Cu can also reversibly undergo hydrogenation by forming two products via disproportionation (Eq. (3)), which is different from Mg<sub>2</sub>Ni by forming a single hydride (Mg<sub>2</sub>NiH<sub>4</sub>).[63]

$$Mg_{2}Cu + H_{2} \longrightarrow MgH_{2} + MgCu_{2}$$
 (3)

The hydrogenation temperature of  $Mg_2Cu$  alloy can be reduced to about 240 °C under 1 bar hydrogen pressure. Unfortunately, this reaction becomes irreversible. Such a reaction displays modified thermodynamics ( $\Delta H_d = 70 \text{ kJ (mol}^{-1} \text{ H}_2$ )) as well.  $MgH_2$  may interact with  $MgCu_2$  and generate  $Mg_2Cu$ . Thus, the modified or substituted  $Mg_2Cu$  alloys can be achieved. Additionally, it has been proved that the Mg-Cu-H nanoparticle system possesses modified thermodynamics: the hydrogenation enthalpy

and entropy are improved to be -67.5 kJ ( $\text{mol}^{-1}$  H<sub>2</sub>) and -124.4 J ( $\text{K}^{-1}$   $\text{mol}^{-1}$  H<sub>2</sub>), respectively.[64]

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When the concentration of Mg in the alloy exceeds the normal composition corresponding to Mg<sub>2</sub>Cu, the PCI curve of this Mg-Mg<sub>2</sub>Cu alloy exhibits two plateaus and enhanced hydrogen storage properties, which closely resembles the Mg-Mg2Ni system.[34] For example, the alloy consisting of 90.5 wt.% Mg together with 9.5 wt.% Cu can react quickly with hydrogen at a temperature lower than 300°C under pressure of 3 MPa, achieving an exceptional hydrogen storage content over 6.62 wt.%. Accordingly, the upper plateau is attributed to the interaction of hydrogen and intermetallic compound, i.e., Mg<sub>2</sub>Cu with hydrogen.[63] Besides, it's worth noting that the existing Mg<sub>2</sub>Cu in two-phase Mg-Mg<sub>2</sub>Cu alloy catalyzes the reaction between hydrogen and Mg, in comparison with the higher hydrogenation pressure and temperature of single-phase Mg alone.[65, 66] This has also been confirmed by thermodynamics and surface research. As shown in Figure 4, they concluded that the outside Mg surface exposes to oxygen and forms an oxide layer, conversely, the interface between Mg and Mg<sub>2</sub>Cu is out of touch with oxygen leading to a lack of barrier. Therefore, it was assumed in their models that in contrast to that of Mg, the external surface of Mg<sub>2</sub>Cu retains its capability to liberate hydrogen which is released to the underlying Mg afterward. Hence, it was proposed that hydrogen tends to hinder Cu from reacting with oxygen but not impeding Mg.[45] Furthermore, the decomposition of MgH<sub>2</sub> in two-phase Mg-Mg<sub>2</sub>Cu alloy with the existence of Mg<sub>2</sub>Cu is fairly quick, especially at the larger H/Mg ratios, where the equilibrium dissociation pressures can be achieved even at 275°C.

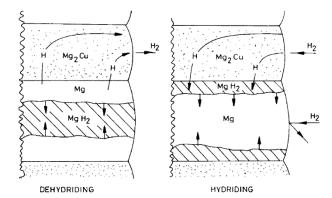


Fig. 4. Hydriding and dehydriding model of Mg<sub>2</sub>Cu catalyzed Mg. Reproduced by permission from Selvam *et al.*, Int. J. Hydrogen Energy 11, 169 (1986). Copyright 1986 by Elsevier.

*Mg-Ag alloys*: Douglass[67] has investigated the reaction behaviors between hydrogen and Mg-Ag alloys with Ag concentration ranging between 1-5 at.%. The noticeable points of the hydrogenation and dehydrogenation behaviors of Mg-transition metal alloys are listed in Table 1. These data indicate the effects of Ag on the dehydrogenation process in comparison with the remarkable systems, like Mg-Ni and Mg-Cu. Besides, it is interesting to note that the hydrogen storage properties of Mg<sub>3</sub>Ag have also been investigated.[68, 69] Similar to Mg-Cu alloys, the reversible Mg<sub>3</sub>Ag-H<sub>2</sub> system undergoes the hydrogenation via the reaction in Eq. (4), which possesses a lower ΔH<sub>d</sub> value (69.8 kJ/mol H<sub>2</sub>).[70]

$$Mg_3Ag + 2H_2 \rightleftharpoons 2MgH_2 + MgAg \tag{4}$$

The results in Table 1 obviously display that mixing Mg with other metals generates Mg-based alloys that can effectively enhance hydrogenation and dehydrogenation thermodynamics. In addition, the effect of the solid solution on the hydrogen storage properties of Mg-based compounds has been studied. For example, Si *et al.*[71] fabricated the Mg<sub>5.7</sub>In<sub>0.3</sub>Ag alloy by casting, founding that this alloy formed by mixing

Mg(In) solid solution and Mg<sub>3</sub>Ag compound with the following reactions (Eq. (5-6)):

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$$Mg(In)+Mg_3Ag+2H_2 \rightleftharpoons 2MgH_2+(Mg, In)Ag$$
 (5)

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$$2MgH_2 + (Mg, In)Ag \rightleftharpoons (Mg, In)_3Ag + 2H_2$$
 (6)

This study confirmed that the (Mg, In) $_3$ Ag-H $_2$  system can alter the thermodynamics ( $\Delta H_d = 62.6 \text{ kJ} \text{ (mol}^{-1} \text{ H}_2)$ ), which was attributed to the dual destabilization by adding Ag as well as the dissolution of In. Particularly, the solid solution of In introduces the catalytic effect to enhance the hydrogen desorption from additional MgH $_2$ . As indicated by decreased activation energy (78.2 kJ mol $^{-1}$ ), Mg $_{5.7}$ In $_{0.3}$ Ag showed the faster hydrogen desorption kinetics than that of the Mg $_6$ Ag sample.

Table 1. Hydrogen absorption and desorption behavior of various Mg-transition metal alloys.

Alloy	Hydrogen	Hydriding conditions		Hydrogen	Dehydi	driding	
composition	content	Pr.	Temp.	released	Pr.	Temp.	
(atomic%)	(wt.%)	(atm)	(°C)	(wt.%)	(atm)	(°C)	
Mg <sub>2</sub> Ni	3.6	25	350	_	_		
Mg-Mg <sub>2</sub> Ni	5.7	25	350	_	_	_	
Mg <sub>2</sub> Cu	2.7	30	300	_	_	_	
Mg-Mg <sub>2</sub> Cu	6.6	30	300	_	_	_	
$\mathrm{Mg_2Fe}^*$	5.4	20-120	450-520	_	_	_	
$Mg-Mg_{17}Y_{13}$	5.0	10	400-450	4.5	3.0	320	
Mg-1Y	4.5	56	400	4.0	1.0	300	
Mg-5Y	7.0	56	400	3.4	1.0	300	
Mg-5Mn	6.0	56	400	1.5	1.0	300	
Mg-5Co	2.0	56	400	0.0	1.0	300	
Mg-1Ag	5.7	56	400	2.0	1.0	300	
Mg-5Ag	5.3	56	400	0.0	1.0	300	
Mg-1Ag-1Y	6.0	56	400	_	_	_	

Mg-1Ag-1Y	6.3	56	400	_	_	_
Mg-5Ni-5Y	5.2	56	400	3.1	1.0	300
Mg-5Al-5Y	5.0	56	400	3.1	1.0	300
Mg-10Al-10Y	4.1	43	400	_	1.6	310
Mg-34Al-10Y	3.6	43	400	_	2.2	310
					1.0	286
Mg-10Cu-5Ni-	3.7	21	400	_	2.0	310
					1.5	299
$Mg_{80}Ag_{15}Al_5$	1.7				2.2	300
$Mg_{85}Ag_5Al_{10}$	3.8				2.6	300
$Mg_{90}Ag_{7.5}Zn_{2.5}$	4.2				2.8	300
$Mg_{78}Ag_{16.5}Zn_{5.5}$	2.5				2.8	300

Besides, Mg-Ag-Me ternary alloys have also been investigated. For example, Lu *et al.* fabricated Mg-Ag-Al[72], Mg<sub>80</sub>Ag<sub>15</sub>Al<sub>5</sub> and Mg-Ag-Zn [73] alloys and revealed that their reaction routes differ from that in pure Mg. An intermediate phase, comprising a new ternary solid solution MgAg(Al), was found to react with MgH<sub>2</sub> during the dehydrogenation process, thus leading to an rise in the hydrogen desorption equilibrium pressure (0.22 MPa at 300 °C) with a reversible hydrogen storage capacity of 1.7 wt.%. The compositional adjusted Mg<sub>85</sub>Ag<sub>5</sub>Al<sub>10</sub> can possess a reversible hydrogen storage capacity of about 3.8 wt.% and an increased equilibrium pressure (0.26 MPa at 300 °C). In addition, a large fraction of phase boundaries were found to be existed in the hydrogenated Mg-Ag-Zn alloys, which were prepared by ball milling MgH<sub>2</sub> with Ag(Zn) solid solution, contributing to more hydrogen diffusion channels.

## 2.1.3 Mg-based hydrogen alloys with multi-step disproportionation reaction

Different from Mg-based hydrogen alloys with one-step disproportionation reaction, Mg-based hydrogen alloys with multi-step disproportionation reaction, such as Mg-Ba alloys, Mg-Ca alloys, and Mg-Ga alloys, means this type of materials contains more than one hydrogen desorption processes for forming the hydrides.

### (1) Mg-Ba alloys

Ab initio calculations were adopted by Bhihi and collaborators[74] which predicted that modifying MgH<sub>2</sub> with a small quantity of alkaline metals (Sr, Ba) could reduce remarkably the stability of MgH<sub>2</sub>. Mg-Ba system comprises various types of alloys (e.g., Mg<sub>17</sub>Ba<sub>2</sub>, Mg<sub>23</sub>Ba<sub>6</sub>, and Mg<sub>2</sub>Ba).[75] Wu *et al.*[76] investigated the hydrogen storage properties and phase transition mechanisms of Mg<sub>17</sub>Ba<sub>2</sub> alloy via induction melting. The reversible hydrogen storage content of Mg<sub>17</sub>Ba<sub>2</sub> alloy is about 4.0 wt.%. The PCI curves of Mg<sub>17</sub>Ba<sub>2</sub> are displayed in Figure 5 and the dehydrogenation pathway with three steps can be expressed in Eq. (7-9) as follows:

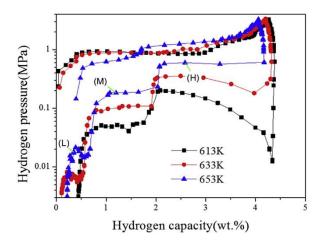


Fig. 5. PCI curves of Mg<sub>17</sub>Ba<sub>2</sub> compound measured at different temperatures. Three points (H), (M), and (L) are indicated in the PCI curves. Reproduced by permission from Wu *et al.*, J. Alloys Compd. 690, 519 (2017). Copyright 2017 by Elsevier.

High platform: 
$$MgH_2 \rightarrow Mg+H_2$$
 (7)

324 Medium platform:

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$$Ba_2Mg_7H_{18} \rightarrow Ba_6Mg_7H_{26} + H_2$$
 (8)

326 Low platform:

The hydrogen desorption activation energy of Mg<sub>17</sub>Ba<sub>2</sub> was verified to be 173.92 kJ/mol. Moreover, the dehydriding thermodynamics data of Mg<sub>17</sub>Ba<sub>2</sub> at different platforms are listed in Table 2.

Table 2. Dehydrogenation enthalpy and entropy change of Mg<sub>17</sub>Ba<sub>2</sub> compound at different platforms. Reproduced by permission from Wu *et al.*, J. Alloys Compd. 690, 519 (2017). Copyright 2017 by Elsevier.

Temperature	ΔΗ	ΔS
(K)	$(kJ (mol^{-1} H_2))$	$(J (K^{-1}mol^{-1} H_2))$
High platform	88.9	150.9
Medium platform	107.9	170.3
Low platform	165.8	240.9

# (2) Mg-Ca alloys

Chiotti et al [77] proved that CaMg<sub>2</sub> could interact with hydrogen and then convert to CaH<sub>2</sub> and elemental Mg at 450 °C. Meanwhile, the hydrogen storage capacity of CaMg<sub>2</sub> alloy is hopeful to exceed 6.3 wt.%, with the H/M ratio of 2. Adding Ni to Mgbased alloys is widely applied to catalyze hydrogen on the Mg surface when the hydrogenation process moves forward. Then several CaMg<sub>2</sub>-based alloys associated with Ni have been found to show outstanding hydrogen storage capacities. For example, Lupu *et al.*[78] found that CaMg<sub>1.8</sub>Ni<sub>0.5</sub> alloy possesses 5.7 wt.% hydrogen storage capacity at 338 °C with rapid hydriding kinetics. Terashita *et al.*[79] reported that (Ca<sub>0.8</sub>La<sub>0.2</sub>)Mg<sub>2.2</sub>Ni<sub>0.1</sub> alloy could absorb 5.1 wt.% hydrogen even at ambient temperature. To improve the hydrogen capacity and reduce costs of CaMg<sub>2</sub>-based alloys,

Ma *et al.*[80] designed a CaMg<sub>1.9</sub>Ni<sub>0.1</sub> alloy by adding a small quantity of Ni through induction melting. The experimental results showed that the addition of Ni enables the CaMg<sub>1.9</sub>Ni<sub>0.1</sub> alloy to have a room-temperature absorption of hydrogen under mild hydrogen pressure, reaching the hydrogen storage content of 5.65 wt.% and distinct activation energy of 41.74 kJ/mol.

## (3) Mg-Ga alloys

There are a lot of intermetallic compounds included in the Mg-Ga alloy system (e.g., Mg<sub>5</sub>Ga<sub>2</sub>, Mg<sub>2</sub>Ga, and MgGa). The solid solubility of Ga in Mg-Ga alloy system reaches 5 wt.% at temperature of 573 K,[81] and a Mg(Ga) solid solution can be generated during the hydriding/dehydriding process of Mg-Ga alloy. For instance, Wu *et al.*[82] prepared the solid solution expressed as Mg(Ga) at a rather high temperature and found that the Mg(Ga) solid solution creates reversible hydrogen-absorbing capacity (5.7 wt.%) for Mg-Ga alloy. The (de)hydrogenation process of intermetallic compounds, such as the Mg<sub>5</sub>Ga<sub>2</sub> compound, was found to be reversible with the reaction expressed as Eq. (10):

$$Mg_5Ga_2 + H_2 \rightleftharpoons 2Mg_2Ga + MgH_2$$
 (10)

While the hydrogen desorption process of the Mg-Ga hydrides consists of two steps: the first one is the combination of Mg<sub>2</sub>Ga with MgH<sub>2</sub> to produce Mg<sub>5</sub>Ga<sub>2</sub> and liberate H<sub>2</sub> simultaneously; the second step involves the transformation of MgH<sub>2</sub> to Mg and H<sub>2</sub>. Especially, the reaction occurred in the first step improves the whole dehydriding process and decreases the dehydriding enthalpy. The dehydriding enthalpy and activation energy of the Mg-Ga alloy are proved to be 68.7 kJ/mol H<sub>2</sub> and 149 kJ/mol, respectively. When comparing to the pure Mg enthalpy (77.1 kJ/mol H<sub>2</sub>), it is obvious noted that Mg-Ga alloy has improved the dehydrogenation thermodynamic properties.

#### 2.2 Solid solutions

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Generally, alloying to form the intermetallic compounds is an achievable method to improve the thermodynamic properties of Mg-base hydrogen storage alloys. But there are some weaknesses yet, such as the decrease in the hydrogen capacity due to the heavy alloying metallic elements and the poor reversibility resulted from the broken bonds between Mg and other metallic elements during the hydriding reaction. Besides, most of the intermetallic compounds, such as Mg-Fe, Mg-Co, and Mg (In, Cd), possess the higher ΔH for the dehydriding process than that of Mg/MgH<sub>2</sub>. Hence, further study should be carried out to solve these remaining problems. Alternatively, constructing an Mg-based solid-solution alloy is believed to be a destabilization strategy, which can slightly modulate the structure and composition of Mg at the expense of moderate capacity, thus likely adjusting the thermodynamic stability. Especially, Cd is the exclusive element expressing unlimited solid-state solubility in Mg. In this regard, Douglass et al.[67] firstly covered the Mg-1 at.% Cd solid solution, which presents a 5 wt.% hydrogen storage content at 673 K in 24 h. Besides, Schulz[83] comprehensively studied the hydriding kinetic and thermodynamic properties of Mg-x at.% Cd (x = 5, 10, and 20) alloys, which are extremely difficult to activate for the hydrogen absorption even after annealing at temperature of 523 K for 24 h under 1.5 MPa hydrogen pressure. Interestingly, Skripnyuk et al. [84] synthesized Mg<sub>3</sub>Cd alloys via high-energy mechanical milling, which displays a reversible hydrogen storage content of 2.8 wt.% along with a 2.5 wt.% hydrogen storage capacity at the temperature of 573 K in 120 s. Fortunately, there is no measurable pressure hysteresis detected from the PCT curve of Mg<sub>3</sub>Cd shown in Figure 6 with a hydrogenation enthalpy of -65.5 kJ mol<sup>-1</sup>.

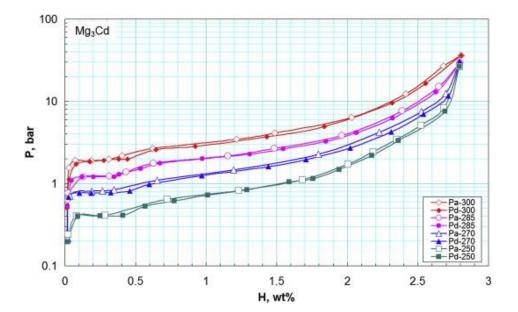


Fig. 6. PCT curves of the studied Mg<sub>3</sub>Cd alloy at temperature ranging 250-300 °C. The open and filled symbols correspond to the absorption and desorption branches of the curves, respectively. Reproduced by permission from Skripnyuk *et al.*, Int. J. Hydrogen Energy 37, 10724 (2012). Copyright 2012 by Elsevier.

On the basis of the binary phase diagram belonging to the Mg-In system, it could also possess a considerable solubility up to 10 at.% within a wide range of temperatures.[45, 85, 86] The reversible formation of Mg (In) solid solution supplies an effective strategy to modulate the dehydrogenation thermodynamic properties of MgH<sub>2</sub>. The Mg (In) solid-solution alloys absorb hydrogen and generate MgH<sub>2</sub> together with disordered Mg-In compounds. The corresponding lattice constants, as well as hydrogen storage capacities of Mg (In) solid-solution, are summarized in Table 3. The Mg<sub>0.95</sub>In<sub>0.05</sub> solid-solution alloy can reversibly react with hydrogen at temperature of 573 K according to the following equation (Eq. (11)):

$$Mg_{0.95}In_{0.05} + 0.9H_2 \rightleftharpoons 0.9MgH_2 + 0.05MgIn$$
 (11)

The hydrogen storage content of Mg<sub>0.95</sub>In<sub>0.05</sub> is up to 5.3 wt.%, while it owns sluggish

kinetic property in the hydrogenation/dehydrogenation process.[87] Accordingly, Zhu et al.[88] added some other elements to synthesize ternary Mg-based solid-solution alloys, involving Mg (In, Al), Mg (In, Cd) and Mg (In, Y) alloys. Mg (In, Al) ternary solid solution indicates the modified dehydriding reversibility as well as a significant reduction of  $\Delta H$  when comparing to the binary Mg (Al) solid solution, owing to the dissociation of Al in the  $\beta$  phase.

In terms of the Mg-In-Y ternary system, a reversible solubility of Y in Mg could be obtained upon decomposing the  $In_3Y$  phase during dehydrogenation, while the reversible dissolving of Y is relatively deficient attributing to the production of  $YH_2$ . The  $Mg_{90}In_5Y_5$  alloys exhibit a reduced hydriding enthalpy of 62.9 kJ (mol<sup>-1</sup>  $H_2$ ), which is decreased by 5 kJ (mol<sup>-1</sup>  $H_2$ ) and 12 kJ (mol<sup>-1</sup>  $H_2$ ) when comparing to the figures of the  $Mg_{95}In_5$  binary solid solution alloys and pure Mg, respectively.[89] The hydrogenation process of the  $Mg_{90}In_5Cd_5$  alloy resembles the Mg-In-Y system, which can be expressed as the following equation (Eq. (12)):

$$Mg_{90}In_5Cd_5+70H_2 \rightleftharpoons 70MgH_2+5MgIn+5Mg_3Cd$$
 (12)

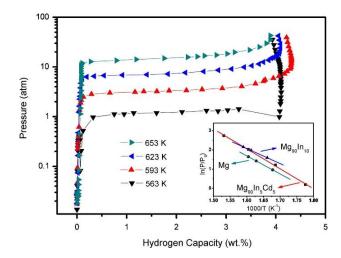


Fig. 7. PCT and Van't Hoff plot (the inset) for the hydrogen desorption of the Mg<sub>90</sub>In<sub>5</sub>Cd<sub>5</sub> alloy. Reproduced by permission from Lu *et al.*, J. Alloys Compd. 645,

Table 3. Lattice constants of Mg-based solid solutions and their hydrogen storage properties. Reproduced by permission from Zhang *et al.*, RSC Adv. 9, 408 (2019).

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0.11.1.1.1	Lattice constants (nm)		$ \Delta H $	ΔS	Capacity
Solid solution	a	С	(kJ (mol <sup>-1</sup> H <sub>2</sub> ))	(J (K <sup>-1</sup> mol <sup>-1</sup> H <sub>2</sub> ))	(wt.%)
$Mg_{0.9}In_{0.1}$	0.31929	0.52061	65.2	121.8	4.2
$Mg_{0.95}In_{0.05}$	0.32027	0.52086	68.1	125.5	5.3
$Mg_{0.98}In_{0.02}$	0.32077	0.52106	69.6	126.0	6.4
$Mg_{0.75}Al_{0.25}$	0.31990	0.51960	76.8	138.6	5.0
$Mg_{0.9}In_{0.05}Al_{0.05}$	0.31980	0.51929	66.3	121.2	4.8
Mg90In5Cd5	0.31925	0.51964	86	154.8	4.3

The dehydrogenation enthalpy ( $\Delta H$ ) and entropy ( $\Delta S$ ) of the Mg<sub>90</sub>In<sub>5</sub>Cd<sub>5</sub> alloy are 86.0 kJ (mol<sup>-1</sup> H<sub>2</sub>) and 154.8 J (K<sup>-1</sup> mol<sup>-1</sup> H<sub>2</sub>), respectively. The PCT curves indicate a reversible hydrogen storage content of 4.3 wt.% as well as a raised equilibrium pressure of MgH<sub>2</sub> in Mg<sub>90</sub>In<sub>5</sub>Cd<sub>5</sub> alloy compared with that of pure MgH<sub>2</sub> (Figure 7). The Mg<sub>90</sub>In<sub>5</sub>Cd<sub>5</sub> alloy exhibits an improved hydriding kinetic property and a reduced hydriding activation energy of 61.0 kJ mol<sup>-1</sup> as well, while the hydrogen desorbing rate is tardy as a result of the long-range diffusion of In and Cd in MgH<sub>2</sub>.[90]

## 2.3 Other compounds

MgH<sub>2</sub> generating from ball milling proceeds a serious growth in crystallite size or subsequent structural relaxation of defects upon the very first hydrogen cycle, which slowly shrinks the benefit of nanocrystallization. Therefore, it urgently desires an

appropriate approach to preserve nanoparticles from aggregation or recrystallization. It has been found that pure Mg embedded in 2D or 3D material could prevent the growth of nanoparticles. In this regard, Mg nanoparticles limited in carbon aerogels (CA) have appealed to much attention.[91-93] For example, Liu et al.[92] reported that Mg nanoparticles conned in carbon aerogels via the hydriding process of infiltrated dibutyl-Mg followed by hydrogen release at 623 K, which has a size in the range of 5.0 to 20.0 nm. The hydrogenation and dehydrogenation enthalpies of the confined Mg were determined to be  $65.1\pm1.56$  kJ (mol<sup>-1</sup> H<sub>2</sub>) and  $68.8\pm1.03$  kJ (mol<sup>-1</sup> H<sub>2</sub>), respectively. Jia et al. [94] synthesized the MgH<sub>2</sub>@CMK-3 nanoconfinement system and experimentally accomplished the low-temperature hydrogenation starting from 323 K. Comparing with the calculated reaction energy (E<sub>r</sub>) from clusters of pure MgH<sub>2</sub> and MgH<sub>2</sub>/C (Figure 8), they deduced that the interfacial effect can effectively increase the low-temperature dehydriding properties of MgH<sub>2</sub> clusters, even though the cluster is not ultra-small (Figure 8c). Accordingly, they presented a novel mechanism for destabilizing Mg-H bonding through the mix of the size effect and MgH<sub>2</sub>-carbon scaffold interfacial bonding, which is more superior to nanoparticles or 2D films. The use of scaffolds impedes the particle enlargement and agglomeration, but it leads to a critical capacity loss. Hence, altered forms of stabilization should be searched to increase the storage capacity, while presenting adequate stabilization for nanosized Mg without scaffolds, such as the appending of modified graphene nanoribbons, the introduction of a second phase, reserving additional hydrogen and core-shell methods, should be conducted.

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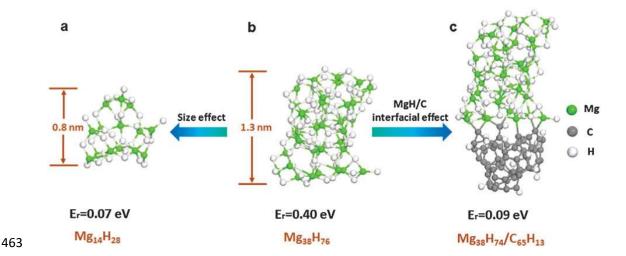


Fig. 8. Reaction energy (Er) for hydrogen release from clusters of pure MgH<sub>2</sub> and MgH<sub>2</sub>/C. (a) Pure Mg<sub>14</sub>H<sub>28</sub> cluster; (b) Mg<sub>38</sub>H<sub>76</sub> cluster; (c) Mg<sub>38</sub>H<sub>74</sub> adsorbed on the cluster of amorphous carbon. Mg, C and H atoms are indicated by green, grey and white spheres, respectively. Reproduced by permission from Jia *et al.*, Phys. Chem. Chem. Phys. 15, 5814 (2013). Copyright 2013 by RSC.

In addition, Mg-based glasses or nanoglasses is also a new system that attracts extensive attention. For instance, Lin *et al.*[95] found that the Mg-Ce-Ni metallic glasses (MGs) can reversibly absorb and desorb about 0.2-0.4 wt.% H at room temperature without pre-activation, and the hydrogenation capacity of the glassy Mg-based alloy is twice as that of the corresponding crystalline alloy due to its free volume and disordered atomic structure. Recently, Lin *et al.*[96] continued to investigate the hydrogenation kinetics of two five-component Mg<sub>60</sub>Ce<sub>10</sub>Ni<sub>20</sub>Cu<sub>5</sub>X<sub>5</sub> (X = Co, Zn) metallic glasses under a hydrogen atmosphere. This work demonstrated that alloying with Zn leads to the negligible impact on the hydrogenation kinetics and storage capacity of the Mg-Ce-Ni-Cu metallic glass. However, alloying with Co can remarkably improve the hydrogenation kinetics and storage capacities. Apparent activation energies for the hydrogenation were calculated to be 64.4 kJ/mol, and 107.2

kJ/mol, respectively, for the  $Mg_{60}Ce_{10}Ni_{20}Cu_5Co_5$  and  $Mg_{60}Ce_{10}Ni_{20}Cu_5Zn_5$  metallic glasses.

# 3. Approaches to modifying the properties of Mg-based alloys

Mg-based alloys, considered as a potential candidate for hydrogen storage, possess a rather high dehydriding temperature and sluggish kinetic properties of their hydride MgH<sub>2</sub>, which blocks their practical applications. In this section, some particular effective approaches to modifying the kinetics and thermodynamics of Mg-based hydrogen storage alloys will be reviewed.

## 3.1 Kinetic modifying

In the past few decades, significant progress has been made in improving the hydrogenation/dehydrogenation kinetics of Mg-based alloys by nanostructuring, synthesizing metastable phases, doping catalytic additives and changing the reaction path. However, the tuning of their kinetic properties is still a great challenge. Herein, we present a summary of the recent advances and developments in enhancing the kinetics of Mg and Mg-based alloys.

### 3.1.1 Nanostructuring

It has been found that raising the densities of various defects, including grain/interphase boundary, dislocations, and stacking faults, etc., via nanostructuring is favorable to the hydrogenation/dehydrogenation kinetics of hydrogen storage alloys, without increasing cost and slightly reducing hydrogen storage capacity.[23, 97-100] On the other hand, the introduction of extra boundary/surface might also reduce the reaction enthalpy of Mg-H systems. Therefore, nanostructuring can be an effective strategy to dually tune the thermodynamics and kinetics of Mg-based hydrogen storage materials. For example, in the process of ball milling, one typical method for

nanostructuring, the impact of high-speed balls on the sample introduces the severe plastic deformation, which subsequently results in the structural defects, increased stress and increased free energy of the uniform-composition sample system. More importantly, the decreased particle size of the sample during nanostructuring will lead to the shortening of the required length of hydrogen diffusion path, increasing of the specific surface area and nucleating sites of the metal hydrogenation reaction, which are all beneficial to the boosting of hydrogenation and dehydrogenation kinetics of Mg-based alloys.[101, 102]

Nanostructuring has been most systematically investigated regarding the Mg<sub>2</sub>Ni alloy among the Mg-based hydrogen storage alloys.[103, 104] For example, Mg<sub>2</sub>Ni can be protected by hydrogen from ball milling, during which hydrogen reacts with Mg<sub>2</sub>Ni alloy, denoting the hydrogen reserves of 1.6 wt.%. The ball-milled sample has a good hydrogen absorption performance, with a hydrogen absorption temperature of 140 °C, and a reduced hydrogen release temperature of 250 °C. Besides, Song *et al.*[105] prepared Mg<sub>2</sub>Ni alloy samples by means of mechanical ball grinding, melting and sintering, which could release hydrogen at 270 °C.

Particularly, Zhang and his coworkers[19] presented an innovative strategy, namely microencapsulated nanoconfinement, for the synthesis of a structure where the monodispersed Mg<sub>2</sub>NiH<sub>4</sub> nanoparticles are anchored onto the graphene layer surface by the method of hydriding chemical vapor deposition (HCVD), as schematically displayed in Figure 9. The as-formed material holds greater stability in structure and an excellent dehydriding kinetic rate. In addition, the MgO coating layer with a thickness of around 3 nm effectually divorces the nanoparticles from accumulating with each other during hydrogenation/dehydrogenation cycles, bringing elevated thermal and mechanical stability. Furthermore, the MgO layer displays exceptional gas-selective

permeability to hinder the further oxidation of Mg<sub>2</sub>NiH<sub>4</sub> and available for the hydrogenation/dehydrogenation process as well. Consequently, extraordinarily low activation energy (31.2 kJ mol<sup>-1</sup>) for the hydrogen release reaction is acquired.

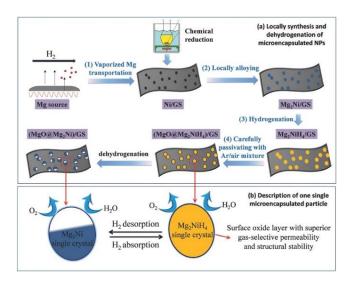


Fig. 9. Schematic of (a) the local synthesis of monodispersed Mg<sub>2</sub>NiH<sub>4</sub> nanoparticles locally derived from Ni/GS by HCVD and the structural evaluation after hydrogen desorption. Reproduced by permission from Zhang *et al.*, Adv. Mater. 29, 1700760 (2017). Copyright 2017 by Wiley.

The mechanical alloying-induced nanostructuring can not only make powder particles more evenly distributed, but also refine grains, thus improving hydrogen storage kinetic performance. Therefore, nanostructuring of Mg-based alloys proposes a promising route to modify their kinetics meanwhile without an obvious decline in their hydrogen capacities. The formation of a nanocrystalline structure and associated defects through mechanical milling is often perceived as leading to enhanced hydrogen kinetics. Similarly to the case of surfaces discussed above, grain boundaries between nanocrystals contain excess energy, resulting in surface energy, thus providing another potential tool for reducing the reaction enthalpy of metal hydrides. In fact, the presence

of distinct types of lattice defects (grain boundaries, dislocations, stacking faults, and possible amorphization in some regions) that may likely act as either heterogeneous nucleation sites or diffusion pathways for hydrogen to be drawn away from the growing fronts and improve the hydrogen sorption characteristics subsequently.

The hydrogen release mechanism of bulk Mg<sub>2</sub>NiH<sub>4</sub> with crystal defects and cracks was found that the hydride/metal transform from Mg<sub>2</sub>NiH<sub>4</sub> to Mg<sub>2</sub>NiH<sub>x</sub>. As for the case of Mg<sub>2</sub>NiH<sub>x</sub>, Tran et al.[106] found a high density of various stacking faults in the dehydrided material (Figure 10). Note that similar results have also been reported in various alloy systems regarding the formation of defects in subsequent hydriding/dehydriding cycles. For instance, hexagonal closed-pack structured systems such as LaNi<sub>5</sub>[107] and FeTi[108, 109], have also been reported to possess the various defects, including vacancies, dislocations stacking faults, and a network of dislocations or deformation twins locating ahead of the Mg/MgH<sub>2</sub> interface.[110, 111] These defects-induced misfits are considered necessary to maintain the lattice coherency at the hydride/metal interphase and dissipate the accumulated elastic strain during the phase transformation. Specifically, stacking faults is greatly favorable for subsequent hydriding/dehydriding cycles, and it is therefore purposely introduced by severe deformation methods to facilitate the activation of hydrogen storage materials.[112] A variety of studies[113-118] also suggested that the formation of lattice defects such as grain boundaries, which can act as pathways for transportation of hydrogen through the oxide layer, can activate the material and then promote the kinetics of the hydrogen storage alloys.

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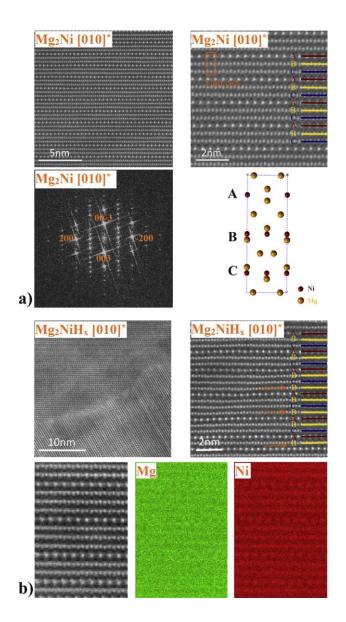


Fig. 10. a) Atomic-resolution images of the perfect unreacted  $Mg_2Ni$  lattice projected along [010] zone axis and the corresponding atomic model, b) Atomic-resolution images of the adjacent dehydrided  $Mg_2NiH_x$  ( $x\sim0$ -0.3) regions (along [010] zone axis), showing a high probability of stacking faults (as indicated by the arrows) along with an EDS map. Reproduced by permission from Tran *et al.*, J. Power Sources 341, 130 (2017). Copyright 2017 by Elsevier.

## 3.1.2 Synthesizing metastable phases

The strategy of synthesizing metastable phases has been proved to modify the

kinetics of Mg-based hydrogen storage alloys. Specifically, the addition of early TMs (TM = Ti, Zr, Hf, V, Nb, and Ta) is helpful to stabilize the structure. A series of metastable Mg-rich Mg<sub>6~7</sub>TMH<sub>12~16</sub> hydrides with CaF<sub>2</sub> related structure, have been synthesized, [119, 120] which can desorb 4.7 wt.% of hydrogen at 330 °C but decomposes into Mg and TiH<sub>2</sub>, but still require extremely high hydrogen pressure in the rehydrogenation process. Calizzi *et al.*[121] prepared Mg-Ti nanostructured samples containing a metastable Mg-Ti-H fcc phase, finding that the mean crystallite sizes of Mg and  $\beta$ -MgH<sub>2</sub> are both decreased with the increase in Ti content (Figure 11). Their results only showed the enhanced kinetic properties in the Mg-Ti system. Another research showed that the hydriding enthalpy of Mg-Fe-based materials with a crystallite size of 10 nm can be decreased by 6 kJ (mol<sup>-1</sup> H<sub>2</sub>) between 523 K and 673 K.[122]

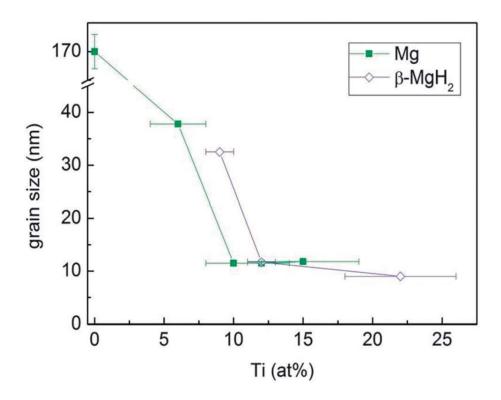


Fig. 11. Mean crystallite size of the Mg and  $\beta$ -MgH<sub>2</sub> phases in the Mg-Ti and Mg-Ti-H samples as a function of Ti content. Reproduced by permission from Calizzi *et al.*, Phys. Chem. Chem. Phys. 18, 141 (2016). Copyright 2016 by RSC.

The metastable nanostructured Mg-based alloys formed by the mechanical alloying approach might effectively solve the sluggish kinetics issue, as widely investigated by Shao and his coworkers.[59, 60] A considerable quantity of defects along with plastic deformation during mechanical alloying processes might result in the phase transitions in the synthesized Mg-based metastable nanostructured alloys, e.g., forming the BCC crystal structures with the characteristic performance of preserving the initial lattice structure during hydrogenation and dehydrogenation processes. Particularly, a summary of different Mg-based metastable nanostructured alloys with BCC lattice structure has been conducted by Shao,[123] especially the Mg-Co based metastable nanostructured alloys with BCC crystal structures. For example, Shao *et al.*[9, 124] reported Mg<sub>50</sub>Co<sub>50</sub> and Mg<sub>55</sub>Co<sub>45</sub> metastable BCC alloys with hydrogen storage values of 2.67-3.24 wt.% at 258 K, which is the lowest hydrogenation temperature for Mg-based materials described in the literature. Notably, Mg-Co BCC alloys possess a theoretical hydrogen storage content up to 20 wt.% in terms of geometrical calculation, albeit it is impossible to completely obtain up to date.

More specifically, Shao and his coworkers [125] explored the phase and morphology evolutions of ball-milled metastable nanostructured Mg-based Mg<sub>50</sub>Co<sub>50</sub> hydrogen storage alloys with various milling durations as well. Co was found to be dispersed on the surface of Mg particles upon the start of milling, which is gradually cracked into a smaller size. After milling for 25 h, the FCC Co phase is synthesized, then the Co particles are dissolved into Mg particles. As the milling time prolongs to 50 h, the Mg particle size is markedly minished and the structure shifts to the BCC phase after 45 h. After 100 h milling, only one single BCC phase can be characterized, as shown in Figure 12. Moreover, differential scanning calorimetry (DSC) curves of both 50 h-, and 100 h-milled Mg<sub>50</sub>Co<sub>50</sub> alloys showed two clear exothermic peaks,

which move to higher temperatures as milling time increasing due to the less amount of remaining catalytic Co phase. A widen exothermic peak including two overlapped peaks were observed in the 300 h-milled sample, which may be resulted from the welding on the particle surface during further milling, leading to fewer defects and less surface area on the surface. In terms of hydrogen storage properties, it was proved that the 100 h-milled Mg50Co50 alloy can react with more hydrogen at 258 K than that at a higher temperature of 323 K, as shown in Figure 13. The hydrogenation process detected by PCT measurements was thermodynamically dominant. The 50 h-milled Mg50Co50 alloy presented superior kinetics and hydriding capacity than that of 100 h-milled Mg50Co50 alloy, owing to the catalytic effect of remained Co in the 50 h-milled sample.

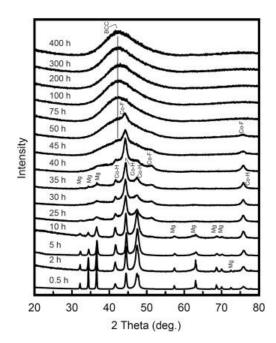


Fig. 12. XRD patterns of Mg<sub>50</sub>Co<sub>50</sub> alloys ball milled for various periods. Reproduced by permission from Shao *et al.*, Int. J. Hydrogen Energy 38, 7070 (2013). Copyright 2013 by Elsevier.

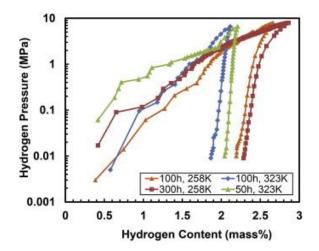


Fig. 13. PCT curves at 258 K and 323 K of the Mg<sub>50</sub>Co<sub>50</sub> alloys milled for different durations (50 h, 100 h, and 300 h). Reproduced by permission from Shao *et al.*, Int. J. Hydrogen Energy 38, 7070 (2013). Copyright 2013 by Elsevier.

## 3.1.3 Doping catalytic additives

Doping catalytic additives has demonstrated as the most promising strategy to improve the reaction kinetics of Mg-H in Mg-based systems. This is mainly because the addition of catalysts can effectively reduce the reaction energy barrier, thus accelerating the hydrogen absorption/desorption rate of Mg-H systems. Several catalysts were employed such as transition metals,[126-130] metal oxides,[5, 7, 33, 131] intermetallic compounds that absorb hydrogen in milder conditions,[25, 132] and carbon materials.[133, 134]

In addition to metallic elements (discussed in section 2), some transition metal oxides, i.e., Nb<sub>2</sub>O<sub>5</sub>, TiO<sub>2</sub>, V<sub>2</sub>O<sub>5</sub>, Cr<sub>2</sub>O<sub>3</sub>, Mn<sub>2</sub>O<sub>3</sub>, Fe<sub>3</sub>O<sub>4</sub>, CuO and SiC[33, 131] can also be added to elevate the hydrogenation and dehydrogenation performance of Mg-based alloys. For example, Nb<sub>2</sub>O<sub>5</sub> proved to have more obvious enhancement in kinetics[135-

144] in comparison with other oxides. The hydrogen desorption/absorption kinetics below 5 min at 300 °C could be obtained with Nb or Nb<sub>2</sub>O<sub>5</sub> addition.[144-146] Bhat *et al.*[143] reported that nanocrystalline Nb<sub>2</sub>O<sub>5</sub> with high specific surface area induce the fastest kinetics than commonly used Nb<sub>2</sub>O<sub>5</sub> (Figure 14). A further improvement in the sorption properties of Nb<sub>2</sub>O<sub>5</sub> doped MgH<sub>2</sub> was found when a small amount of Cr<sub>2</sub>O<sub>3</sub> was added (Figure 15) by Patah *et al.*[135] They reported a drastic reduction in the activation energy of Cr<sub>2</sub>O<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub> doped MgH<sub>2</sub> up to 136 kJ·mol<sup>-1</sup> in comparison with 197 kJ·mol<sup>-1</sup> and 206 kJ·mol<sup>-1</sup> for 1 mol% doped MgH<sub>2</sub> and pure MgH<sub>2</sub> respectively. Although the explanation for the action of these catalysts is still not clear, it is suggested that these catalysts are responsible for modification of Mg surface on mechanochemical treatment destruction of MgO layer, the formation of active nucleation centers and partial reduction of the oxides to form metal clusters (V, Nb).[147]

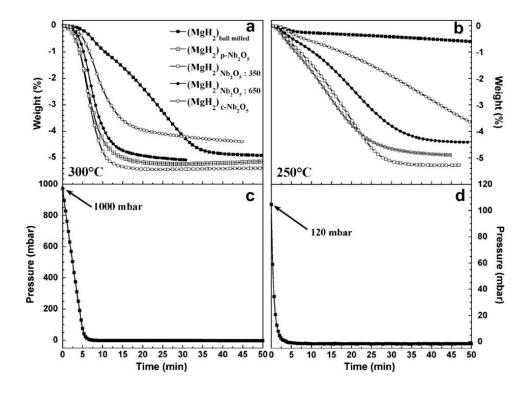


Fig. 14. Hydrogen desorption kinetics of (MgH<sub>2</sub>)<sub>bm</sub> and selected (MgH<sub>2</sub>)<sub>catalyst</sub> at (a) 300 °C and (b) 250 °C, and their corresponding pressure (c) and (d) during desorption, respectively. Reproduced by permission from Bhat *et al.*, J. Alloys Compd. 460, 507 (2008). Copyright 2008 by Elsevier.

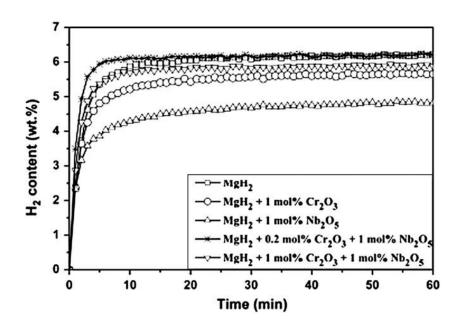


Fig. 15. The amount of the hydrogen absorbed as a function of reaction time at 300 °C under 1 MPa H<sub>2</sub>. Reproduced by permission from Patah *et al.*, Int. J. Hydrogen Energy 34, 3032 (2009). Copyright 2009 by Elsevier.

Wang *et al.*[148] synthesized Mg-Ni-MnO<sub>2</sub> by mechanical alloying and indicated that the hydrogenation of the alloy reaches 6.2 wt.% within 50 s at 200 °C under pressure of 2.0 MPa. The deposit-taking 6.2 wt.% hydrogen can be released in full within 400 s. Zou and his collaborators[149] prepared the Mg-TM-La (TM = Ti, Fe, Ni) ternary composites by arc plasma evaporation. The detailed investigation[150] of the hydrogen storage properties of the as-formed composites presented a remarkable modification in the hydrogenation kinetics as well as a decrease of hydrogen release

temperature, which is ascribed to the catalytic effect of Mg<sub>2</sub>Ni and La<sub>2</sub>O<sub>3</sub>.

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In addition, the addition of new catalyst SiC has been reported to improve the hydrogenation properties of MgH<sub>2</sub> by Ranjbar et al. [136], e.g., the improved hydrogen absorption/desorption kinetics and increased capacity of MgH<sub>2</sub> caused by increasing the surface area and defect concentration. An additional improvement was achieved by adding catalyst Ni to the MgH2/SiC composite. Halides can also enhance the hydrogenation and dehydrogenation performance of Mg-based alloys.[1, 150, 151] For example, Ismail et al.[152] used 10 wt.% LaCl<sub>3</sub> to ball mill with Mg hydride. They proved that introducing LaCl<sub>3</sub> to the alloys can decrease the dehydrogenation temperature by 50 °C and minimize the activation energy of hydrogen release by 23 kJ/mol, respectively, when comparing to the as-milled pure Mg hydride. The hydrogenation capacities of the doped and pure Mg hydride are respectively 5.1 wt.% and 3.8 wt.% within 2 mins at temperature of 300 °C. Meanwhile, 4.2 wt.% hydrogen can desorb from doped Mg hydride, but only 0.2 wt.% from the pure Mg hydride. Clearly, doping LaCl<sub>3</sub> can boost the kinetics owing to the catalytic effect of the La-Mg alloy and the MgCl<sub>2</sub> produced at the heating process. This study indicates that halide can encourage the refinement of metal powder of Mg-Ni alloy in the ball milling process, and effectually modulate the metal surface by destroying the oxidation layer on the metal surface, so as to promote the hydrogenation and dehydrogenation reaction of the alloy, which is particularly prominent in the first hydrogen absorption of the alloy.

Table 4. Hydrogenation properties for Mg-based alloys doping catalytic additives

Material	Temperature	Pressure	Kinetics	Max.	Ref.
	(°C)	conditions	(min)	Hydrogen	
		(bar)		(wt.%)	
MgH <sub>2</sub> -17 wt.% Nb <sub>2</sub> O <sub>5</sub>	T <sub>abs</sub> : 274	P <sub>abs</sub> : 10	t <sub>abs</sub> : 2	7.0	
	T <sub>des</sub> : 274	P <sub>des</sub> : 0.001	t <sub>des</sub> : 3		
Mg-10 wt.% Cr <sub>2</sub> O <sub>3</sub>	T <sub>abs</sub> : 300	P <sub>abs</sub> : 10	t <sub>abs</sub> : 3	6.0	
	T <sub>des</sub> : 300	P <sub>des</sub> : 1	t <sub>des</sub> : 5		
MgH <sub>2</sub> -1mol% La <sub>2</sub> O <sub>3</sub>	T <sub>abs</sub> : 303			6.0	
	T <sub>des</sub> : 303				
MgH <sub>2</sub> +1 mol% Cr <sub>2</sub> O <sub>3</sub> +0.2	T <sub>abs</sub> : 300		t <sub>abs</sub> : 5	6.0	
mol% Nb <sub>2</sub> O <sub>5</sub>			t <sub>des</sub> : 20		
Mg-3Ni-2MnO <sub>2</sub>	T <sub>abs</sub> : 200	P <sub>abs</sub> : 20	t <sub>abs</sub> : 50 s	6.2	[148]
	T <sub>des</sub> : 310	P <sub>des</sub> : 1	t <sub>des</sub> : 400 s		
Mg-10 wt.% LaCl <sub>3</sub>	T <sub>abs</sub> :300		t <sub>abs</sub> : 2	5.1	[152]

### 700 3.1.4 Forming nanocomposite alloys

Early in the 1990s, it has been reported that better comprehensive hydrogen storage properties of Mg-based alloys can be achieved once combining the Mg-based hydrides with other types of alloys that have excellent hydrogen kinetics. As these two components can simultaneously absorb/desorb hydrogen during the hydriding/dehydriding process, a cooperative interaction might be existed between them to improve the hydrogen storage performances as well as the thermodynamics. Thus, Mg-based hydrogen storage nanocomposite materials have been extensively investigated so as to obtain hydrogen storage content up to 5 wt.% (Mg content larger than 90 wt.%), under milder conditions.

A series of new Mg-based hydrogen storage nanocomposites have been synthesized

by the addition of LaNi<sub>5</sub>, FeTi, C and all kinds of organic compounds, such as Mg-x wt.% LaNi<sub>5</sub>, Mg-x wt.% FeTi, Mg-x wt.% CFMmNi<sub>5</sub>, Mg<sub>2</sub>Ni-x wt.% Ti<sub>2</sub>Ni, Mg-Mg<sub>2</sub>Ni<sub>0.75</sub>Fe<sub>0.25</sub>, Mg-C and tetracyanoethylene(TCNE)-Mg<sub>2</sub>Ni, phthalonitrile(PN)-Mg<sub>2</sub>Ni, naphthacene-Mg<sub>2</sub>Ni and chloranil-Mg<sub>2</sub>Ni, etc. The hydrogen storage properties of some nanocomposites are summarized in Table 5.[153, 154]

Table 5. Properties of some Mg-based nanocomposite hydrogen materials. Reproduced by permission from Broom *et al.*, Springer London (2011). Copyright 2011 by Springer-Verlag London.

	Hydrogen storage	ATT	AC
Composite	capacity	ΔΗ	$\Delta S$
	- •	$(kJ (mol^{-1} H_2))$	$(K^{-1} \text{ mol}^{-1} H_2))$
	(wt.%)		
Mg-30 wt.% CFMmNi <sub>5</sub> *	5.6(500 °C)	-29	-112.14
Mg-30 wt.% LaNi <sub>5</sub>	5.0(300 °C)	-	-
$Mg\text{-}Mg_2Ni_{0.75}Fe_{0.25}$	3.3(320 °C)	77.3(lower)	37.9
		65.2(higher)	16.2
Mg <sub>2</sub> Ni-40 wt.% Ti <sub>2</sub> Ni	165mAh·g <sup>-1</sup>	-	-
PN- Mg <sub>2</sub> Ni	-	66.4	-
(Mg-C) <sub>ChorTHF</sub>	(180 °C)	-	-
$Ml_{0.7}Mg_{0.3}Ni_{3.2}$	1.7(25 °C)		
LaCaMgNi <sub>9</sub>	1.8(20 °C)	-33.0	-120
CaTiMgNi <sub>9</sub>	1.87(20 °C)	-33.4	-121.0
LaCaMgNi <sub>6</sub> Al <sub>3</sub>	1.87(20 °C)	-30.0	-101.3
LaCaMgNi <sub>6</sub> Mn <sub>3</sub>	1.80(20 °C)	-32.3	-111.0

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In addition, Zhu and his colleagues [27, 155] prepared Mg-MmM5 (LaNi5-based alloys) nanocomposites by the mechanical alloying. Particularly, the microstructures and hydrogenation properties of ball-milled Mg-MmNi<sub>5-x</sub>M<sub>5</sub> nanocomposite systems have been studied, exhibiting the existence of nanometer-sized MmNi<sub>5-x</sub>M<sub>x</sub>-Mg and Mm<sub>2</sub>Mg<sub>17</sub> phases and the improved hydrogen absorption properties, as shown in Figure 16. Gross et al. [97] then prepared La<sub>2</sub>Mg<sub>17</sub>-LaNi<sub>5</sub> nanocomposites via ball milling as well, showing superior kinetics to the properties of pure La<sub>2</sub>Mg<sub>17</sub>. The La<sub>2</sub>Mg<sub>17</sub>-LaNi<sub>5</sub> composite comprises a complicated porous mixture of three phases: Mg2Ni (~1 µm), La (~100 nm), and Mg. During the process of hydrogenation and hydrogen release, the complex interactions between various phases, the changes in phase structures, and the synergistic effect between various phases might cooperatively to improve the kinetic performance of Mg.[156] For example, the hydrogenation and dehydrogenation kinetics of Mg in La<sub>2</sub>Mg<sub>17</sub>-LaNi<sub>5</sub> composites are actually catalytically boosted by closely contacting with Mg2Ni, while slightly influenced by the La phase. In other words, the properties of hydrogen storage materials might be effectively modulated when the heterogeneous complex system (including adding catalyst phase) is achieved.

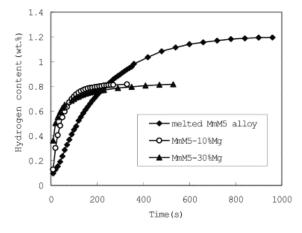


Fig. 16. Kinetic curves for melted MmM<sub>5</sub> alloy and nanophase composite of compositions MmM<sub>5</sub>-10% Mg and MmM<sub>5</sub>-30% Mg measured under isobaric conditions at 333 K. Reproduced by permission from Zhu *et al.*, J. Alloys Compd. 330-332, 708 (2002). Copyright 2012 by Elsevier.

AB<sub>3</sub>-based composites, like LaCaMgNi<sub>9</sub>, CaTiMgNi<sub>9</sub>, LaCaMgNi<sub>6</sub>Al<sub>3</sub>, and LaCaMgNi<sub>6</sub>Mn<sub>3</sub> were formed via partially substituting. Interestingly, every alloy can be easily activated at ambient temperature under 3.3 MPa hydrogen pressure and the hydrogen storage of which are 1.8 wt.% hydrogen.[28, 29] Peng and his coworkers[157] proposed a Ml<sub>0.7</sub>Mg<sub>0.3</sub>Ni<sub>3.2</sub> (Ml expresses La-rich mischmetal) hydrogen storage alloy via induction melting and proved that this alloy owns a multi-phase microstructure involving (MlMg)Ni<sub>3</sub>, (MlMg)Ni<sub>2</sub>, and MlNi<sub>5</sub> phases, reaching a summit hydrogen storage content of 1.7wt.% at ambient temperature. Besides, they reported that the grain size apparently alters the hydrogen storage content of AB<sub>3</sub>-base Ml-Mg-Ni multi-phase alloys as well. More specifically, the hydrogen storage capacity declines with grain size decreasing, which is ascribed to the inadequate hydrogen storage in the grain boundary region.[157, 158]

By reactive milling, Floriano *et al.*[21] prepared Mg-based nanocomposites involving Ti-Cr-V alloys as additives for hydrogen storage. Especially, Ti-Cr-V -based

involving Ti-Cr-V alloys as additives for hydrogen storage. Especially, Ti-Cr-V -based alloys are one of the earliest candidates for practical hydrogen storage applications, which possess the BCC solid solution structure and can absorb up to 3.7 wt.% hydrogen at ambient temperature. The doping of TiCrV and TiCr<sub>1.2</sub>V<sub>0.8</sub> alloys significantly enhances the dehydrogenation properties of Mg in their corresponding Mg-based nanocomposites, in comparison with their counterparts without additive. They also found that Mg-based nanocomposites containing an amount of 5 mol% of TiCrV can contribute to the optimum hydrogen storage properties, showing a more effective

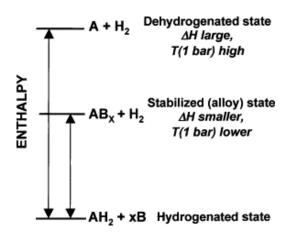
reduction in desorption temperature ( $\sim$ 240 °C) (than the composite containing TiCr<sub>1.2</sub>V<sub>0.8</sub> alloy). Furthermore, faster absorption and desorption kinetics at temperatures of 275 °C and 300 °C can be obviously observed for the Mg-based nanocomposites containing 5 mol% of TiCrV and TiCr<sub>1.2</sub>V<sub>0.8</sub> in comparison with the pure Mg.

The above reviewed experimental results suggest that, by forming the Mg-based nanocomposites, the additions can be inlaid on the surface of matrix particles (such as Mg or Mg<sub>2</sub>Ni particles) and change the microstructures and phase constitutions, which might provide more active sites and pathways for hydrogen sorption and diffusion. Generally, single-phase hydrogen storage materials hardly fulfill the requirements of practical applications. Based on the advantages of each sole-phase material, it may be possible to achieve thermodynamics and kinetics dual tuning. In this regard, the incorporation of doping catalysis and nanostructuring or destabilization to establish the Mg-based nanocomposite/multiphase systems might be an effective methodology to dually tailor the thermodynamics and kinetics of Mg-based systems.

## 3.2 Thermodynamic modifying

Compared with the thermodynamic destabilization by solid solution,[159] alloying is more effectual to improve the thermodynamics of  $MgH_2$  in Mg-based alloys. The added alloying metals (e.g., Si, Al, Ge) may combine with Mg to generate diverse stable phases, which are likely to alter the reaction pathway and decrease the dehydriding enthalpy further. Figure 17 schematically displays an accepted enthalpy diagram to exhibit how the additive destabilizes the tightly bound hydride.[160] The alloying element, B, decreases the hydrogen release enthalpy via the synthesis of  $AB_x$  and successfully undermines the stability of the hydride,  $AH_2$ . Consequently, this reaction existing with a decreased enthalpy can raise the equilibrium pressure and decrease the

### 787 dehydriding temperature.



below (Eq. (13)):[85]

Fig. 17. Generalized enthalpy diagram illustrating destabilization through alloy formation upon dehydrogenation. Including the alloying additive, B, reduces the enthalpy for dehydrogenation through the formation of  $AB_x$  and effectively destabilizes the hydride  $AH_2$ . Reproduced by permission from Vajo *et al.*, J. Alloys Compd. 446-447, 409 (2007). Copyright 2007 by Elsevier.

Alloying some typical elements, such as Si, Ge, Sn, and Al, etc., with Mg, have been widely investigated as well, aiming to alter thermodynamic stabilization properties of Mg-based alloys. For example, Vajo *et al.*[161]reported that alloying Mg with Si can decrease the enthalpy markedly by changing the pathway of the dehydrogenation reaction. Upon the hydrogen release of MgH<sub>2</sub>, Mg interacts with Si to produce a more stable compound (Mg<sub>2</sub>Si) with the decreased dehydrogenation enthalpy. The de/hydrogenation of the MgH<sub>2</sub>-Si system follows the reaction mechanism as

 $2MgH_2 + Si \rightleftharpoons Mg_2Si + 2H_2 \tag{13}$ 

Alloying Si with MgH<sub>2</sub> is predicted to effectively undermine the Mg-H bond with a decreased enthalpy of 41 kJ (mol<sup>-1</sup> H<sub>2</sub>) owing to the existence of Mg<sub>2</sub>Si.[85]

Furthermore, thermodynamic calculations indicate the release temperatures for the equilibrium pressure of 1 bar and 100 bars are approximately 293 K and 423 K, respectively. Therefore, it might suggest that the MgH<sub>2</sub>/Si system, with a 5.0 wt.% hydrogen storage content, could be applied for hydrogen storage at low temperatures. Nevertheless, there fund a difficulty in hydrogen re-absorption of Mg<sub>2</sub>Si resulted from the poor kinetic properties as well as the mass transport of Mg and Si into divided phases.[162, 163]

Gennari and his collaborators[164] discovered that the existence of Ge can reduce the hydrogen desorption temperature of Mg<sub>2</sub>Ge from 323 to 423 K, which was successfully synthesized via mechanical milling. In addition, Walker *et al.*[165] accomplished the ball-milling reaction of MgH<sub>2</sub> with Ge under Ar atmosphere to synthesize the Mg<sub>2</sub>Ge alloy (Eq. (14)).

$$2MgH_2 + Ge \rightleftharpoons Mg_2Ge + 2H_2 \tag{14}$$

Their results demonstrated that Ge can destabilize the thermodynamics of MgH<sub>2</sub>, leading to the remarkable reduction of dehydrogenation enthalpy to 14 kJ (mol<sup>-1</sup> H<sub>2</sub>) and temperature to 403 K. However, the dehydrogenation product Mg<sub>2</sub>Ge cannot reabsorb hydrogen to generate MgH<sub>2</sub> and Ge. Meanwhile, the additional Si and Ge cannot produce their hydrides in the Mg-based alloys as well. Therefore, the hydrogen storage content is partly decreased.

Some works have also shown that the addition of Sn may play a beneficial effect on the dehydrogenation properties of Mg and Mg-based alloys. For example, the Sn/MgH<sub>2</sub> nanocomposite formed by mechanical milling presents a considerably decreased dehydrogenation temperature.[164] Chen *et al.*[166] discovered the presence of a weakened Mg-H bond via partial replacement of Sn for Mg by the insight into the electron structure and charge density of MgH<sub>2</sub>,

Based on the Mg-Sn binary phase diagram,[68, 166] the equilibrium solubility of Sn in Mg can be insignificantly reduced below 573 K, meaning that it's hardly for Sn to dissolve in Mg lattice. There present two eutectic reactions containing the Mg/Mg<sub>2</sub>Sn and Mg<sub>2</sub>Sn/Sn mixtures. Recently, Urretavizcaya and Meyer found the possibility of shifting the cubic Mg<sub>2</sub>Sn to the metastable hexagonal Mg<sub>2</sub>Sn via the mechanical mixing of Mg and Sn under Ar or hydrogen atmosphere.[167] Meanwhile, Mg<sub>2</sub>Sn might catalyze the hydrogenation/dehydrogenation of Mg due to the demonstrated mechanism resembling the eutectic mixtures of Mg/Mg<sub>2</sub>Ni.[168]Besides, in the view of the good size figure of Mg and Sn atoms, the solubility of Sn in Mg could be further enlarged via ball milling. The synthesis of Mg(Sn) solid solution might elevate the hydrogen storage content owing to the lack of affinity of Sn to H than Mg.

Moreover, researchers proved that the solubility of Sn in Mg lattice is insignificant resulted from the Mg<sub>2</sub>Sn formed preferentially. While the additional Sn improves the grain refinement of Mg owing to the production of Mg<sub>2</sub>Sn. Although Mg<sub>2</sub>Sn can hardly storage hydrogen practically, the ball-milled Mg/Mg<sub>2</sub>Sn nanocomposites present hydrogenation/dehydrogenation kinetic properties along with destabilized thermodynamics as shown in Figure 18.[166]

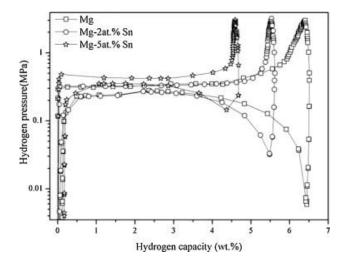


Fig. 18. PCI curves at 596K for Mg, Mg-2 at.% Sn and Mg-5at.% Sn. Reproduced by permission from Zhong *et al.*, J. Alloys Compd. 509, 4268 (2011). Copyright 2011 by Elsevier.

Zaluska and his colleagues[18] proved that combing Mg with Al might destabilize the MgH<sub>2</sub> in thermodynamics. In 1978, Douglass[67] obtained 6.3 wt.% hydrogen storage capacity by melting Mg-Al alloy. The hydrogen storage performance of some types of Mg-Al alloys with different compositions, such as Mg<sub>3</sub>Al<sub>12</sub>( $\gamma$ ), Mg<sub>17</sub>Al<sub>12</sub>( $\gamma$ ), and Mg<sub>2</sub>Al<sub>3</sub>( $\beta$ ), and the effect of adding the third element on its hydrogen storage properties are summarized in Figure 6.[45, 69] The problem is that the Mg-Al alloy will undergo disproportionation reaction at a higher temperature (348 °C) to generate MgH<sub>2</sub> and Al according to the reaction (Eq. (15-16)):

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$$Mg_2Al_3 + 2H_2 \rightleftharpoons 2MgH_2 + 3Al$$
 (15)

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$$Mg_{17}Al_{12} + 17H_2 \rightleftharpoons 17MgH_2 + 12Al$$
 (16)

The reaction rate of Mg-Al alloys, however, seems to be sluggish, thus leaving the infeasible application for this system. The theoretical hydrogen capacity of MgH<sub>2</sub>-Al is up to 4.4 wt.% and the dehydrogenation enthalpy reduces slightly by 6 kJ (mol<sup>-1</sup> H<sub>2</sub>). But the destabilization effect of this system is relatively weak (only around 50 K reduction in decomposition starting temperature).[169] Especially, the reversible hydrogen absorption was achieved through three transformation steps, from the initial reaction from only Mg to form MgH<sub>2</sub>, then the decomposition of the  $\gamma$ -Mg<sub>17</sub>Al<sub>12</sub> phase into the Mg-poor  $\beta$ -Mg<sub>2</sub>Al<sub>3</sub> phase, and the final formation of the Mg-hydride phase from the resulting Mg<sub>2</sub>Al<sub>3</sub>.[170] Besides, Mg-based ternary alloys, such as Mg-Al-Me, Mg-Al-Ti, Mg-Fe-Ti and

hydrogen sorption properties of 1.5 mm thick Mg-based films with Al, Fe, and Ti as alloying elements. These ternary alloys display remarkable sorption behavior, e.g., the films can absorb 4-6 wt.% hydrogen in seconds and desorbing in minutes at 200 °C. Meanwhile, this sorption kinetics are stable for the Mg-Al-Ti and Mg-Fe-Ti alloys, which showed no degradation in capacity even after 100 absorption/desorption cycles. For the Mg-Al-Fe alloy, the properties are clearly worse compared to the other ternary counterparts.

Table 6. Hydriding characteristics of various binary and ternary Mg-Al alloys.

Alloy composition	δΤ*	Hydrogen	Plateau pressure at 300°C
(atomic ratio)	(°C)	absorbed (wt.%)	(atm)
Mg <sub>17</sub> Al <sub>12</sub> (γ-phase)	-	3.31	-
Mg <sub>4</sub> Al <sub>5</sub> (ε-phase)	-	2.77	-
$Mg_2Al_3(\beta$ -phase)	-	3.28	-
MgAl (β+γ-phase)	-	0.38	-
$Mg_{0.62}Al_{0.38}$	19	2.30	1.4
$Mg_{0.59}Al_{0.36}Ni_{0.05}$	28	3.36	1.8
$Mg_{0.59}Al_{0.36}La_{0.05}$	31	3.04	1.9
$Mg_{0.59}Al_{0.36}Y_{0.05}$	30	2.01	2.2
$Mg_{0.56}Al_{0.34}La_{0.10}$	-	2.12	1.7
$Mg_{0.56}Al_{0.34}Y_{0.10}$	40	3.29	2.1-2.6
$Mg_{0.56}Al_{0.34}Ni_{0.05}Y_{0.05}$	-	2.58	1.5
$Mg_{0.56}Al_{0.34}Mm_{0.10}{}^{\dagger}$	-	2.15	1.8
$Mg_{0.80}Al_{0.10}Y_{0.10} \\$	65	4.08	1.7

$Mg_{0.80}Al_{0.10}La_{0.10}$	123	4.22	2.1
$Mg_{0.91}Al_{0.09}$	-	7.0	-
$Mg_{0.9}Al_{0.1}$		H/M=1.75	
$(Mg_{70}Al_{30})-99+(Nb_2O_5)-1mol.\%$		4.7(250 °C)	
$Mg_{70}Al_{15}Ti_{15}$		4.0 -	
Mg <sub>85</sub> Al <sub>7.5</sub> Ti <sub>7.5</sub>		5.4	

\* The temperature rise observed during hydriding which is found to be a good qualitative measure of hydriding kinetics. The increase in the  $\delta T$  value indicates relatively the rapidity of hydriding kinetics.

 $\dagger$  Mm = Mischemetal

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### 3.3 Kinetic and thermodynamic dual modifying

# 3.3.1 Tuning alloy composition

886 In recent works, it has been found that some specific Mg-based hydrogen storage alloys are able to realize the dual tuning effects on the thermodynamic and kinetic 887 properties. Normally, the catalytic elements/alloys should be added to these dual 888 modifying-effect Mg-based alloys for further optimization, such as most widely 889 investigated Mg (In)-based alloys. 890 For example, Zhou et al.[172] used Ti intermetallic compound to promote the 891 dehydrogenation kinetic properties of Mg(In) solid solution. They reported that the 892 destabilization in thermodynamics of Mg<sub>0.1</sub>In alloy can also possess excellent hydrogen 893 desorption kinetics, e.g., it begins to release hydrogen at about 100 °C and hydrogen 894 can be completely released at 150 °C after 3 hours,[173] simultaneously destabilizing 895 the thermodynamics and kinetics of MgH<sub>2</sub>. However, the formation of Mg(In) solid 896

solution demands the association of prolonging sintering and mechanically milling, ascribing to the greatly varied atomic radii between the soft metal In (1.93 Å) and Mg (1.73 Å),[87] which might lead to rather sluggish dehydriding kinetics of this alloys. Ouyang *et al.*[174] subsequently developed an innovative efficient approach, plasma milling, to synthesize the Mg(In)-MgF<sub>2</sub> composite that shows the enhanced dual modifying effects. The hydrogen capacity of Mg(In) solid solution in Mg(In)-MgF<sub>2</sub> composite is improved significantly up to 5.16 wt.%, as shown in Figure 20. Simultaneously, the kinetics is also boosted due to the catalysis *in situ* formed MgF<sub>2</sub>. In this connection, the *in situ* formed MgF<sub>2</sub> serves as a catalyst to accelerate the reaction rate of the following equation:

$$Mg(In) + 8H_2 \rightleftharpoons MgH_2 + \beta^{"}$$
 (17)

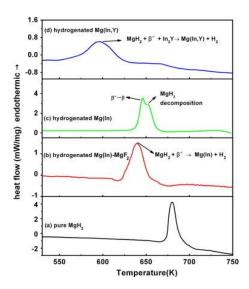


Fig. 19. DSC curves for (a) Pure MgH<sub>2</sub>, (b) hydrogenated Mg(In)-MgF<sub>2</sub> composite, (c) hydrogenated Mg(In) solid solution and (d) hydrogenated Mg(In, Y) solid solution, with a heating rate of 2 K/min. Reproduced by permission from Ouyang *et al.*, J. Alloys Compd. 586, 113 (2014).Copyright 2014 by Elsevier.

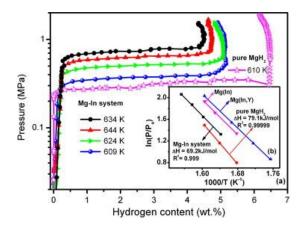


Fig. 20. (a) PCI curves for the hydrogen desorption of the Mg(In)-MgF<sub>2</sub> composite and pure MgH<sub>2</sub>, (b) Van't Hoff plots of the Mg(In)-MgF<sub>2</sub> composite, pure MgH<sub>2</sub>, Mg(In) and Mg(In, Y) solid solutions. Reproduced by permission from Ouyang *et al.*, J. Alloys Compd. 586, 113 (2014). Copyright 2014 by Elsevier.

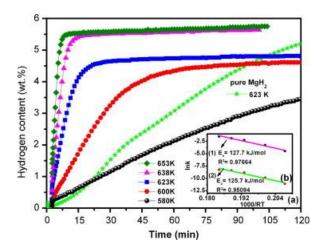


Fig. 21. (a) Dehydriding kinetic curves for the hydrogenated Mg(In)-MgF<sub>2</sub> composite, (b): (1) and (2) are the Arrhenius plots fitted by the JMAK model and the Jander diffusion model, respectively. Reproduced by permission from Ouyang *et al.*, J. Alloys Compd. 586, 113 (2014). Copyright 2014 by Elsevier.

Meanwhile, Cao *et al.*[175] synthesized Mg<sub>98</sub>In<sub>5</sub>Al<sub>5</sub>Ti alloy by plasma milling to explore the dual-modifying effects of added elements of In, Al, and Ti. In particular,

Lu *et al.*[176, 177] described the hydrogen storage performance of a set of Mg-In-Ni ternary alloys and their structural transformation during hydrogenation and dehydrogenation, and investigated the mechanisms of dual modifying effects. For the first time, they observed the reversible hydrogen-induced phase change between the two new Mg-In-Ni ternary intermetallic compounds (Mg<sub>14</sub>In<sub>3</sub>Ni<sub>3</sub> and Mg<sub>2</sub>InNi). In the hydrogenation process, the Mg<sub>14</sub>In<sub>3</sub>Ni<sub>3</sub> alloy breaks up into a combination of MgH<sub>2</sub> and Mg<sub>2</sub>InNi, which is entirely reversible in the dehydrogenation reaction with a hydrogen storage content of 1.8 wt.% (Eq. (18)).

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$$8MgH_2 + 3Mg_2InNi \rightleftharpoons Mg_{14}In_3Ni_3 + 8H_2$$
 (18)

The reaction enthalpy and dehydrogenation activation energy for the dehydrogenation of MgH<sub>2</sub> and Mg<sub>2</sub>InNi were calculated to be 70.1 kJ (mol<sup>-1</sup> H<sub>2</sub>) and 78.5 kJ mol<sup>-1</sup>, respectively, both of which are lower than that of pure MgH<sub>2</sub> (Figure 22). The *in-situ* XRD patterns for the hydrogen release of hydrogen absorbed Mg<sub>14</sub>In<sub>3</sub>Ni<sub>3</sub> at several temperatures are displayed in Figure 23. The reversible synthesis of these two novel Mg-In-Ni ternary phases destabilizes both the dehydrogenation thermodynamics and kinetics of MgH<sub>2</sub>.

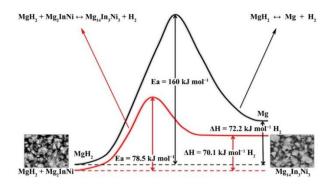


Fig. 22. The energy barrier schematic diagram of Mg-In-Ni ternary alloys. Reproduced by permission from Lu *et al.*, J. Phys. Chem. C 119, 26858 (2015). Copyright 2015 by

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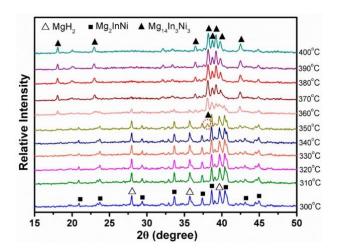


Fig. 23. *In situ* XRD patterns for the dehydrogenation of hydrogenated Mg<sub>14</sub>In<sub>3</sub>Ni<sub>3</sub> (the mixture of MgH<sub>2</sub> and Mg<sub>2</sub>InNi) at different temperatures. Reproduced by permission from Lu *et al.*, J. Phys. Chem. C 119, 26858 (2015). Copyright 2015 by ACS publications.

### 3.3.2 Adopting novel synthetic techniques

Thus far, many new techniques have been developed to synthesize MgH<sub>2</sub> for hydrogen storage, such as mechanical milling,[178] thin-film technology,[179] hydrogen plasma metal reaction,[180] hydriding chemical vapor deposition,[9] melt spinning,[181] severe plastic deformation,[182, 183] chemical reduction,[184] and electro-chemical deposition.[185] Particularly, severe plastic deformation technique has been receiving extensive attention as it can be developed to control the microstructural evolution (decreasing grain sizes, increasing the density of defects, inducing the formation of textures, designing special types of grain boundaries and increase the degree of supersaturation), control the surface reactivity (and easy contamination that comes with it) and evaluate alternatives for scaling-up production. [183, 186] For example, Mg and MgH<sub>2</sub> powders have been processed by high-pressure

torsion (HPT) to reduce the crystallite size, generate defects and promote consolidation of the powders, which clearly improve the surface resistance to atmospheric gases.[183] With the same principle, there are many types of severe plastic deformation techniques, e.g., HPT,[112, 187] extensive equal-channel angular pressing (ECAP) [188], and accumulative roll bonding (ARB), etc.[189, 190]

Skripnyuk *et al.*[182] was pioneered to fabricated the nanostructured ZK60 Mg-based alloys or composites by severe plastic deformation techniques. Other Mg-based alloys such as MgMmNi[191] and MgNi alloys, have also been processed by severe plastic deformation techniques later,[192] e.g., showing the improvement in hydrogenation performance of MgNi alloy associated with the chemical inhomogeneity induced by ECAP processing. Other processing technique such as extensive rolling or ARB have also been used to prepare laminate composites.[193-196] During the ARB processing, two plate specimens (different compositions or not) are stacked and rolled for several passes, as schematically shown in Figure 24, which therefore induce the severe plastic deformation with high strain and strain rate on the specimens, thereby leading to an ultra-fine microstructure finally.



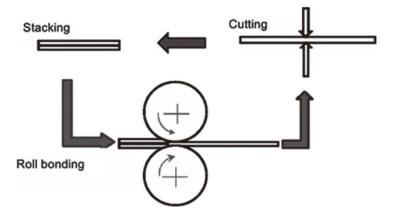


Fig. 24. Schema of ARB process. Reproduced by permission from Valiev *et al.*, Prog. Mater Sci. 51, 881 (2006). Copyright 2006 by Elsevier

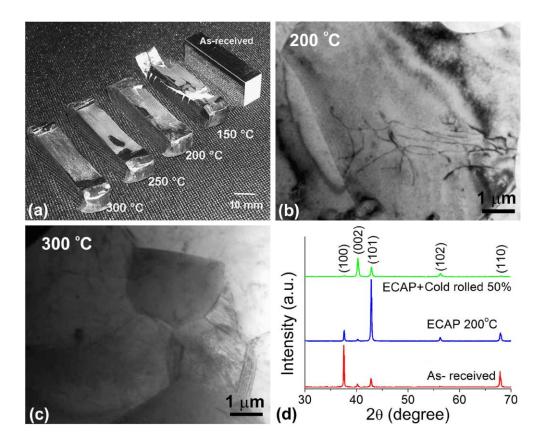


Fig. 25. AZ31 alloy processed by ECAP and ECAP plus cold rolling. (a) Photograph of the specimens after two passes of ECAP at the indicated temperatures; (b) and (c) TEM bright-field images after ECAP processing: (b) ECAP at 200°C; (c) ECAP at 300°. (d) XRD patterns comparing the conditions of as-received (extruded), after ECAP at 200°C, and after ECAP at 200°C followed by cold rolling. Reproduced by permission from Leiva *et al.*, Int. J. Mater. Res. 100, 1739 (2009). Copyright 2009 by Carl Hanser Verlag.

In addition, different severe plastic deformation technologies have also been incorporated to modify the hydrogen storage properties of Mg-based alloys.[197] For example, Figure 25 shows the AZ31 alloy processed by ECAP and cold rolling, [198] i.e., (a) the ECAPed processed samples and in (b) and (c) the resulting microstructures after processing at 200°C and 300°C, respectively. In Figure 25(d), the XRD patterns show the effect of cold rolling in establishing the (002) texture. Huot *et al.*[199]

reviewed the use of ECAP and CR for the enhancement of hydrogen sorption properties of Mg and Mg alloys. The effects of the processing route and type of texture they produced were associated with the hydrogen storage properties. Botta *et al.*[200] also reported the positive effects of texture, small grain size and free surfaces (or interfaces) for the hydrogen storage properties, after processing commercial Mg by melt-spinning, HPT and CR.

### 4. Conclusion and prospects

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In this review, we first introduce the classification of the Mg-based hydrogen storage alloys and then summarize some effective measures and the associated progress to enhance the hydrogen storage kinetics and thermodynamics of Mg-based compounds, such as alloying, nanostructuring, synthesizing metastable phases, doping catalytic additives, forming nanocomposite, changing the reaction way, and realizing dual modifying effects, etc. However, it should be noted that no candidate and advanced method can completely meet the demands for practical applications. For example, alloying, doping, synthesizing metastable phases, and changing the reaction path can effectively reduce the formation enthalpy; but unfortunately, sacrifice hydrogen storage content and some of the reactions are irreversible. Nanostructuring is also a promising method to modify the hydrogen storage properties, but the fabrication and weak stability of nanostructures continue to demand improvement. Forming Mg-based nanocomposite materials might be able to combine the excellence of alloy engineering, nanostructuring, and synergistic effects obtained by the RMM (reactive mechanical milling), leading to an instability in the thermodynamics of Mg/MgH<sub>2</sub>. Therefore, further studies on the kinetics and thermodynamics of Mg-based hydrogen storage compounds are still needed to be improved to achieve the practical application goals, possibly focusing on following several aspects:

- 1) Increasing more characteristic octahedral and/or tetrahedral sites to contain hydrogen and additionally possible vacancies to improve the hydrogenation properties of Mg-based materials, such as amorphization via the combination of crystalline and amorphous materials.[95, 201, 202]
- 2) Discovering a superior strategy to maintain the structural stability of nanostructuring. Prospectively, nanostructuring can significantly lighten kinetic barriers and decrease thermodynamic stability. Nevertheless, a great challenge of stability, for example, severe aggregation and structural collapse, is still existed during the hydrogenation/dehydrogenation process. Thus, more fabrications of stabilization should be investigated to elevate the storage capacity meanwhile exploring possible stabilization for the nanosized Mg in the absence of scaffolds, such as introducing graphene nanoribbons,[203] a second phase,[18, 204] and core-shell methods,[129, 205-207], etc.
- 3) Developing the novel preparation techniques to realize the dual modifying of thermodynamic and kinetic properties of Mg-based alloys, such as mechanical milling for nanostructuring, doping catalytic additives, and forming nanocomposites,[178] physical/chemical deposition for realizing nanocomposites,[184] and nanostructuring by wet chemical routes [85], severe plastic deformation,[183] and electrochemical approaches.[185]

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