

A high performance direct carbon solid oxide fuel cell fueled by Ca-loaded activated carbon

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Abstract

Ca-loaded activated carbon is developed as fuel for direct carbon solid oxide fuel cells (DC-SOFCs), operating without any carrier gas and liquid medium. Ca is loaded on activated carbon through impregnation technique in the form of CaO, which exhibits excellent catalytic activity and significantly promotes the output performance of DC-SOFCs. DC-SOFCs fueled by activated carbon with different Ca loading content (0, 1, 3, 5 and 7 wt. %) are tested and the performances are compared with the DC-SOFC

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running on the conventional Fe-loaded activated carbon. It is found that the performance of the DC-SOFC with 5 wt. % (373 mW cm⁻²) and 7 wt.% (378 mW cm⁻²) Ca-loaded activated carbon is significantly higher than that of the cells operated on 5 wt.% Fe-loaded activated carbon, 1 wt.% and 3 wt.% Ca-loaded activated carbon. The discharging time and fuel utilization of the DC-SOFC with 5 wt. % Ca-loaded activated carbon are also the optimal ones among all the cells. The microstructure, element distribution and carbon conversion rate of the Ca-loaded carbon, the impedance spectra of the corresponding DC-SOFCs are measured. The reasons for the reduced fuel utilization of 7 wt. % Ca-loaded carbon fuel are analyzed and the advantage of Ca-loaded carbon for DC-SOFCs is demonstrated in detail.

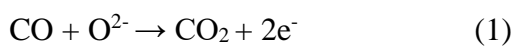
Keywords: Solid oxide fuel cells, Carbon fuel, Ca catalyst, Boudouard reaction

1. Introduction

Currently, fossil fuel is still the major energy source in the world, contributing to 80% of the global primary energy supply [1]. Coal, as the major part of fossil fuels, is abundant and widely available, especially in China [2]. However, the conversion efficiency of conventional coal-fired power plants is relatively low and very difficult to further enhance, due to the limitations of the Carnot cycle. Recently, direct carbon fuel cell (DCFC) has received considerable attention for energy conversion from carbon to electricity, because of its high energy efficiency, environment friendliness and high fuel

utilization [3-10]. Unlike the conventional heat engines, direct carbon fuel cell is not limited by Carnot cycle [3]. Benefitting from the abundant carbon sources and lower CO₂ emissions, DCFC offers advantages of low cost of fuel and less environment impact [11]. Therefore, DCFC might be a promising future power generating technology, as well as a clean coal technology [12-15].

Direct carbon solid oxide fuel cell (DC-SOFC) is a kind of DCFCs with whole solid state configuration, without carrier gas or liquid medium [16-22]. As early as 1988, Nakagawa and Ishida [16] designed a DC-SOFC without any liquid medium and proposed the mechanism of a DC-SOFC as the coupling of electrooxidation of CO on the anode (1) and the Boudouard reaction on the surface of carbon (2).



As the electrochemical characteristics of the cells operating on CO and solid carbon are exactly the same, Xie et.al. verified this mechanism indirectly [21]. Therefore, catalyzing the carbon gasification reaction (the Boudouard reaction) is a simple and effective way to improve the DC-SOFC performance [18, 23, 24]. Iron is one of the efficient catalysts. Tang et. al. demonstrated that the use of Fe catalyst for Boudouard reaction could enhance the performance of DC-SOFCs [18]. Later on, a Ni-YSZ anode-supported SOFC stack fueled by 5 wt. % Fe-loaded activated carbon was developed and yielded a peak power density of 465 mW cm⁻² at 850 °C [20]. Similarly, Skrzypkiewicz et. al. investigated DC-SOFCs operated on Fe₂O₃-loaded carbon fuels.

With Fe₂O₃-loaded carbon, the DC-SOFC delivered a peak power density of 152 mW cm⁻² at 850 °C [25] . Other Boudouard reaction catalysts, like Li, K, Ni and Ca (10 wt. %), were also investigated to promote the DCFC performance [11, 23]. However, compared to a hydrogen fueled SOFC (over 1000 mW cm⁻², at 800 °C), the performance of DC-SOFC (424 mW cm⁻², at 850 °C) [20] is still unsatisfactory. Therefore, to enhance the output performance and fuel utilization of DC-SOFCs, it is necessary to develop more effective catalysts for carbon fuel in DC-SOFCs.

In this work, we report a high performance Ca-loaded activated carbon DC-SOFC, with good fuel utilization. Through the impregnation method, Ca is loaded on the activated carbon in the form of CaO, similar to the conventional Fe-loaded activated carbon for DC-SOFCs. The performances of the DC-SOFCs operated on carbon fuels with different Ca loading content (1-7 wt. %) are compared with that of the DC-SOFC with Fe-loaded (5 wt. %) carbon fuel. The microstructure, element distribution and carbon conversion rate of the Ca-loaded carbon, the impedance spectra of the corresponding DC-SOFCs are measured. The reason for the reduced fuel utilization of 7 wt. % Ca-loaded carbon fuel is analyzed and the advantage of Ca-loaded carbon for DC-SOFCs is demonstrated in detail.

2. Experimental

2.1. Pre-treatment of carbon fuels

Pure activated carbon powders were prepared by crushing activated carbon

granules (Activated Charcoal, 8-16 mesh, Aladdin) using an electric grinder, followed by sieving through a sieve (77 mesh). Six kinds of carbon fuel were prepared (Table 1). 1 wt. %, 3 wt. %, 5 wt. %, 7 wt. % of Ca and 5 wt. % Fe catalyst was loaded on the pure activated carbon powders by impregnation technique, which had been reported previously [18, 20, 23]. $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$ and $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ were dissolved in purified water with a slight stirring, respectively. Under stirring, the pure activated carbon powders were added into the $\text{Ca}(\text{NO}_3)_2$ and $\text{Fe}(\text{NO}_3)_3$ solutions. After stirring for 1 h, the mixtures were heated at 80 °C till the solvent was evaporated. Afterwards, to decompose the nitrate, the catalyst-loaded carbon fuels were placed in a tubing oven, followed by heating at 700 °C for 1 h under N_2 atmosphere. After heat-treatment, $\text{Ca}(\text{NO}_3)_2$ and $\text{Fe}(\text{NO}_3)_3$ decompose into CaO and Fe_2O_3 , depositing on the surface of activated carbon. The form of CaO and Fe_2O_3 have been confirmed by the XRD of Ca-loaded activated carbon before cell operation (Fig. S1 in the supplementary material) and our previous work [26], respectively.

Table 1 – Activated carbon fuels with different catalyst and the performances of the corresponding DC-SOFCs operated on these carbon fuels at 850 °C.

	C-1	C-2	C-3	C-4	C-5	C-6
Catalyst	1 % Ca	3 % Ca	5 % Ca	7 % Ca	5 % Fe	none
Open circuit voltage/ V	0.96	0.98	1.0	1.01	0.96	0.92
Maximum power density/ mW cm ⁻²	324	358	373	378	352	258
Polarization resistance/ Ω cm ²	0.123	0.099	0.095	0.092	0.109	0.164

2.2. Fabrication of SOFCs

Electrolyte-supported button cells were fabricated and tested in this study. To improve the ionic conductivity of electrolyte, 1 wt. % alumina powder was added into Yttria-stabilized-zirconia (YSZ, TZ-8Y, Tosoh Corporation, Tokyo, Japan) [27, 28]. First, YSZ powder and alumina powder (Al_2O_3 , Xinfumeng, China, α -phase, 99.99 % purity) were mixed by wet ball-milling for 3 hours with zirconia balls as milling medium and alcohol as solvent, followed by drying the solvent under an infrared lamp. Then, electrolyte disks were prepared by uni-axial pressing of the Al_2O_3 -added-YSZ powders into pellets (each of 0.15 g in weight and 13 mm in diameter). After that, the pellets were sintered at 1400 °C for 4 hours in air atmosphere. The dense electrolyte pellets were about 300 μm in thickness and 11 mm in diameter. Ag-GDC is chosen to be the materials of anode and cathode, because silver and GDC are not only effective catalysts for electrochemical oxidation of CO, but also excellent anode materials for their high oxygen ion conductivity and electron conductivity [29], which are suitable for DC-SOFC [18]. To prepare anode and cathode, a Ag/GDC slurry was prepared by mixing 37 wt. % silver paste (DAD-87, with 80 wt. % Ag, Shanghai Research Institute of Synthetic Resins, Shanghai, China), 13 wt.% GDC ($\text{Gd}_{0.1}\text{Ce}_{0.9}\text{O}_{2-\delta}$, purity $\geq 99.5\%$, particle size (d_{50}): 0.5-3 μm , Ningbo Institute of Materials Technology & Engineering, China) and 50 wt.% polyvinyl butyral alpha-terpineol solution (weight concentration: 10 %) by grinding in an agate mortar for about 3 hours until the slurry was uniform. Afterward, the resulting slurry was painted onto both sides of the electrolyte disks, and

then annealed at 880 °C in air for 4 hours. The cathode area was controlled to be 0.22 cm², using a mask with a hole in the middle. Finally, SOFCs with a configuration of Ag-GDC/YSZ/Ag-GDC were obtained.

2.3. Cell assembling and characterization

In order to test the SOFCs, silver paste was used as sealing and jointing materials to connect the cells to one end of an alumina tube. Silver wires were attached to the anode and cathode, and connected to an Iviumstate electrochemical analyzer (Ivium Technologies B.V., Netherlands). A SOFC operated on humidified hydrogen (3 vol.% H₂O) was first tested to evaluate the performance of the typical as-prepared SOFCs. The H₂ gas flow rate was 30 mL min⁻¹. For the cells operated on solid carbon fuels, including the five catalyst-loaded activated carbon fuels and pure activated carbon, 0.4 g carbon was filled into each cell. For the other end of the alumina tube, a rubber stopper with a plastic gas-guide pipe was used to block, and leading the emitted gas out. In all testing, the cathode side was exposed to ambient air (Fig. 1). An alternating current voltage perturbation of 10 mV was applied in equilibrium within a frequency range of 0.1- 10⁵ Hz to measure the impedance of the cells. The microstructures of the SOFCs and EDX were characterized by a scanning electron microscope (SEM, Carl Zeiss AG-Merlin, Germany). The reactivity of all the catalyst-loaded carbon fuel in this experiment is investigated under programmed-temperature conditions using a Thermogravimetric analyzer (TGA, Mettler Toledo, Switzerland). In each gasification

experiment, 4-5 mg of carbon fuel was loaded in ceramic pan under a flowing N₂ atmosphere with a flow rate of 50 ml min⁻¹ and a heating rate of 20 °C min⁻¹ from 25 °C to 850 °C. After the temperature reached 850 °C, the atmosphere was switched to CO₂ (50 ml min⁻¹). X-ray diffraction (XRD, Rigaku D/max-III A diffractometer, Japan, Cu-Kα radiation, operated at 35 kV, 30 mA, $\lambda = 1.54184 \text{ \AA}$) was performed on the Ca-loaded carbon fuel before and after discharging process.

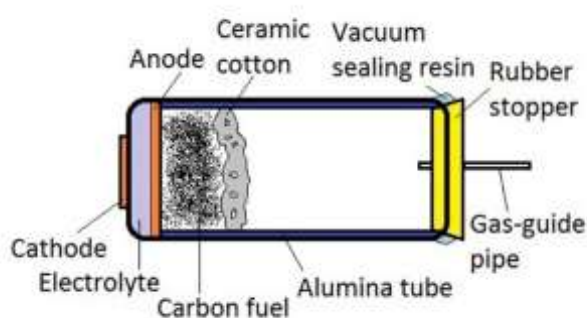


Fig. 1 – Schematic diagram of a DC-SOFC.

3. Results and discussion

3.1. Characteristics of the as-prepared SOFCs

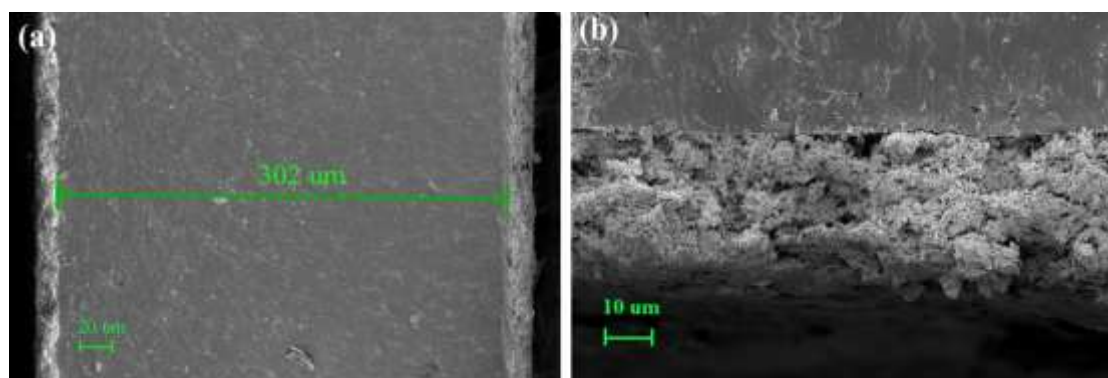


Fig. 2 – SEM pictures of cross-section (a, scale: 300) and anode (b, scale: 1000) of the as prepared SOFC.

157

158 The microstructures of the as prepared SOFCs are shown in Fig. 2. From the
159 section image (Fig. 2a), we can see that the YSZ electrolyte is quite dense, only with
160 some closed pores which will not affect the gas tightness of the cell. The thickness of
161 the YSZ electrolyte is about 300 μm . The anode layer, with a thickness of 20 μm ,
162 closely attaches to the YSZ electrolyte substrate. The surface image of the anode (Fig.
163 2b) shows that the anode is fairly porous with relatively uniform microstructure.

164 To evaluate the performance of a SOFC, the power output curve and impedance
165 spectra of a typical as-prepared SOFC operated at 850 $^{\circ}\text{C}$, with humidified H_2 (3 vol.%
166 H_2O) as fuel, are measured. As shown in Fig.3 (a), an open circuit voltage of 1.05 V
167 and a maximum power density of 404 mW cm^{-2} are obtained, showing that the SOFCs
168 are well prepared. The high linearity of I-V curve is caused by the high electrolyte
169 resistance of DC-SOFC, and the cathode contribution is overshadowed.

170 The errors are calculated through the standard deviation of the data. In the
171 experiment, we controlled the voltages and measured the corresponding currents.
172 Hence the voltages are represented in X-axis and currents Y-axis in Fig. 3 (a). As we
173 can see, the performance errors of the hydrogen cells are very small, indicating that the
174 quality of the as-prepared cells is reliable.

175 Fig.3 (b) is the impedance spectrum of the SOFC under open circuit voltage. As
176 we know, the intercept of the real axis at high-frequency, which represents the ohmic
177 resistance of the cell, is about 0.53 $\Omega \text{ cm}^2$. The low frequency intercept with the real

axis represents the overall resistance of the cell, which is $0.61 \, \Omega \, \text{cm}^2$. Therefore, the polarization of the H_2 fuelled SOFC is $0.08 \, \Omega \, \text{cm}^2$ ($0.61-0.53=0.08 \, \Omega \, \text{cm}^2$).

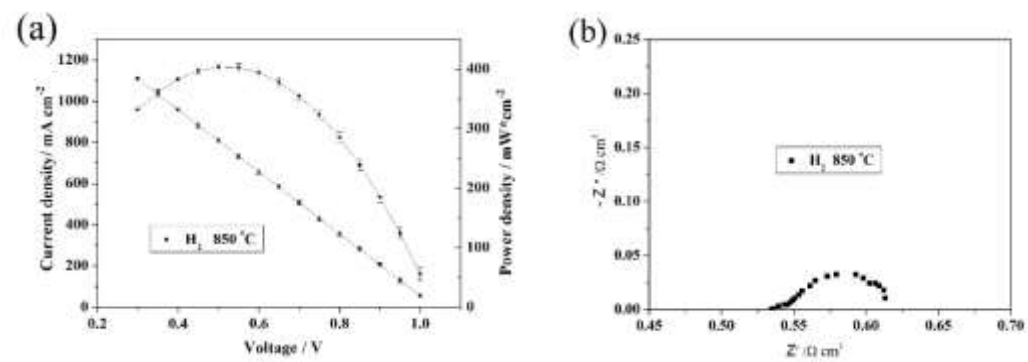


Fig. 3 – The output performance plot with error bars (a) and impedance spectra (b) of a typical as-prepared SOFC operated at 850 °C using H_2 as fuel gas.

3.2. Characterizations of carbon fuels

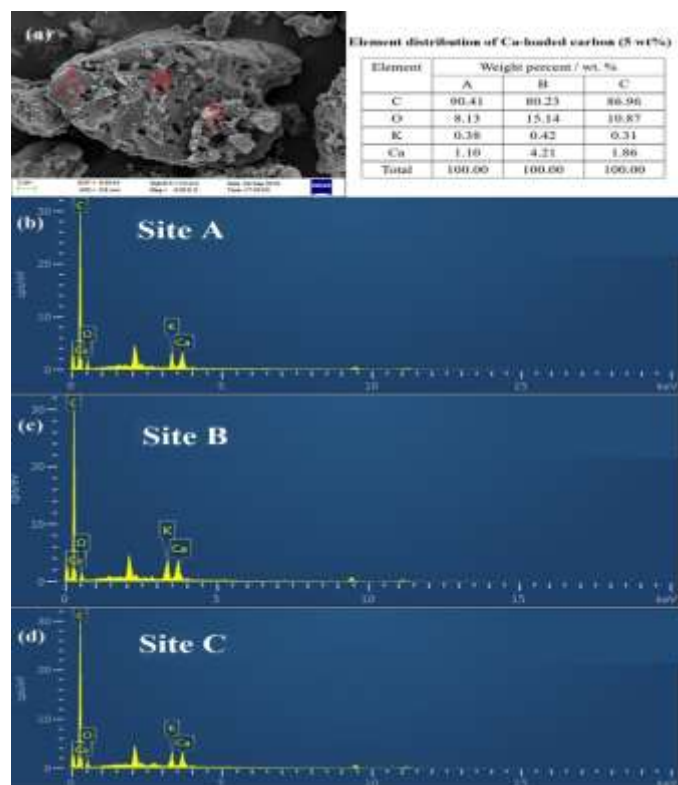


Fig. 4 – SEM image (a) and EDX diagrams of the Ca-loaded activated carbon fuel (5 wt. %) on different sites.

188

189 The microstructure and EDX spectra of Ca-loaded activated carbon fuel on
190 different site are shown in Fig. 4. The surface of the carbon particle is rough with some
191 pores in the bulk, which explains its large surface area. The existence of Ca element of
192 carbon is verified by the EDX measurement. However, the amount of Ca element on
193 smooth surface (site A) is lower than that on holes (site B) and rough surface (site C).
194 It might be caused by the capillary action. The Ca catalyst is loaded on carbon using
195 $\text{Ca}(\text{NO}_3)_2$ aqueous solution as Ca source by impregnation method. Holes on carbon
196 particle provide a room to store $\text{Ca}(\text{NO}_3)_2$ aqueous solution, resulting a higher Ca
197 content on holes and portals. Furthermore, the different distribution of oxygen-
198 containing functional groups on carbon particle might result in the different distribution
199 of Ca catalyst, as the functional groups have a strong adsorption force to metal ions.
200 In addition, the peaks in the EDX diagrams (2.1, 2.2 and 9.5 keV) is attributed to Au,
201 which is a conductive additive to increase the electron conductivity of the sample in
202 scanning electron microscope.

203

204 *3.3. Electrochemical performance of DC-SOFCs*

205 In a DC-SOFC, CO is formed through the Boudouard reaction (2) on the carbon
206 fuel and electrochemically oxidized on the anode of the cell (reaction 1) [21]. From
207 reaction (1), the electrochemical oxidation of CO generates the same molar amount of
208 CO_2 , which would diffuse to the carbon fuel and participate in the Boudouard reaction.

As a result, the OCV and output performance of a DC-SOFC are controlled by the concentration of CO, according to the Nernst equation. However, the concentration of CO is highly dependent on the Boudouard reaction, indicating that the Boudouard reaction directly influences the electrochemical performance of a DC-SOFC. Therefore, the performance of a DC-SOFC operated on carbon fuel can be substantially enhanced by loading Fe catalyst on carbon to facilitate the Boudouard reaction. So far, one of the best reported DC-SOFCs performances has been achieved using 5 wt. % Fe-loaded activated carbon, as shown in Fig. 5a (C-5, 5 wt. % Fe).

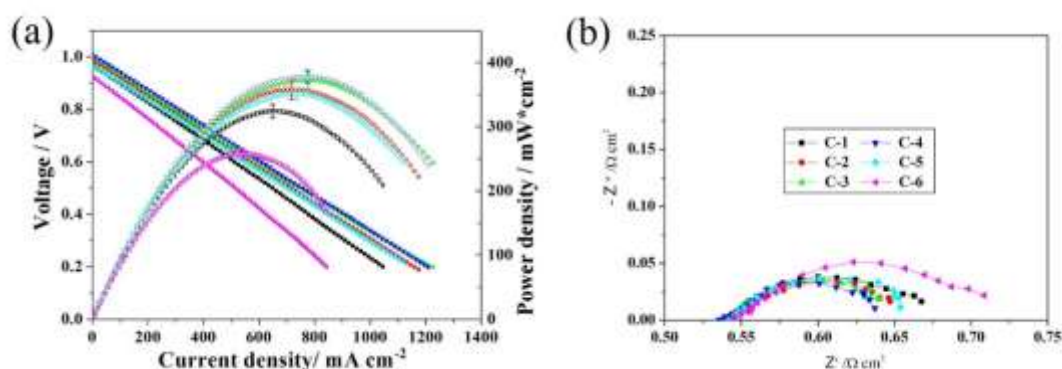


Fig. 5 – I-V-P characteristics (a) with error bars and impedance spectra (b) of the SOFCs operated at 850 °C using the different kinds of catalyst-loaded carbon fuel (C-1, 1 wt.% Ca; C-2, 3 wt.% Ca; C-3, 5 wt.% Ca; C-4, 7 wt.% Ca; C-5, 5 wt.% Fe and C-6, pure activated carbon).

The electrochemical characteristics of the DC-SOFCs operated on 1 wt. %, 3 wt. %, 5 wt. %, 7 wt. % Ca-loaded activated carbon, 5 wt. % Fe-loaded activated carbon and pure activated carbon are shown in Fig. 5 and listed in Table 1. Because of the identical

226 fabricating technique for preparing the cells and operating temperature, the
227 performance difference of the cells should be attributed to the difference of carbon fuel.
228 As shown in Table 1, the performances of the DC-SOFCs operated on the carbon fuels
229 loaded with catalyst, including Ca and Fe, are significantly higher than that with pure
230 carbon fuel (258 mW cm^{-2}), indicating that loading catalyst on carbon fuel is an
231 effective way to improve the output performance, which has been demonstrated by Tang
232 and Liu from our group [18]. For comparison, 5 wt. % Ca-loaded activated carbon DC-
233 SOFC gives a peak power density of 373 mW cm^{-2} , which is even higher than that
234 fueled by 5 wt. % Fe-loaded activated carbon (352 mW cm^{-2}), indicating that Ca
235 exhibits good catalytic effect for Boudouard reaction. What's more, the power densities
236 and OCVs of Ca-loaded activated carbon DC-SOFCs are improved with increasing Ca
237 content from 1 wt. % to 7 wt.%. However, as shown in Table 1, performance difference
238 between 5 wt. % and 7 wt. % Ca content is negligible. In other words, when Ca content
239 is over 5 wt. %, the cell performance improvement is limited. The performances of the
240 DC-SOFCs with Ca-loaded carbon fuel are also significantly higher than the result of
241 Li et. al. (about 150 mW cm^{-2} at 850°C with 10 wt. % Ca loading content) [30], which
242 might due to the totally different cell configuration, carbon phases and Ca loading
243 content. Fig. 5 (b) reveals the electrochemical impedance spectra of the DC-SOFCs
244 measured under open circuit voltage. The ohmic resistances of all the cells are almost
245 the same ($0.54 \Omega \text{ cm}^2$) due to the identical operating temperature and SOFC
246 configuration. However, the polarization resistances of the cells are different. The

lowest polarization resistance is attributed to the 7 wt. % Ca-loaded activated DC-SOFC and the highest polarization resistance is attributed to the pure activated carbon one. It is reasonable that the DC-SOFC operated on the pure activated carbon gives the largest polarization resistance, because the Boudouard reaction (2) rate might be too slow to provide sufficient CO for the electrochemical reaction (1), which also decreases the OCV. Generally, the resistance of a cell under discharging conditions is higher than that under OCV. However, in our experiment, the increased amount of resistance between OCV and discharging conditions is so small that it could be neglected, because of the high linearity of the I-V curves. The better performance and lower polarization resistance of the Ca-loaded activated carbon DC-SOFC than those of the DC-SOFC operated on Fe-loaded activated carbon suggests that the Boudouard reaction on the Ca-loaded activated carbon is better catalyzed than that on the other one, which has been demonstrated before. Huang et al. [31] studied the catalytic effect of alkali (K and Na), alkaline earth (Ca and Mg) and transition (Fe) metals on the Boudouard reaction of fir char and found that catalytic reactivity of the metals in the order of $K > Na > Ca > Fe > Mg$. Similarly, Lahijani et al. [32] investigates the influence of alkali (K and Na), alkaline earth (Ca and Mg) and transition (Fe) metal nitrates on CO₂ gasification reactivity of pistachio nut shell char. The results shows the catalytic reactivity in the order of $Na > Ca > Fe > K > Mg$.

These results support our conclusion that the catalytic activity of Ca is even better than that of Fe. However, to further demonstrate the above conclusion, the reactivity of

all the catalyst-loaded carbon fuel in the experiment is investigated under programmed-temperature conditions using a Thermogravimetric analyzer. Carbon conversion (x) is calculated using the following equation:

$$x = \frac{w_0 - w_t}{w_0 - w_r} \quad (3)$$

where w_0 is the initial mass of the char at the start of gasification, w_t is the mass at gasification time t , and w_r is the mass of ash and catalyst remaining after complete gasification. The carbon conversion of carbon fuel with different loading of catalyst is showed in the following figure (Fig. 6):

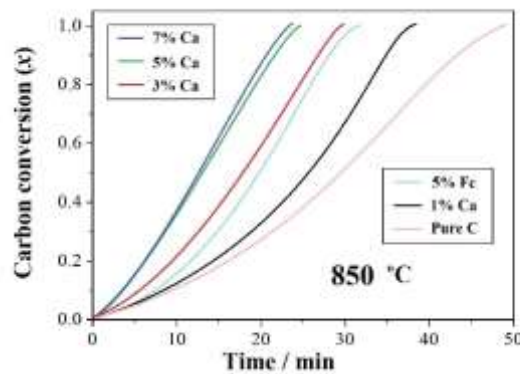


Fig. 6 - Carbon conversion of different catalyst-loaded carbon fuel at 850 °C.

As shown in Fig. 6, the gasification reactivity of carbon fuel enhances with the increasing loading content of Ca. However, carbon conversion rate of 7 % Ca-loaded carbon fuel is almost the same as that of 5 % Ca-loaded carbon, which further explains the results of the corresponding SOFC performances. The catalytic activity of Ca is higher than that of Fe with the same loading content. Such observation is in agreement with the results of Huang and Lahijani [31, 32].

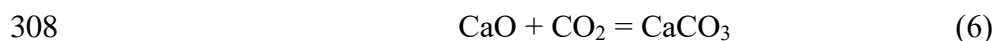
Both Fe and Ca are very effective catalysts to the Boudouard reaction. However, they are not necessarily better than any other metal oxides. For example, the transition metal Co is also a good catalyst for the Boudouard reaction, but its cost is much higher than that of Fe. Similarly, Ca oxide is the most inexpensive among the alkaline earth metal oxides. Meanwhile, the catalytic activity of Fe and Ca are comparable to that of the other transition metal and alkaline earth metal. Therefore, Fe and Ca are loaded on the carbon fuel of DC-SOFCs to promote the Boudouard reaction for producing sufficient CO to the redox reaction of the anode. In general, the mechanism of metal catalytic carbon gasification can be described by the “spill-over” model [33]. Firstly, CO₂ adsorbs and dissociates on a metal catalyst to form a metal catalyst-CO₂ complex. Secondly, the complex migrate to nearby carbon substrate to react with carbon, producing two CO molecules. For Ni catalyst, C dissolves and diffuses in nickel metal, and the carbon gasification takes place on the surface of the Ni metal-gas interface. For Fe catalyzed carbon fuel, carbon gasification can be described using the following model [34]:



where n and m represent different form of Fe catalyst, because Fe catalyst could be Fe₂O₃, FeO, Fe₃O₄ and Fe metal under different operating conditions [35]. The reaction rate-determining step is $\text{Fe}_n\text{O}_{m+1} + \text{C} = \text{Fe}_n\text{O}_m + \text{CO}$.

For the Ca catalyzed carbon gasification, CaO is highly active on chemisorption

306 of CO₂ and further to form CaCO₃, followed by the solid-state reaction between CaCO₃
307 and carbon. The mechanism is described as the following model [36]:



310 In this model, reaction (7) is the reaction rate-determining step. To gasify carbon
311 at the external surface, a catalyst particle must solubilize it at the internal surface. To
312 solubilize carbon atoms there must be active contact with carbon. To have active contact
313 a “sintering-like” faceting of the particle is required. [37] Therefore, Tammann
314 temperature (at which lattices begin to be appreciably mobile) is an important physical
315 condition to evaluate the catalytic activity of a metal oxide on the Boudouard reaction.
316 Actually, the Tammann temperatures of CaCO₃ (533 K) and Fe oxides (FeO (552 K),
317 Fe₂O₃ (633 K), Fe (632 K)) are much lower than that of other metal oxides, such as
318 MgO (1562 K), Cr₂O₃ (1081 K), V₂O₃ (833 K). Benefited from a low Tammann
319 temperature, Fe and Ca exhibit such good catalytic properties for the Boudouard
320 reaction.

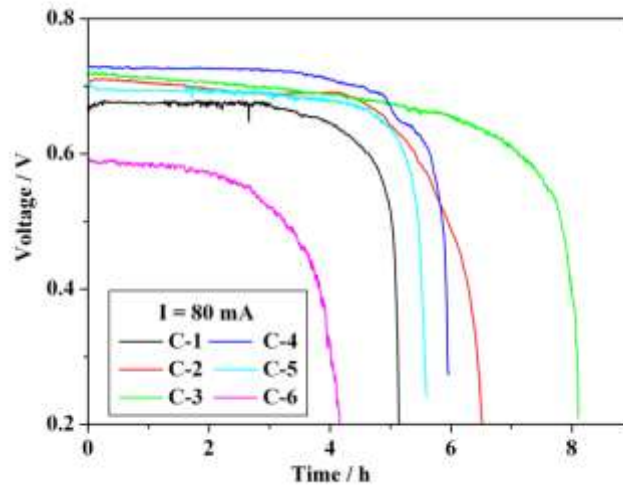


Fig. 7 – The discharging curves of DC-SOFCs with C-1 to C-6 fuels, respectively, operated at constant current (80 mA), at 850 °C.

Table 2 – The discharging times and fuel utilization of DC-SOFCs with C-1 to C-6 carbon fuels.

	C-1	C-2	C-3	C-4	C-5	C-6
Catalyst	1 % Ca	3 % Ca	5 % Ca	7 % Ca	5 % Fe	none
Discharging time/ h	5.15	6.53	8.11	5.96	5.60	4.40
Fuel utilization/ %	11.5	14.6	18.2	13.4	12.6	9.9

Fig. 7 is the discharging curves of the DC-SOFCs with a variety of carbon fuels at 850 °C and at a constant current of 80 mA (364 mA cm^{-2}). Under constant discharging current of 80 mA, the variation trend of the discharging plateaus of all the DC-SOFCs is consistent with that of the I-V-P curves. The discharging

333 times and corresponding fuel utilizations of the DC-SOFCs with the six carbon
334 fuels are listed in Table 2. Apparently, The C-3 (5 wt. % Ca-loaded activated
335 carbon) cell achieves the longest discharging time of 8.11 h, with a discharging
336 plateau significantly higher than that of C-6 (pure activated carbon, 4.40 h) cell
337 and C-5 (5 wt. % Fe-loaded activated carbon, 5.60 h) cell. The above results
338 demonstrate that loading a suitable amount of Ca on activated carbon can
339 promote the discharging time and fuel utilization of a DC-SOFC, which is
340 comparable to a Fe-loaded activated carbon. For the cell with C-4 fuel (7 wt. %
341 Ca-loaded activated carbon), the total test time is reduced to 5.96 h. As the
342 Boudouard reaction catalyst, Ca is distributed on the carbon fuel in form of CaO,
343 which tends to agglomeration and caking. Therefore, CaO might be
344 agglomerated when the amount of Ca increases to 7 wt. %, and further impacts
345 on the catalytic effect of Boudouard reaction and the discharging time of a DC-
346 SOFC. Moreover, the operated temperature is as high as 850 °C, which might
347 further promote the agglomeration of CaO. To demonstrate this conclusion, the
348 microstructures and element distribution are characterized through SEM and
349 EDX. As shown in Fig. 8 (a) and (b), the particles of the 7 wt. % Ca-loaded
350 activated carbon are highly porous, with an average particle size of about 20 μm .
351 EDX measurement on the surface of a particle shows that there is a small amount
352 of Ca (3.84 wt. %) distributed on the surface, as shown in Fig.8 (c). However,
353 after a cell operation of 80 mA at 850 °C, some larger agglomerates are formed,

as shown in Fig.8 (d) and (e). Fig.8 (f) shows an EDX analysis for the surface of such an agglomerate. As it shows, the weight percentage of Ca, C, and O is 38.28, 14.62, and 47.10, respectively. A mole ratio of Ca: C: O=1:1.25:3 is obtained based on these values. Thus it is reasonable to assume that Ca exists in the form of CaCO_3 .

The particle size and distribution of Ca catalyst are further measured by a laser particle size analyzer (LA-960 Laser Particle Analyzer, Horiba Scientific, Japan). Firstly, the 7 wt. % Ca-loaded carbon fuel before and after cell operation are fired in an oxygen atmosphere at 350 °C, respectively, to consume carbon and get Ca catalyst powders. Then the Ca catalyst powders are collected to measure particle size. The particle size distributions are shown in Fig. S2 in the supplementary material. Apparently, after cell operation, the particle size of Ca catalyst grows significantly from a distribution range of 0.1-10 μm to 1-60 μm . The average particle size of Ca catalyst before cell operation is 4.7 μm , and increases to 27.2 μm after cell operation, indicating that Ca catalyst powder particle is significantly grown and agglomerated under cell operation.

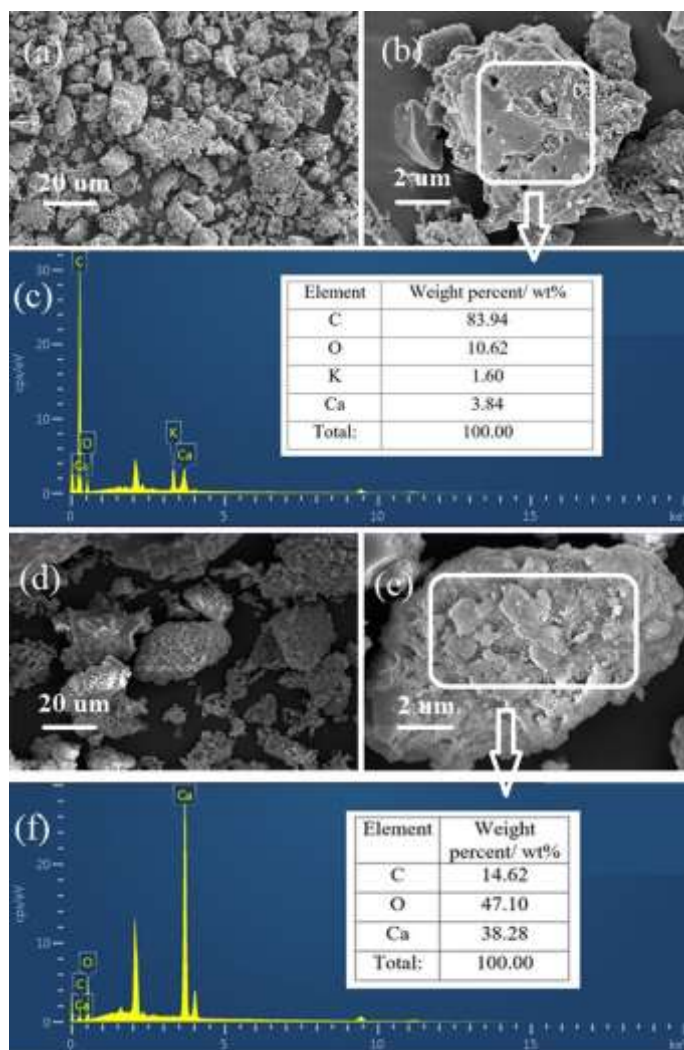


Fig. 8 - SEM pictures of 7 wt. % Ca-loaded activated carbon before (a and b) and after (d and e) cell operation, with corresponding element distribution diagrams (c and f).

In fact, a sintering process of carbon containing calcium is found when it is under prolonged thermal treatments or gasified to burn-off levels in CO_2 atmosphere [38]. Furthermore, the Ca catalyst reactivity decreases remarkably with the sintering process, because of the drop in the available surface area of Ca catalyst and contact area between Ca and C. Therefore, the agglomeration and

sintering of Ca catalyst might be the main reason for the reduced fuel utilization of DC-SOFC.

From Table 2, the total discharging time of C-3 cell is 8.11 h, at a constant discharge current of 80 mA. During the discharging test, there is 2336 C charge delivered, indicating that 0.072 g of carbon has been oxide through electrochemical reaction, calculating base on the overall reaction of the cell as $C + 2O^{2-} = CO_2 + 4e^-$ (4 electrons reaction). Therefore, the carbon fuel utilization of C-3 cell is 18.2 %, as 0.4 g carbon has been loaded into each DC-SOFC. Due to the longest discharging time, the C-3 cell gives the highest fuel utilization among all the cells, which is 45 % higher than that of the C-5 (5 % Fe-loaded activated carbon) cell. This is a further indication of the advantages of the Ca-loaded activated carbon for DC-SOFCs.

4. Conclusions

A Ca-loaded activated carbon is proved to be an excellent carbon fuel for DC-SOFCs. DC-SOFCs operated on solid carbon fuel loading with different Ca amount are tested. It is found that 5 wt. % Ca-loaded activated carbon is the most favoured carbon fuel for DC-SOFC, as the cell powered by 5 wt. % Ca-loaded activated carbon gives the maximum power density of 373 mW cm^{-2} , at 850°C , even slightly higher than that operated on the best reported 5 wt. % Fe-loaded activated carbon (352 mW cm^{-2}), and much larger than that of the cell with pure

carbon (258 mW cm^{-2}). Moreover, the fuel utilization of the DC-SOFC, operated at a constant discharging current of 80 mA and a cell voltage of about 0.7 V, with the 5 wt. % Ca-loaded carbon fuel is the highest among the six kinds of cell. With the same discharging current and higher discharging voltage, the cell with 5 wt. % Ca-loaded activated carbon exhibits 45 % larger discharging time and fuel utilization than that of the cell with Fe-loaded carbon fuel. However, when the amount of Ca increases from 5 wt. % to 7 wt. %, the discharging time and fuel utilization of the cell reduce to 73 %, with a limited superior output performance. SEM and particle size distribution of 7 wt. % activated carbon fuel demonstrated that the reduced fuel utilization might due to the agglomeration and sintering of Ca catalyst. All in all, comparing to the conventional Fe-loaded carbon, Ca-loaded carbon for DC-SOFCs has the advantages of lower cost, higher output performance and fuel utilization. It is a promising catalyst to load on carbon fuels for DC-SOFC.

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Figure captions

Fig. 1–Schematic diagram of a DC-SOFC.

Fig. 2 – SEM pictures of cross-section (a, scale: 300) and anode (b, scale: 1000) of the as prepared SOFC.

Fig. 3 – The output performance plot with error bars (a) and impedance spectra (b) of a typical as-prepared SOFC operated at 850 °C using H₂ as fuel gas.

Fig. 4 – SEM image (a) and EDX diagrams of the Ca-loaded activated carbon fuel (5 wt. %) on different sites.

Fig. 5 – I-V-P characteristics (a) with error bars and impedance spectra (b) of the SOFCs operated at 850 °C using the different kinds of catalyst-loaded carbon fuel (C-1, 1 wt.% Ca; C-2, 3 wt.% Ca; C-3, 5 wt.% Ca; C-4, 7 wt.% Ca; C-5, 5 wt.% Fe and C-6, pure activated carbon).

Fig. 6 - Carbon conversion of different catalyst-loaded carbon fuel at 850 °C.

Fig. 7 – The discharging curves of DC-SOFCs with C-1 to C-6 fuels, respectively, operated at constant current (80 mA), at 850 °C.

Fig. 8 - SEM pictures of 7 wt. % Ca-loaded activated carbon before (a and b) and after (d and e) cell operation, with corresponding element distribution diagrams (c and f).